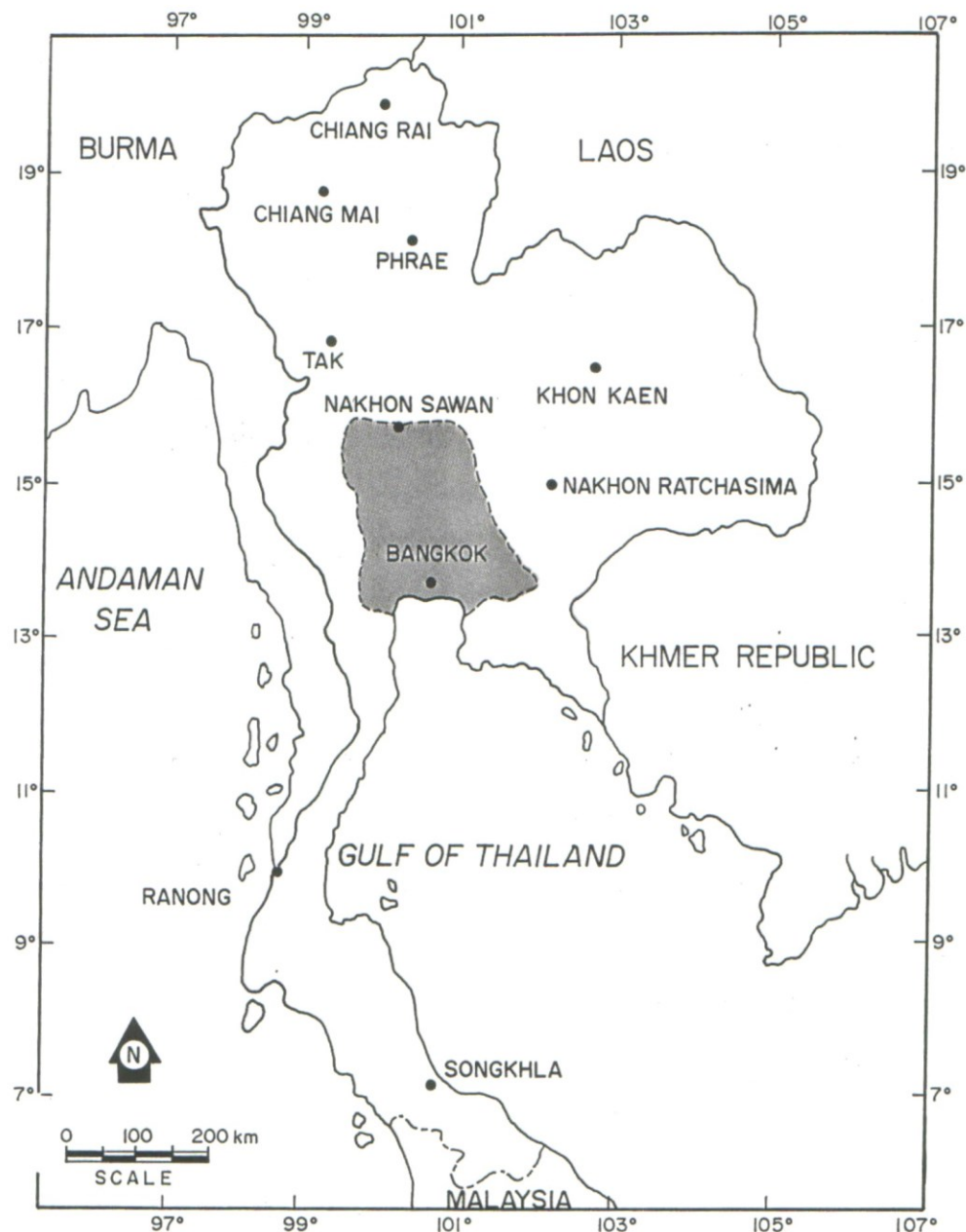


**Monday-4**

**Site Investigation Practice-Case  
studies**



**Location Map of the Lower Central Plain of Thailand  
Showing Approximate Location of Bangkok**

## Tall buildings in Bangkok city











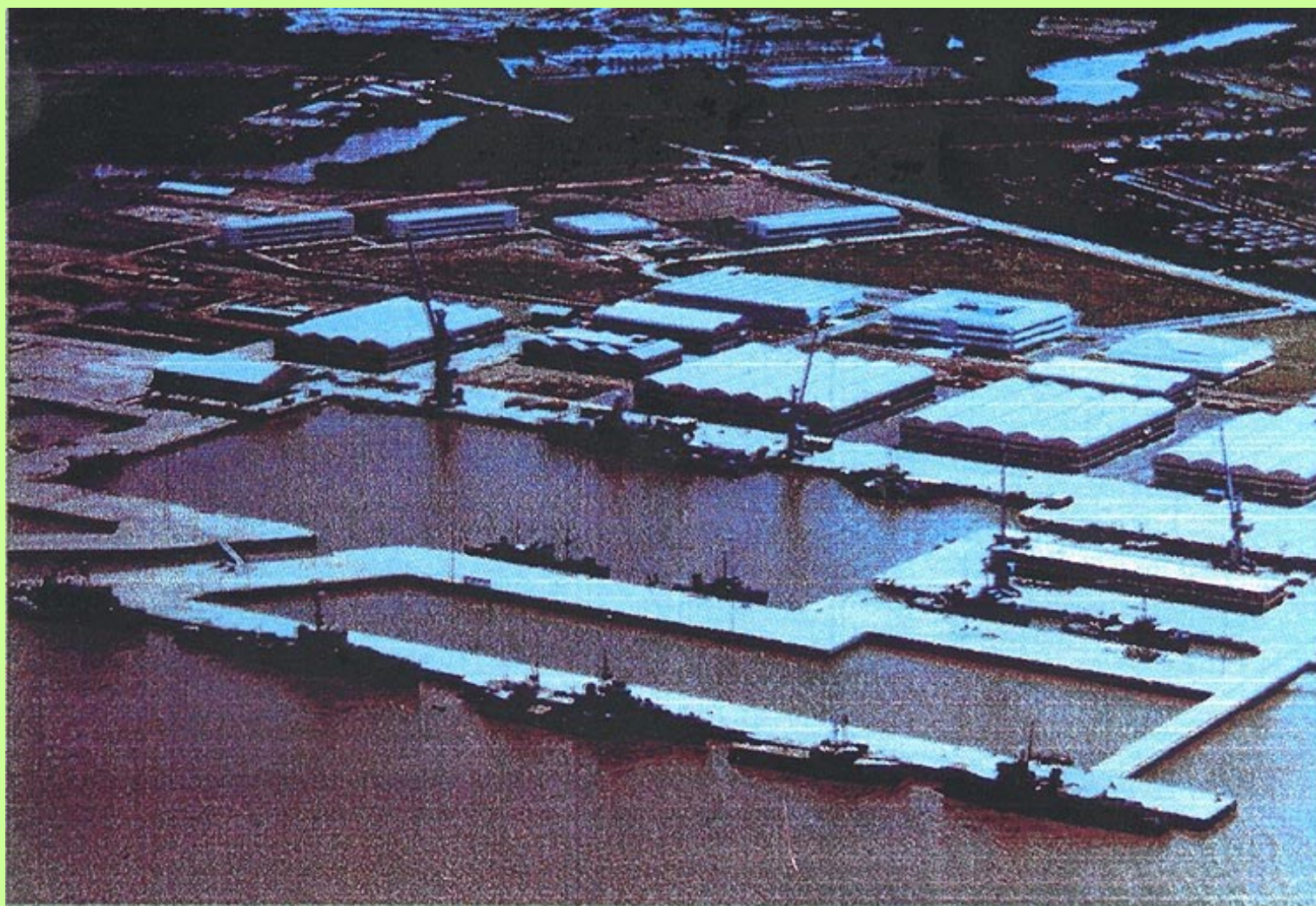






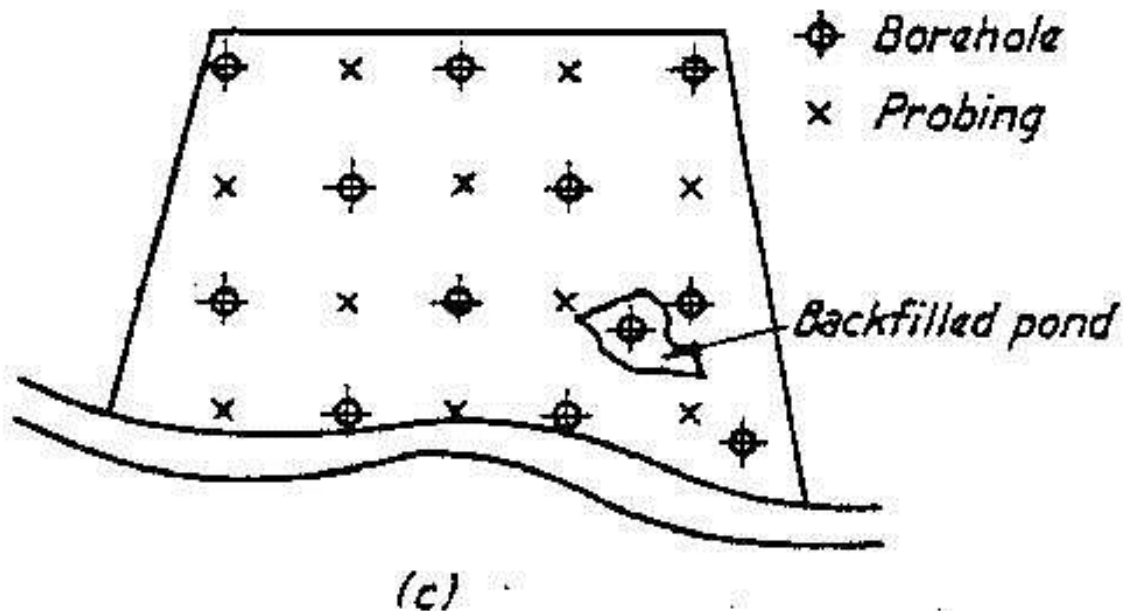
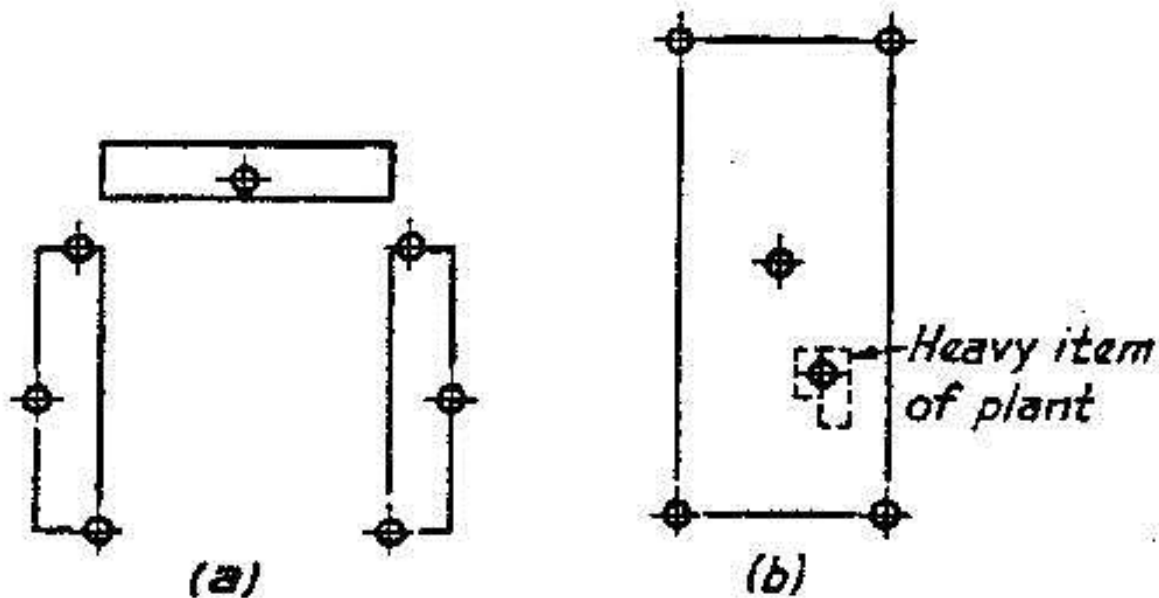




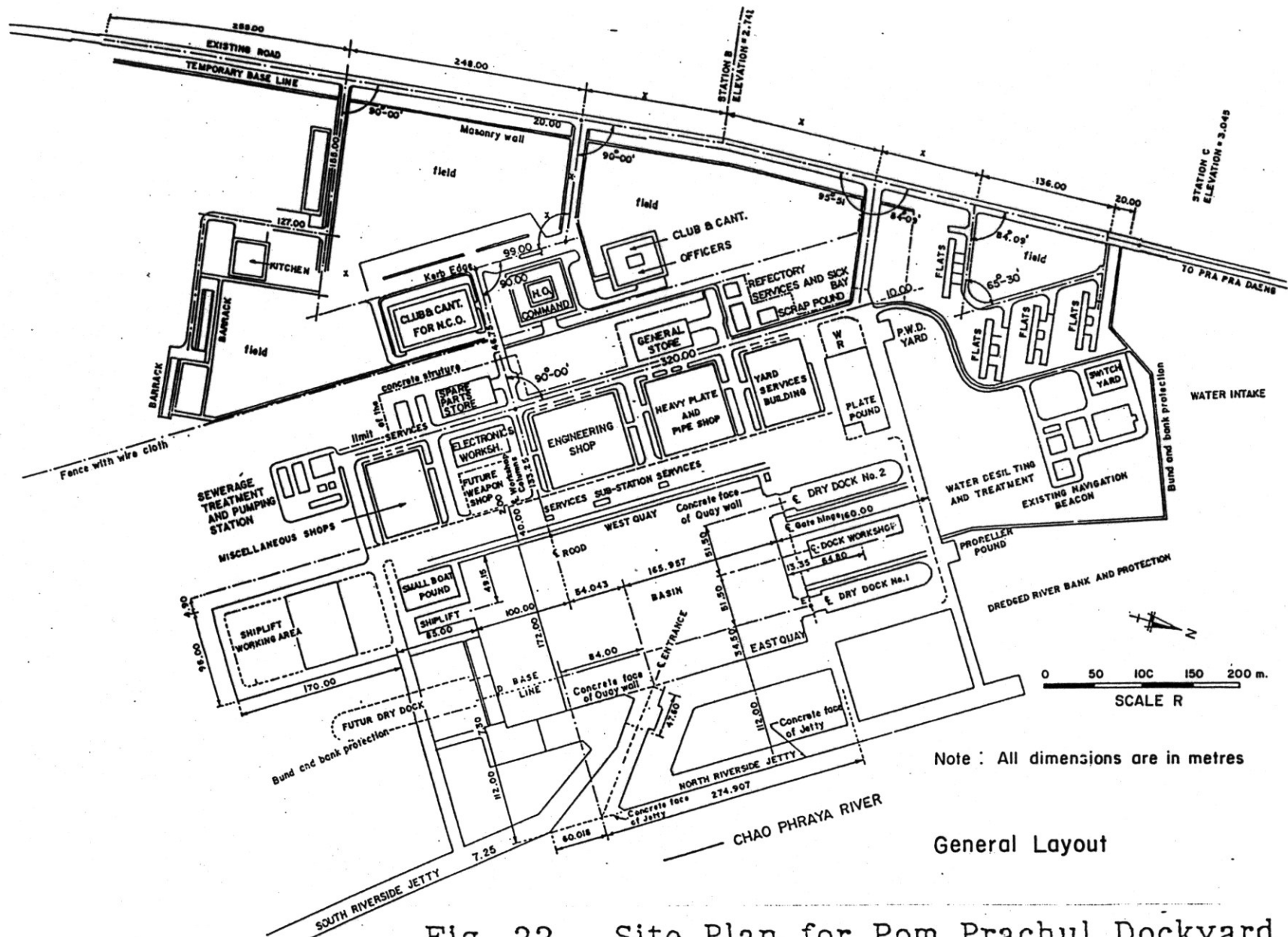




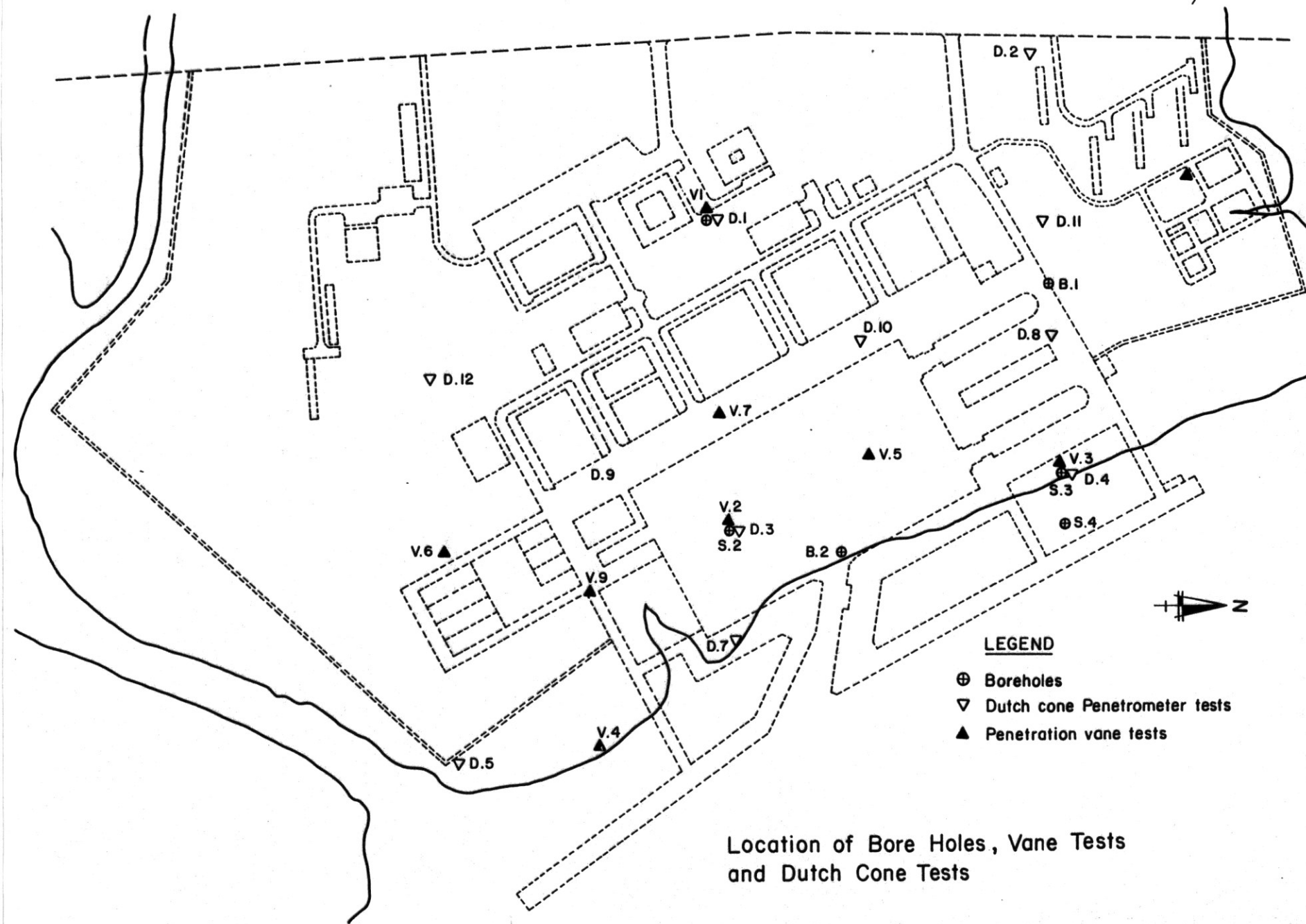
# Borehole numbers



# Borehole layout and in-situ tests







Location of Bore Holes, Vane Tests  
and Dutch Cone Tests

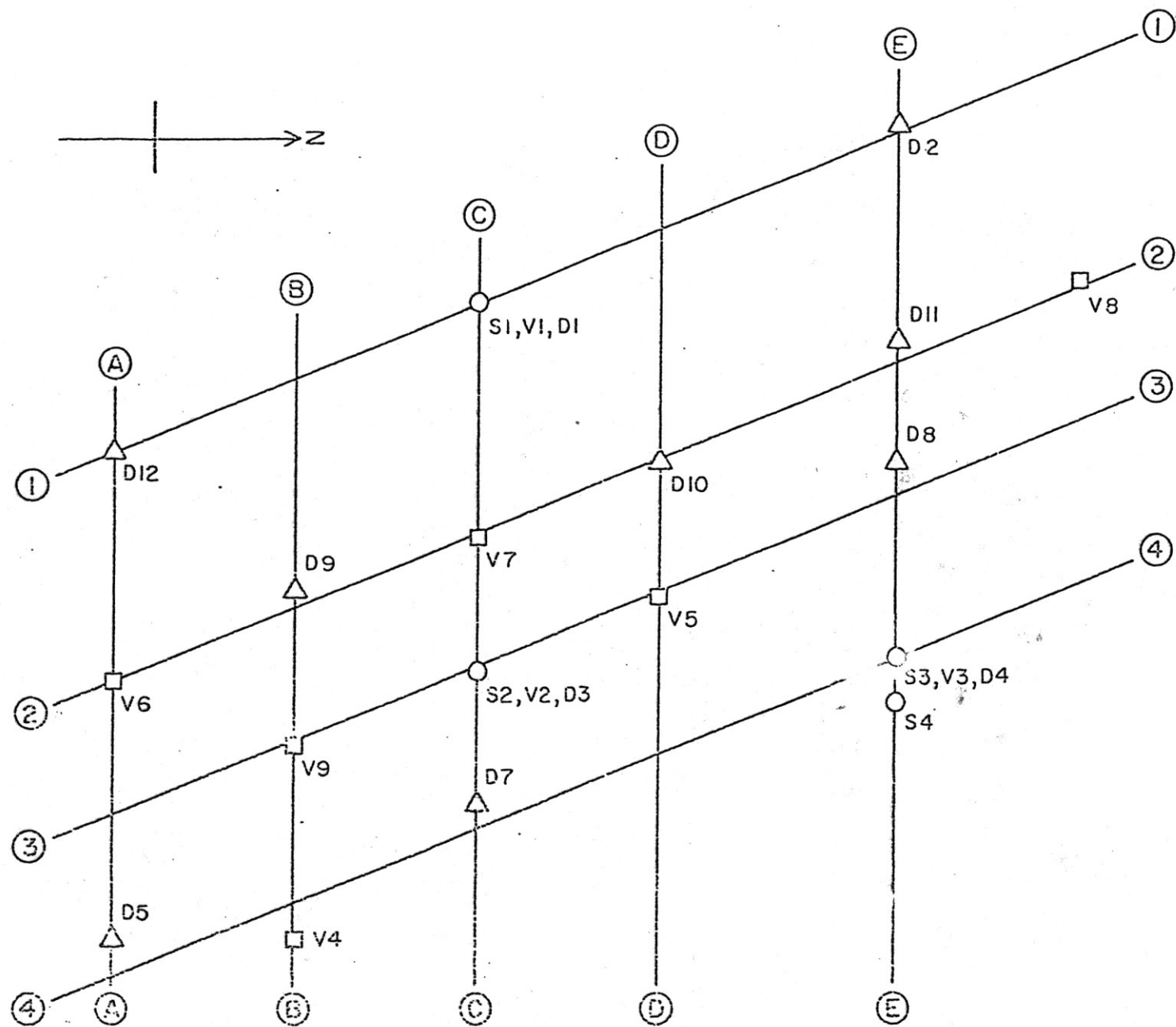


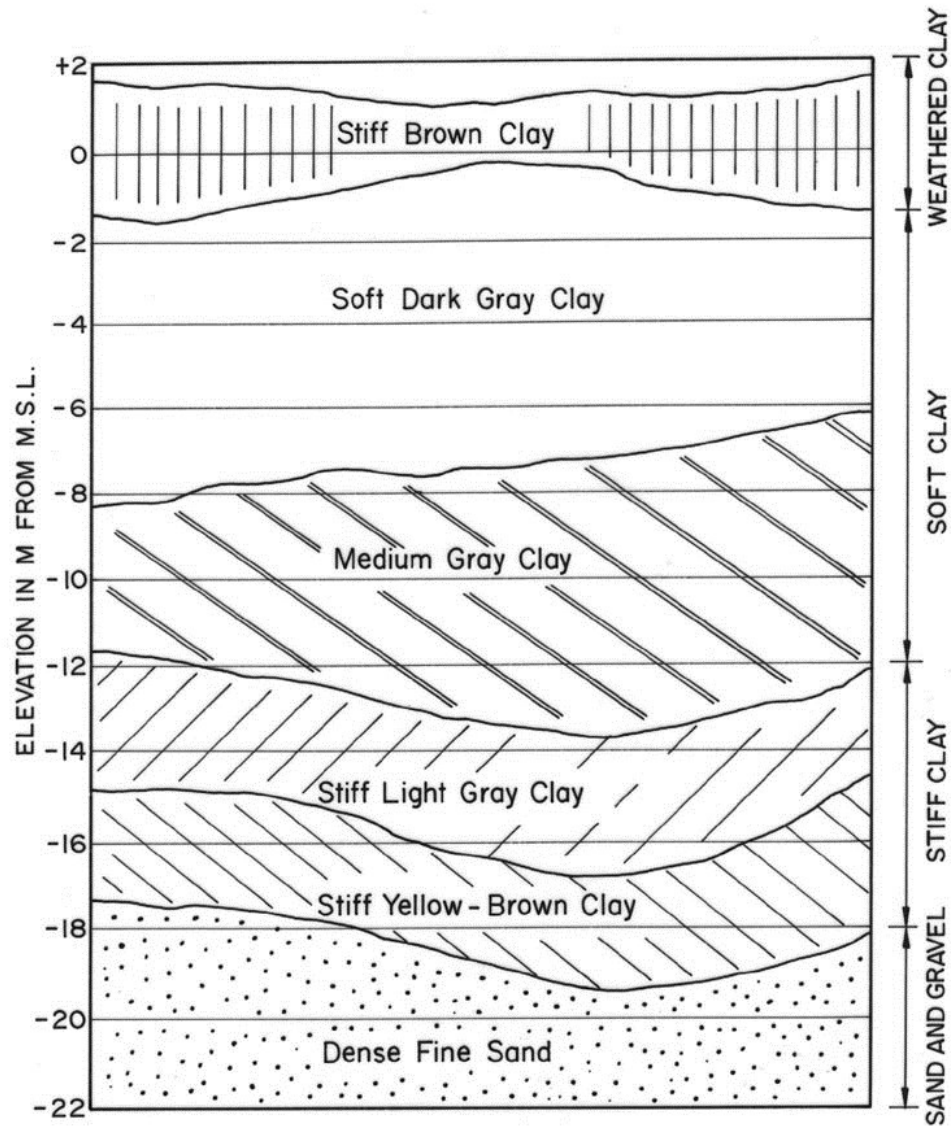
Fig. 5 Locations of Bore Holes , Vane and Dutch Cone Tests











**PROFILE OF BANGKOK SUBSOIL  
(AFTER MUKTABHANT ET AL , 1967 )**











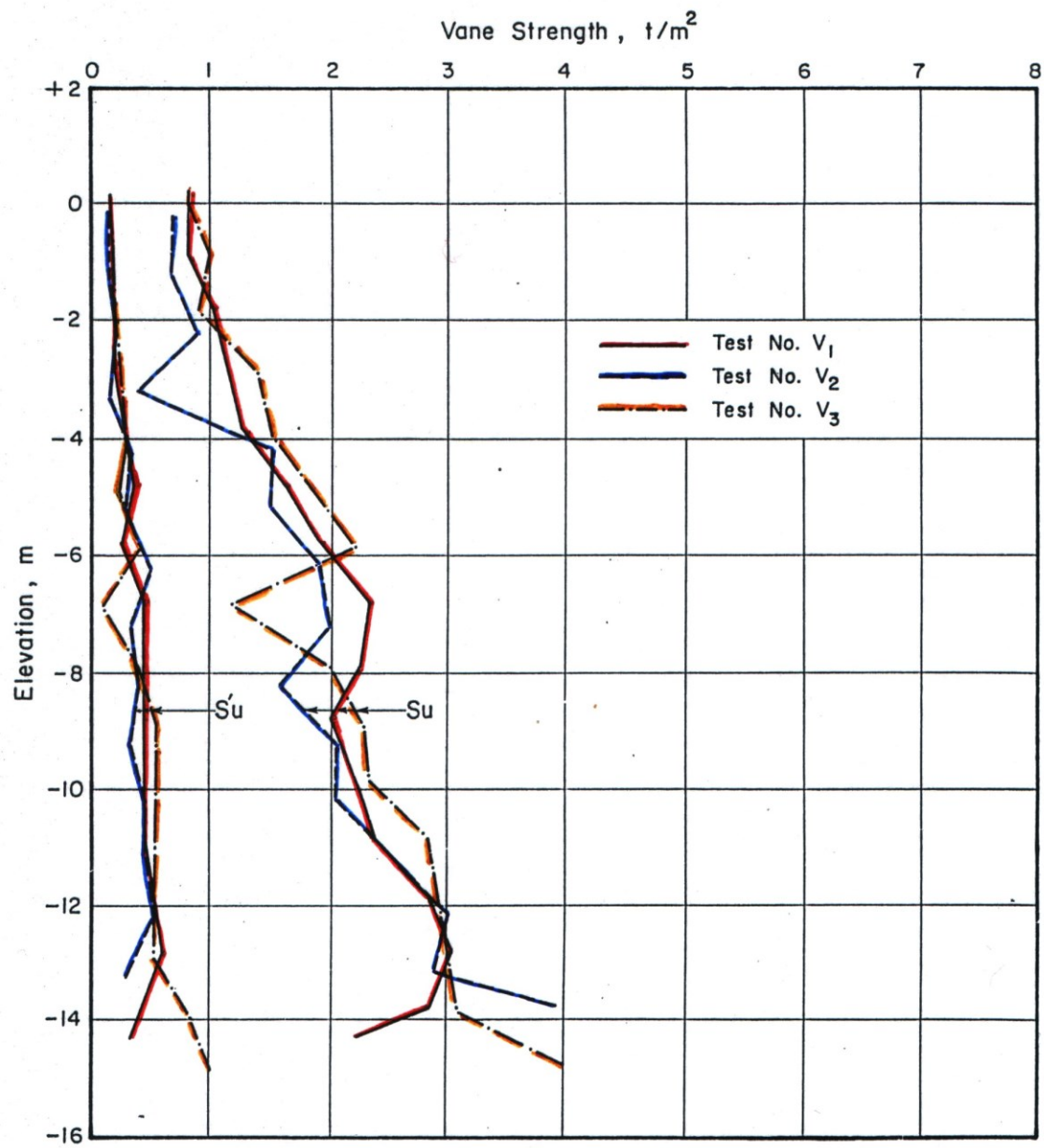
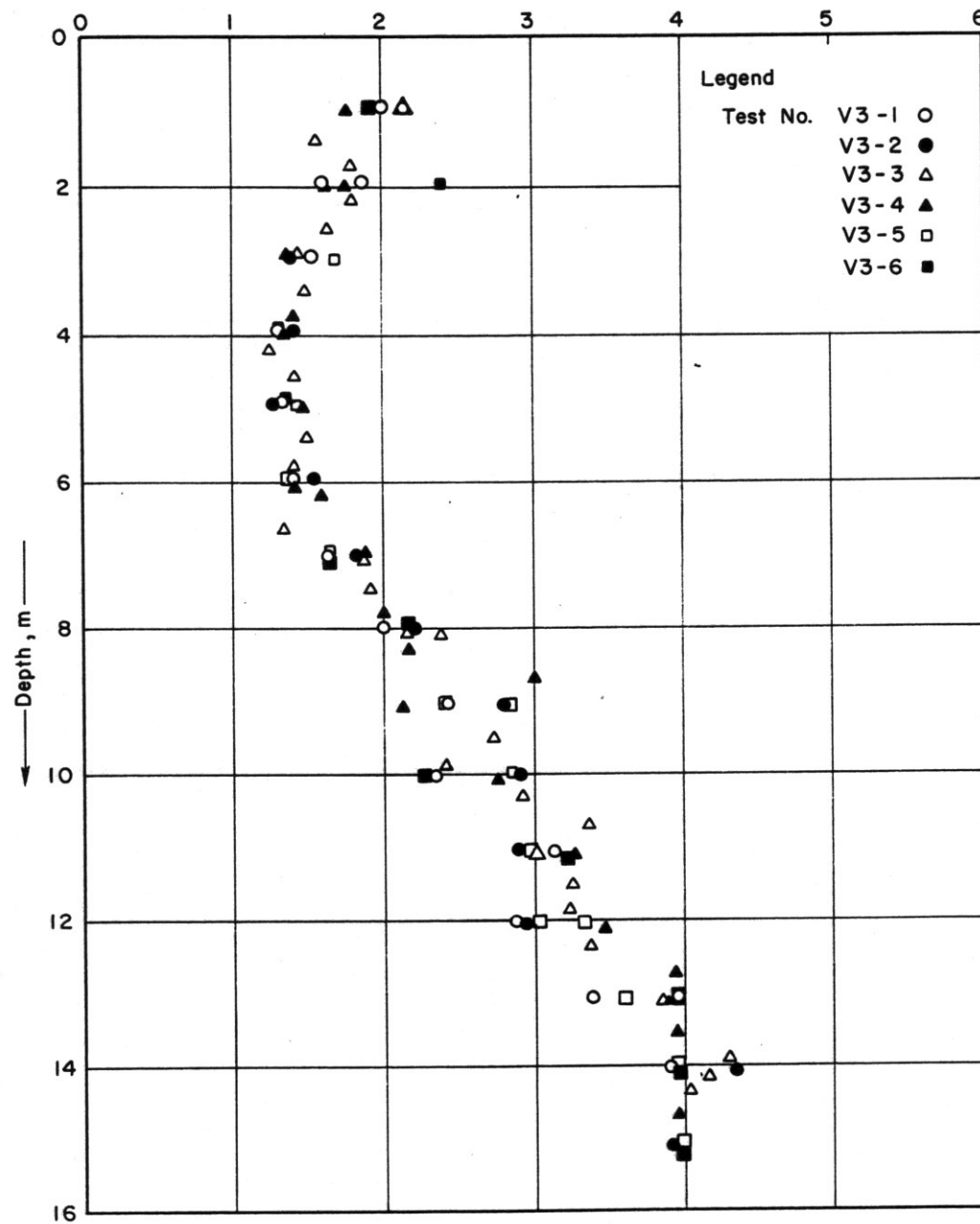


Fig. 7 Vane Strength Profile  
(Pom Prachul)



Vane Shear Strength , tons/m<sup>2</sup> ( After AIT 1973 a & b )



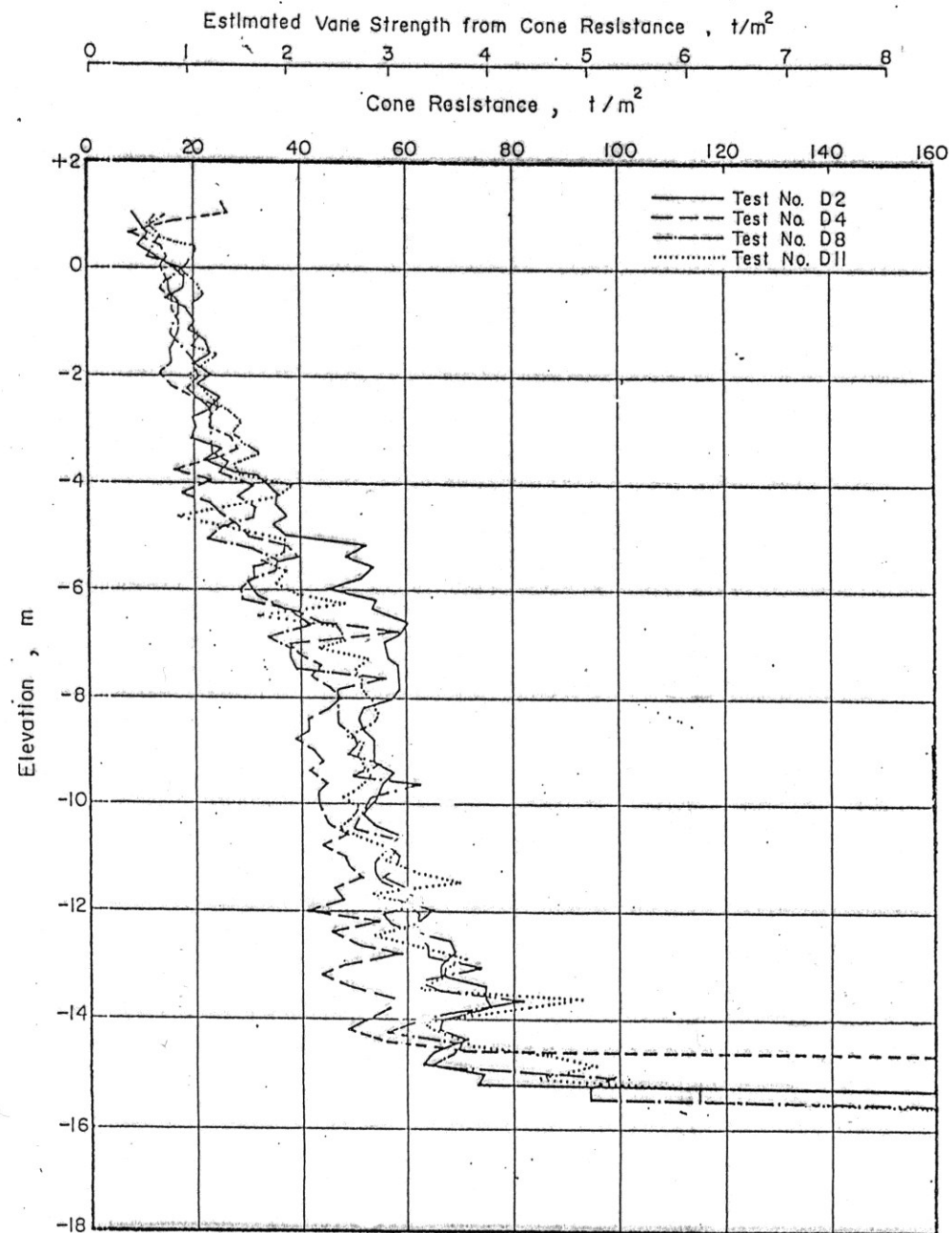


Fig. 50 Grid Line (E)-(E)

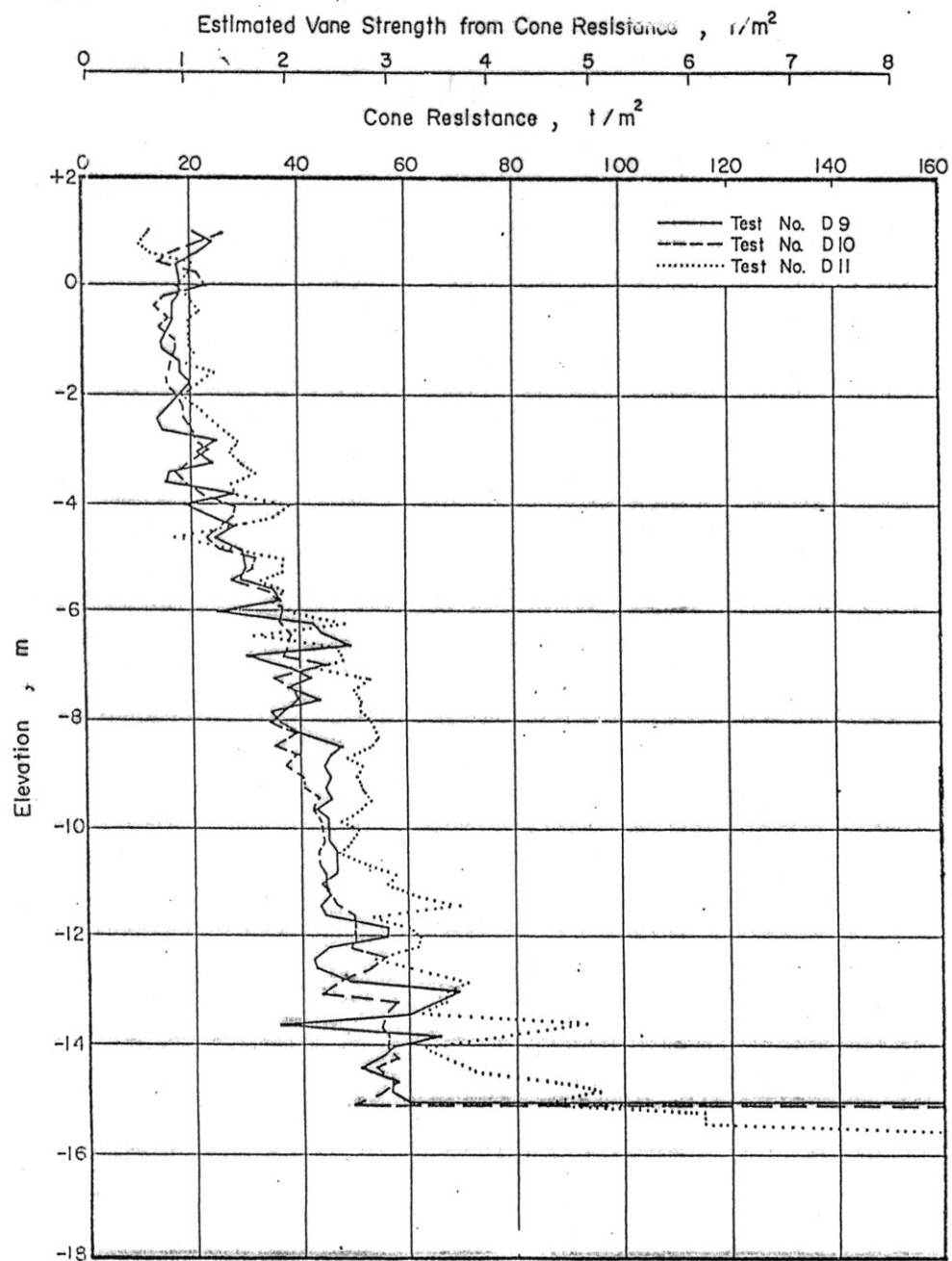


Fig. 40 Grld Line ②-②



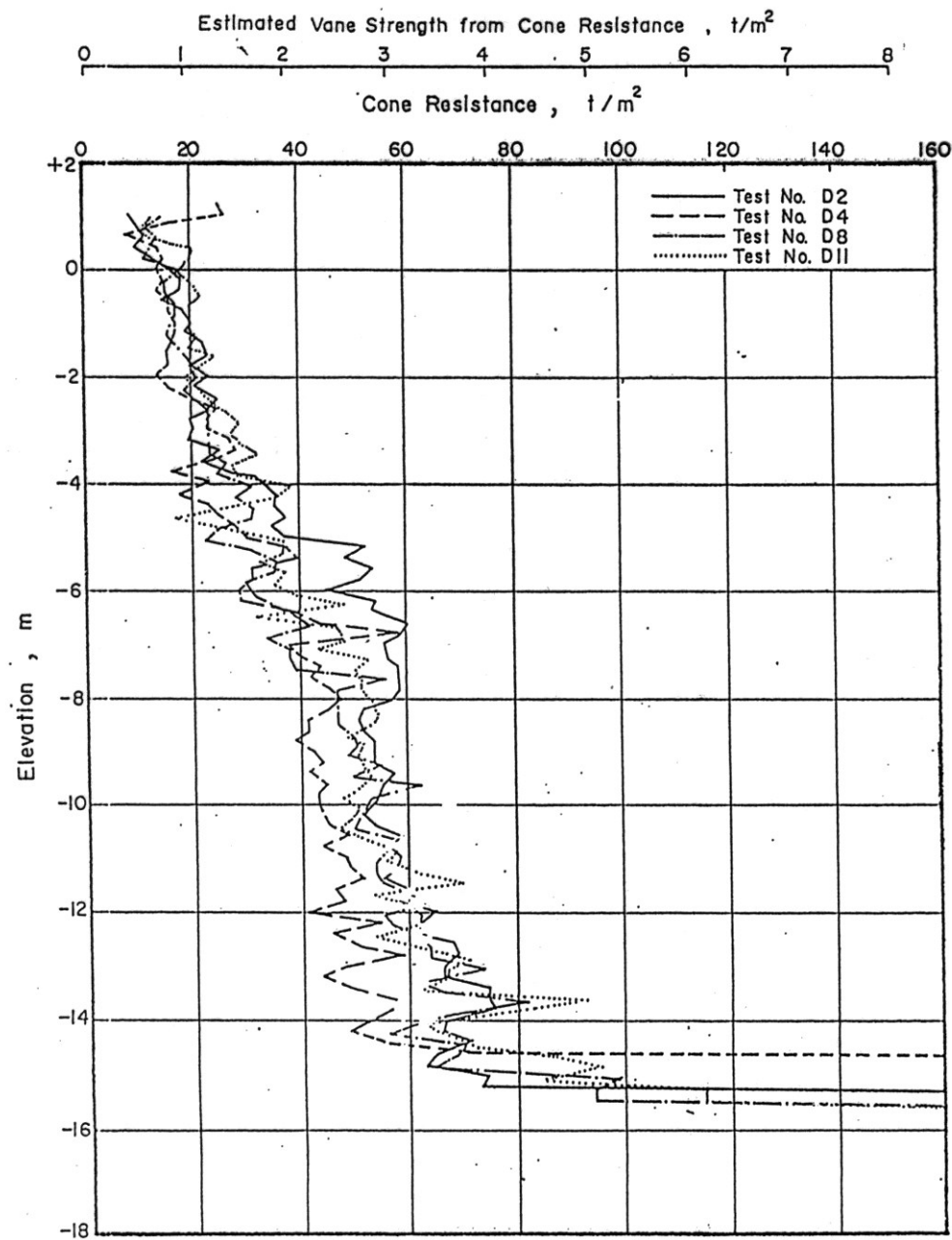


Fig. 50 Grid Line (E)-(E)

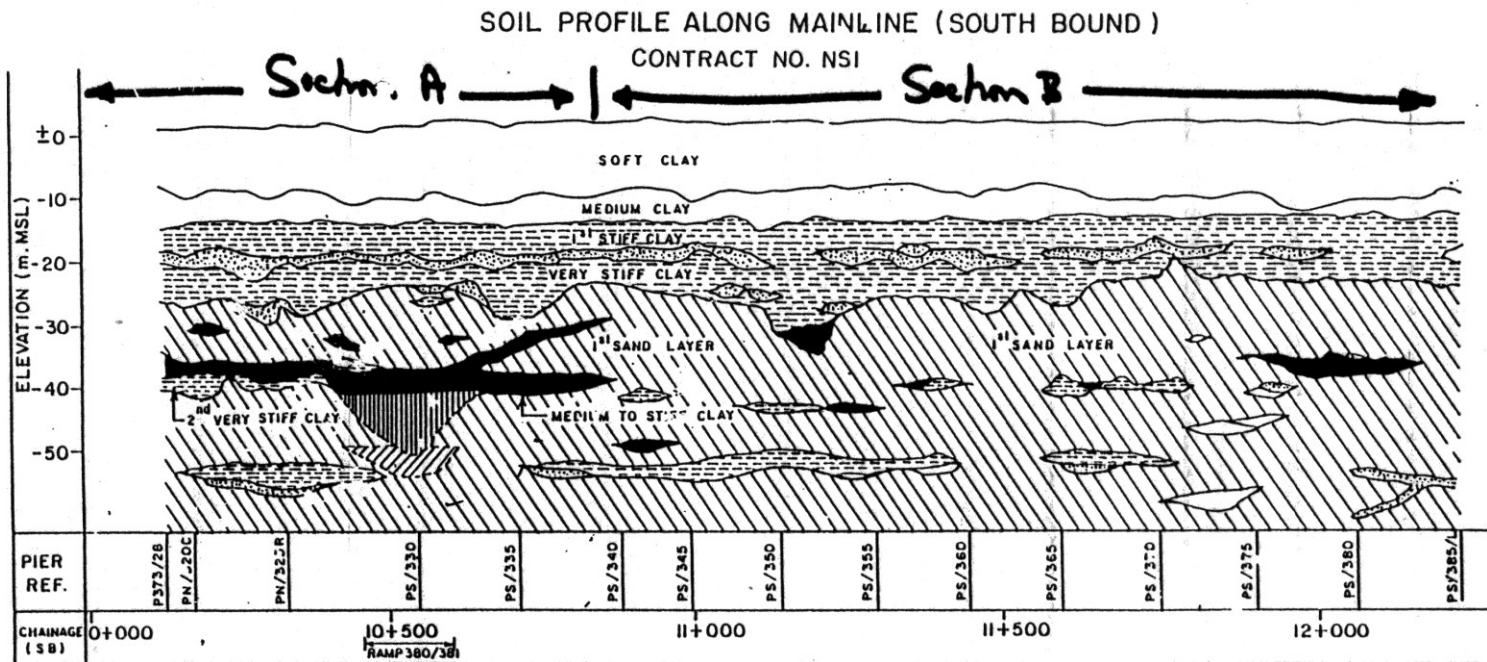








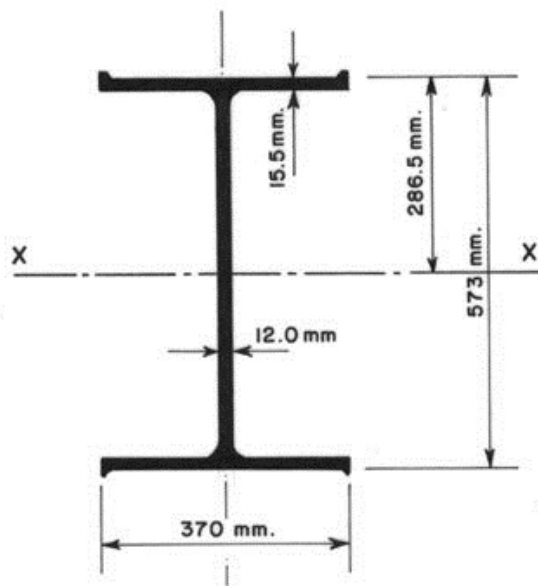




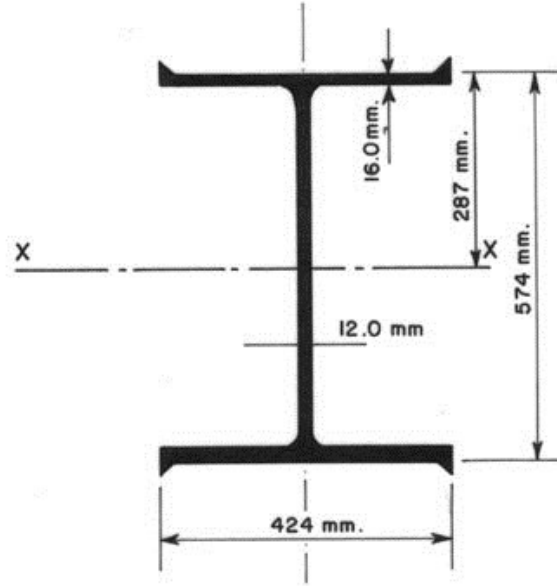
LEGEND

- VERY STIFF CLAY
- MEDIUM TO STIFF CLAY
- SAND
- CLAYEY SAND/SAIDY CLAY
- SOFT TO MEDIUM CLAY

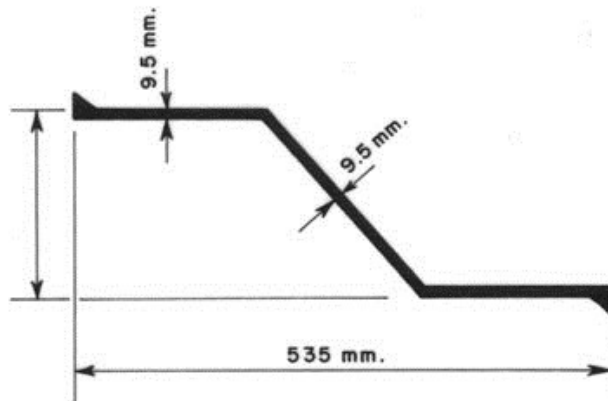
Fig. 1. Soil Profile  
(Bangkok Plain)



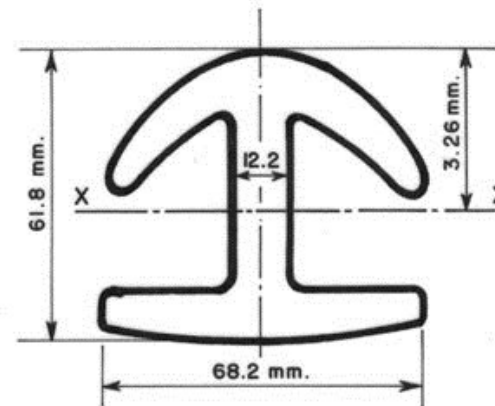
(a) King Pile HZ 600 A



(b) King Pile HZ 600 LS

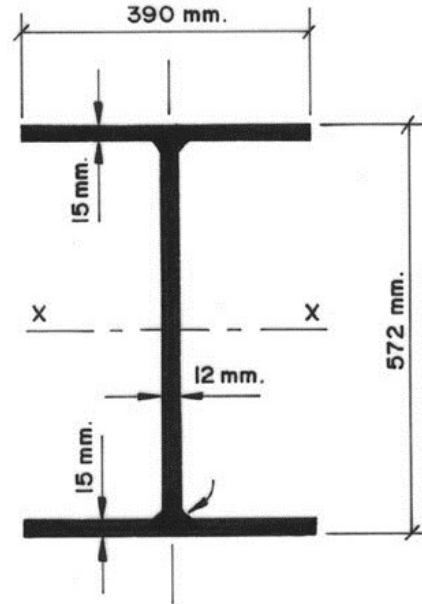


(c) Intermediary Sheet Pile BZ 9.5



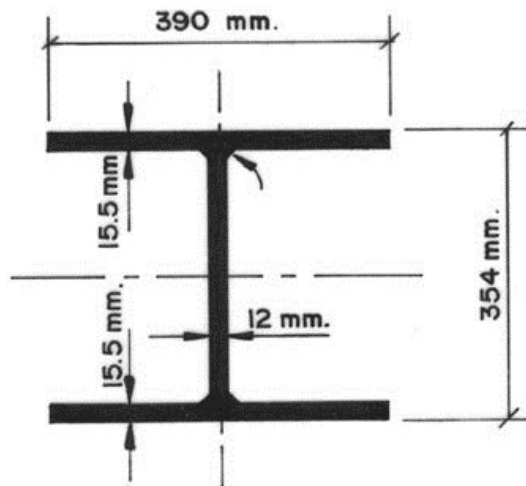
(d) Interlocking Section RH I6





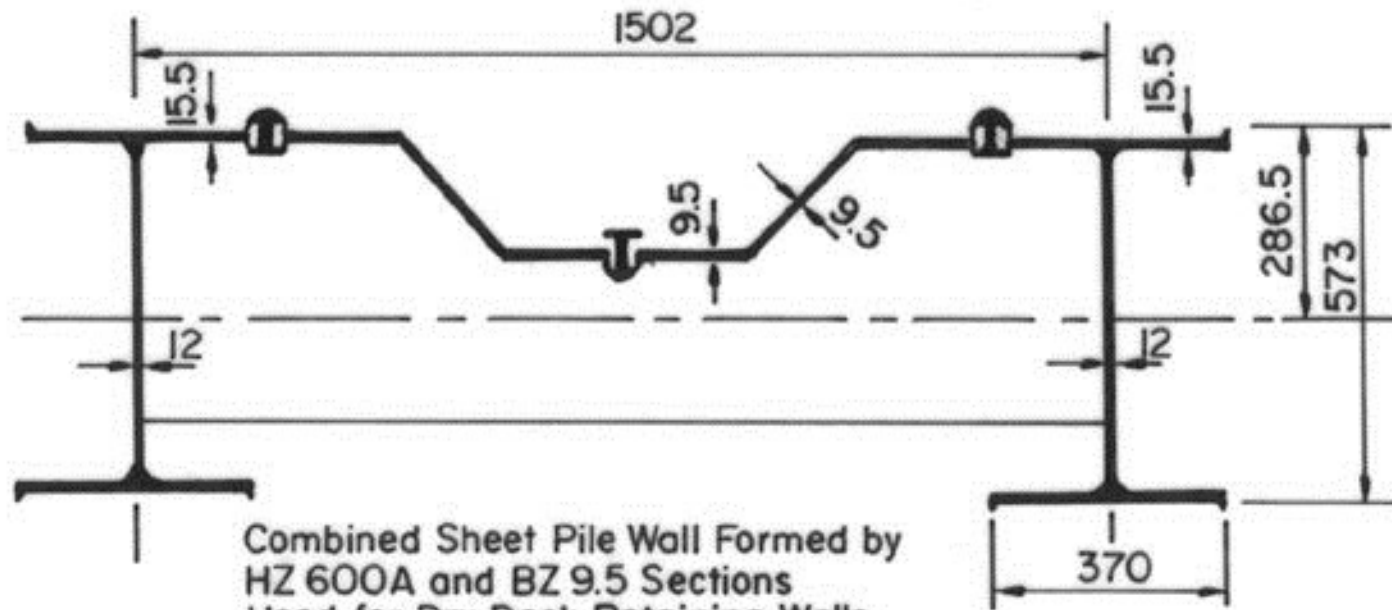
Sectional Area = 182 cm<sup>2</sup>  
 Perimeter = 263.4 cm.

Fig. 3.3 Steel Pile HZ 600 SP

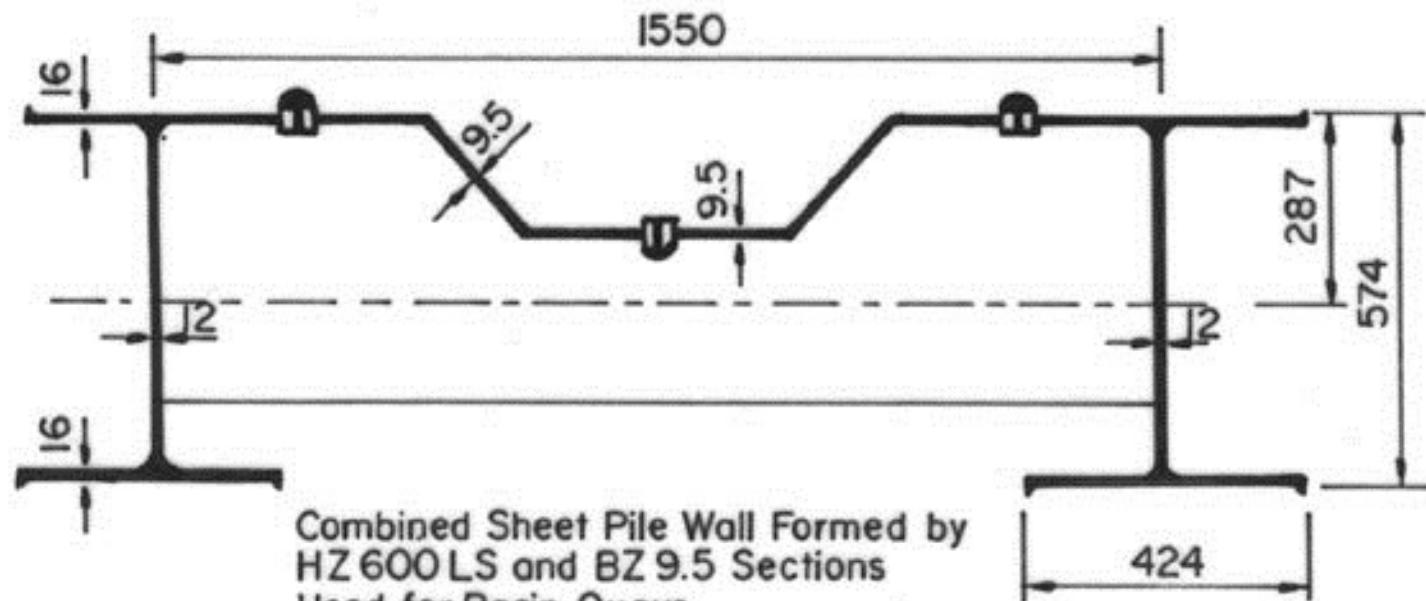


Sectional Area = 160 cm<sup>2</sup>  
 Perimeter = 219.0 cm

Fig. 3.4 Steel Pile HZ 360 SP

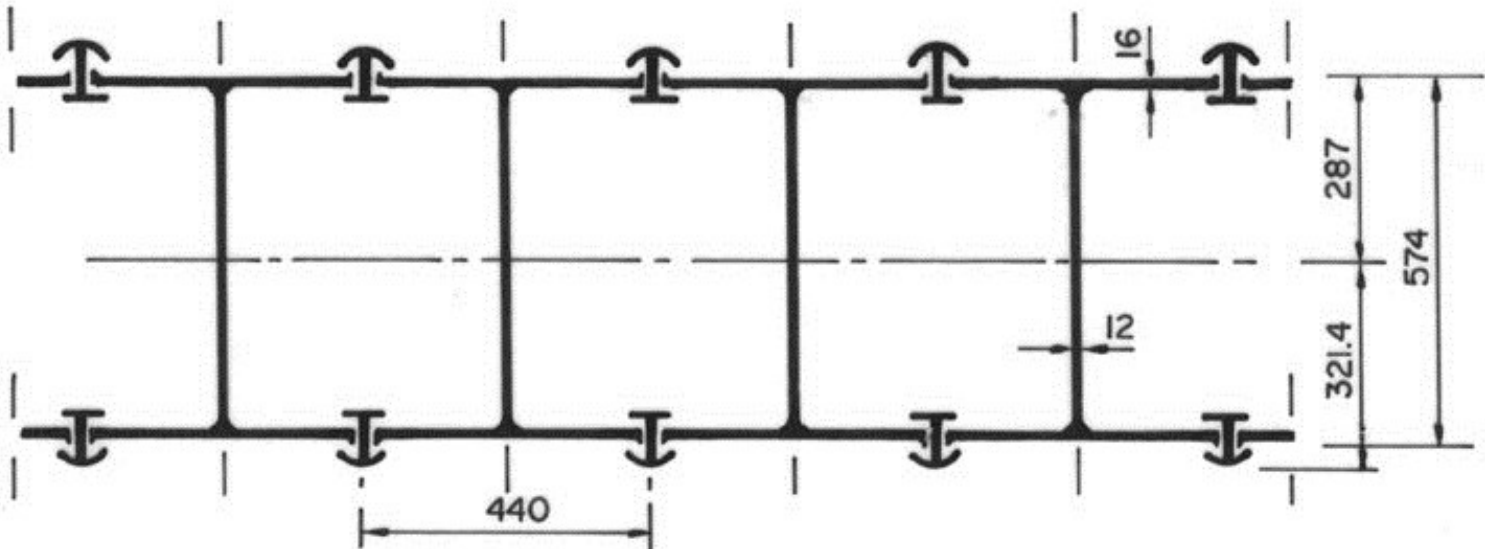


Combined Sheet Pile Wall Formed by  
HZ 600A and BZ 9.5 Sections  
Used for Dry Dock Retaining Walls  
and on riverside of East Quay

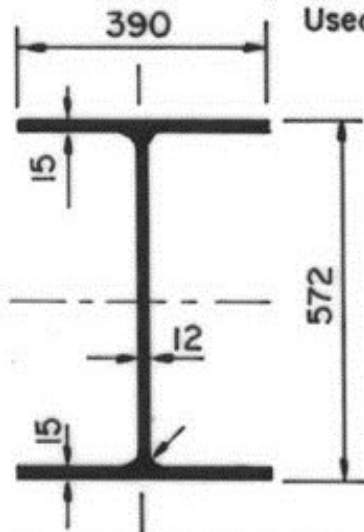


Combined Sheet Pile Wall Formed by  
HZ 600 LS and BZ 9.5 Sections  
Used for Basin Quays

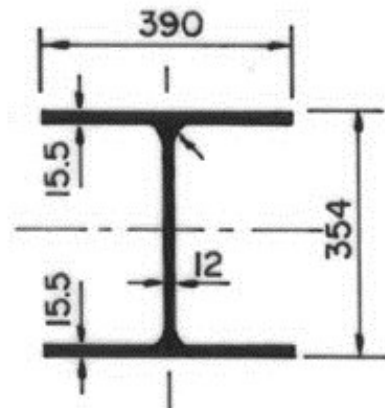




Box Pile Wall Formed by Double HZ 600 LS Sections  
Used for Basin Entrance



Steel Pile HZ 600 SP  
Used to secure Basin Entrance  
and Dry Dock floors



Steel Pile HZ 360 SP  
Used as raking piles to Anchor Beams

Note : All dimensions in millimetres  
All piles supplied by Arbed

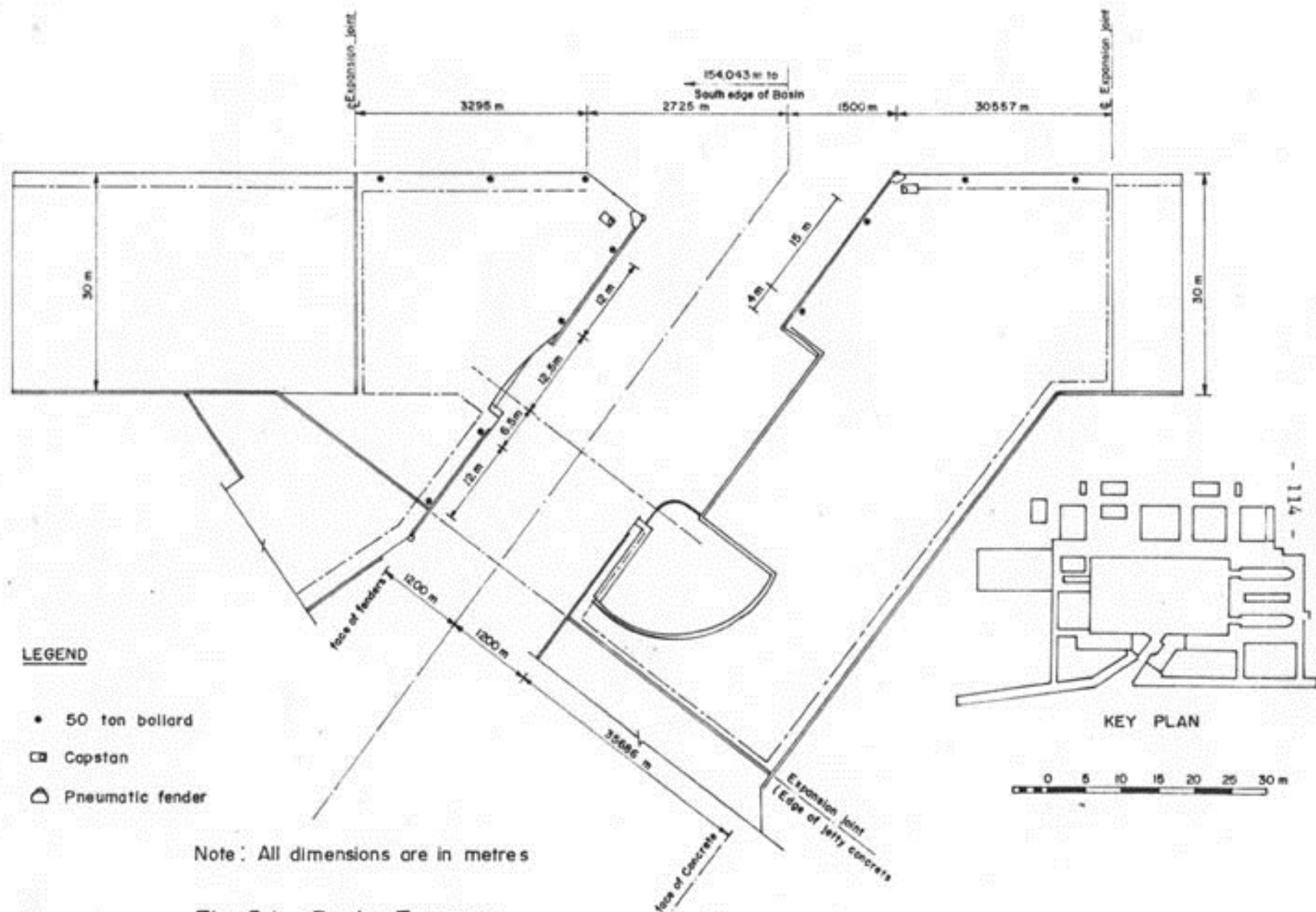
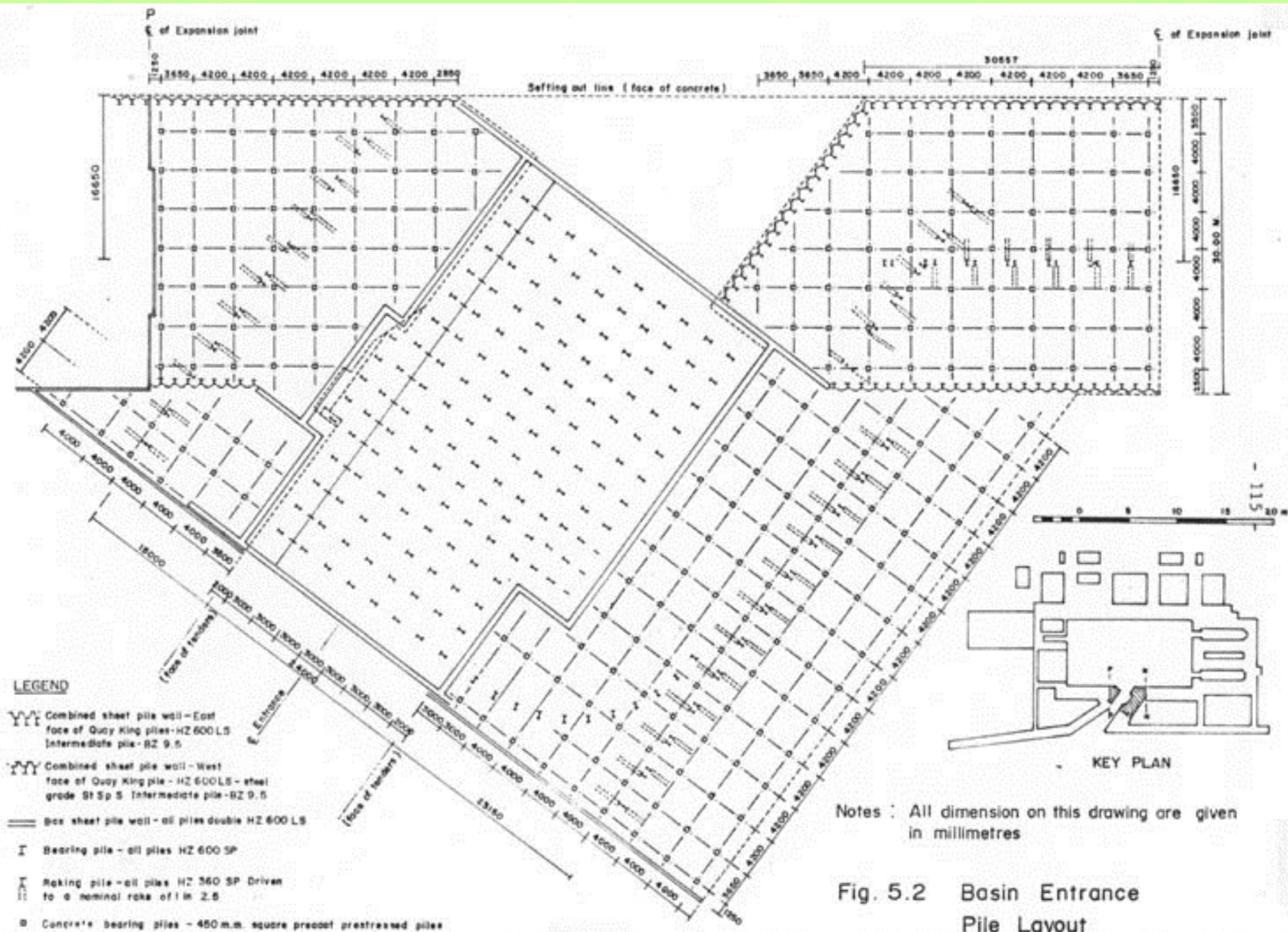


Fig. 5.1 Basin Entrance Layout Plan

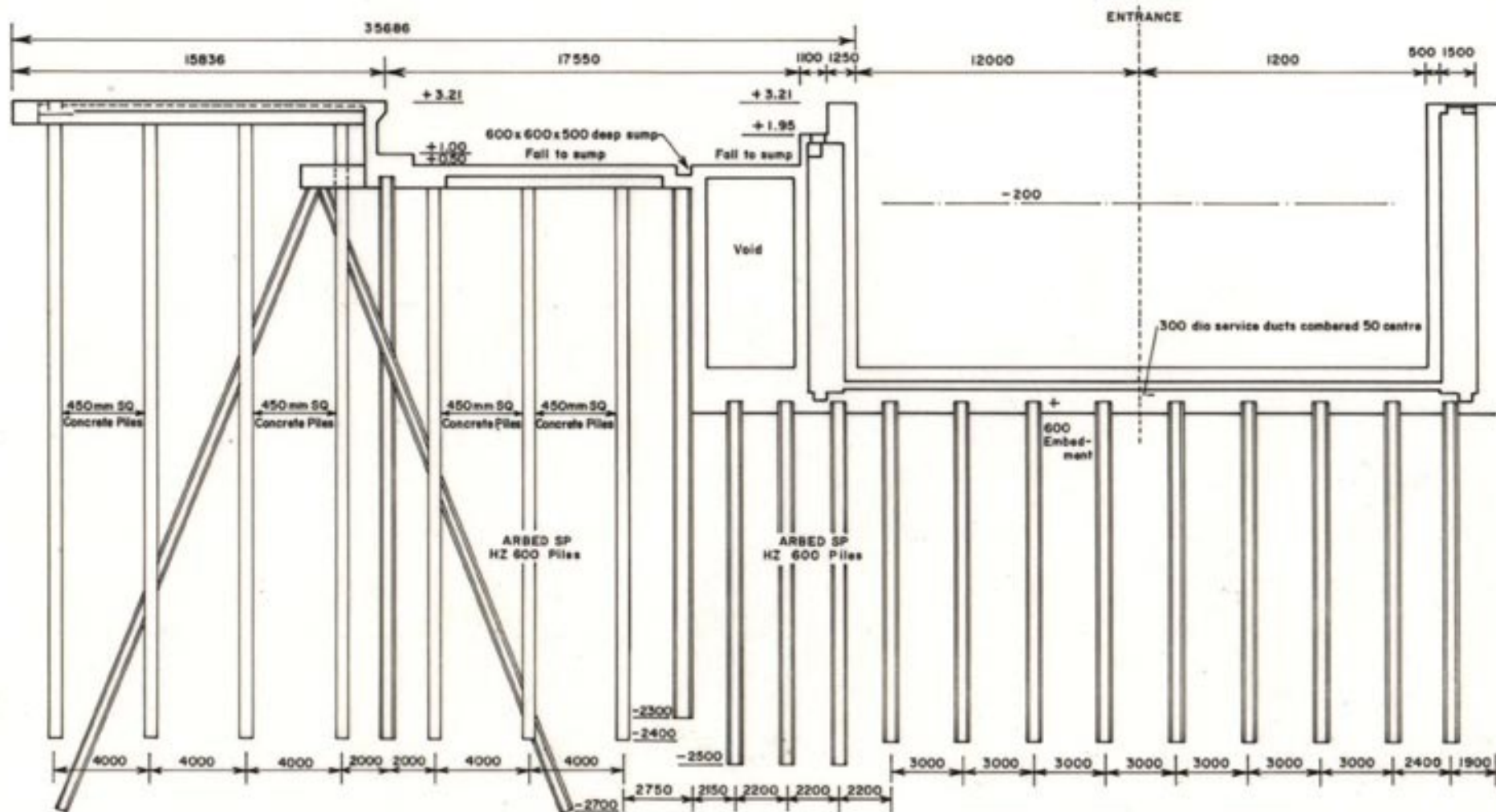






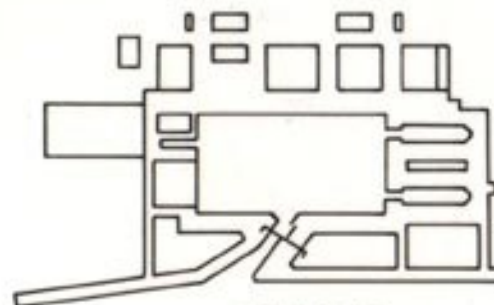




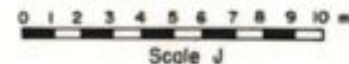


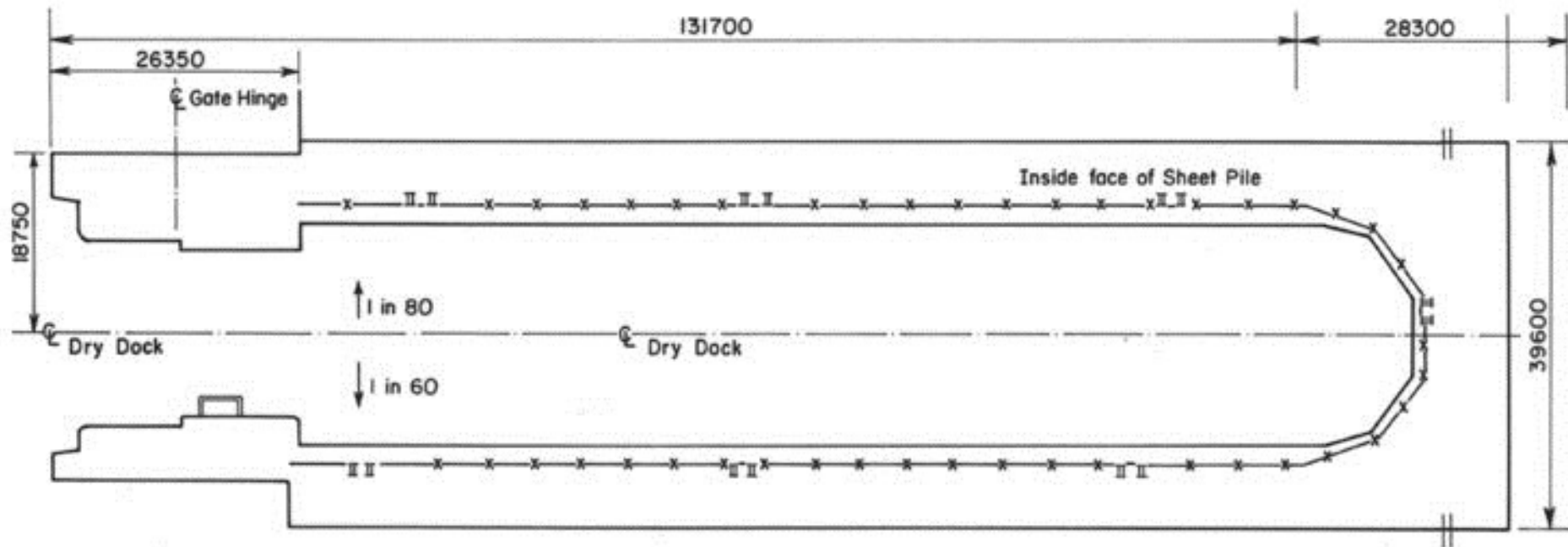
Notes : This figure to be read in conjunction with figure 5.1  
All dimensions are in millimetres  
All levels are in metres

Basin Entrance  
Main Cross Section (A-A)



KEY PLAN

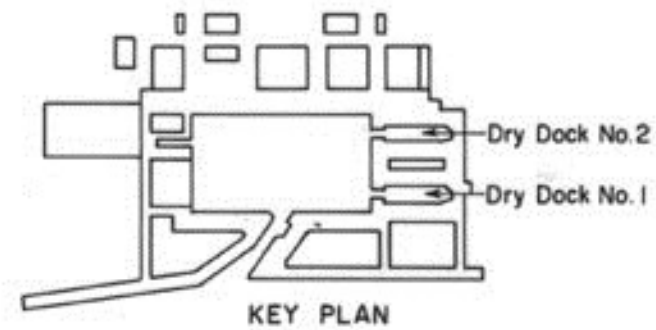




PLAN ON NO. 1 DRY DOCK

Note : All dimensions are in millimetres

Dry Docks  
Layout Plan









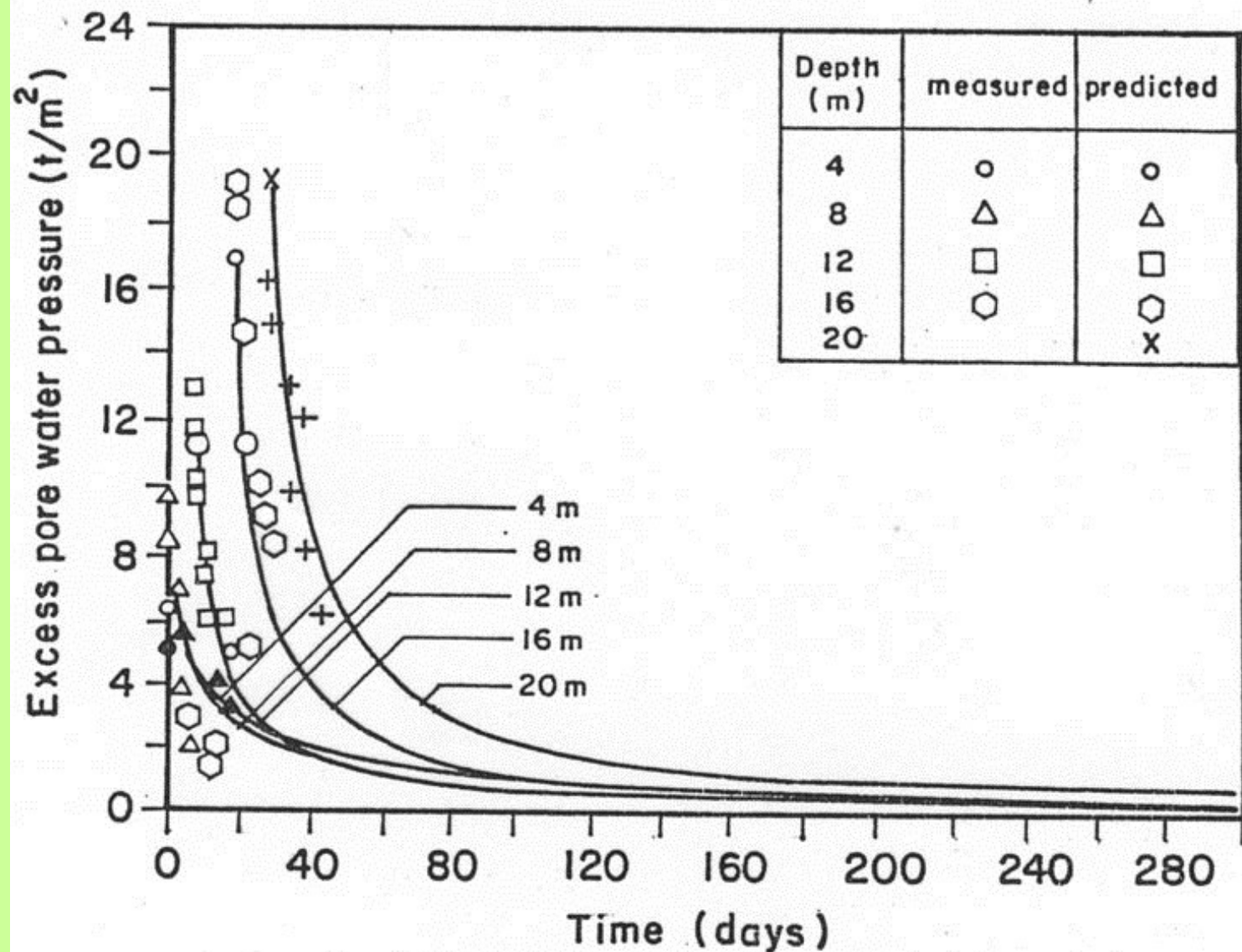






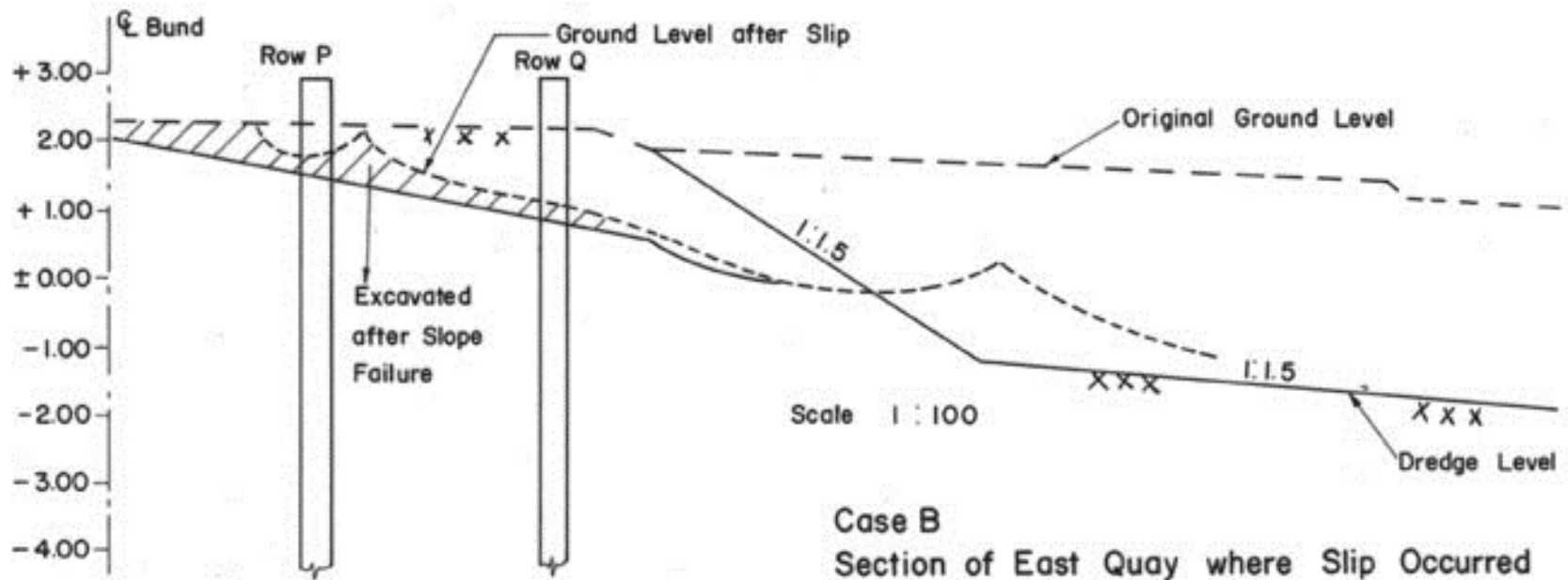
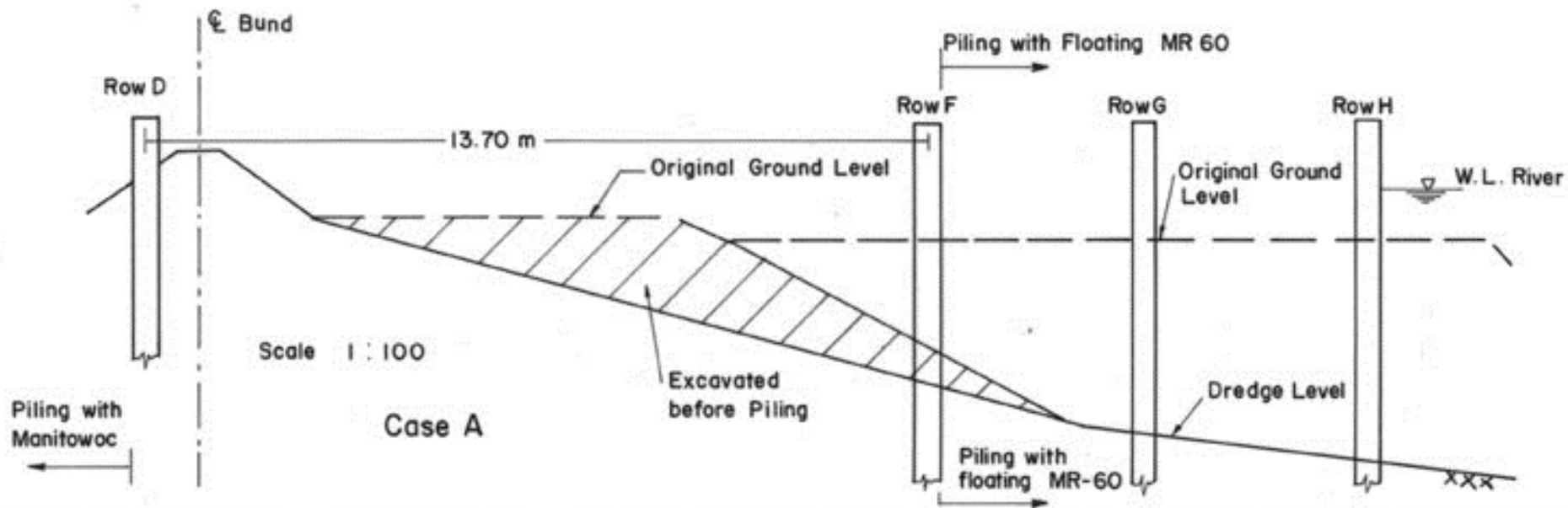


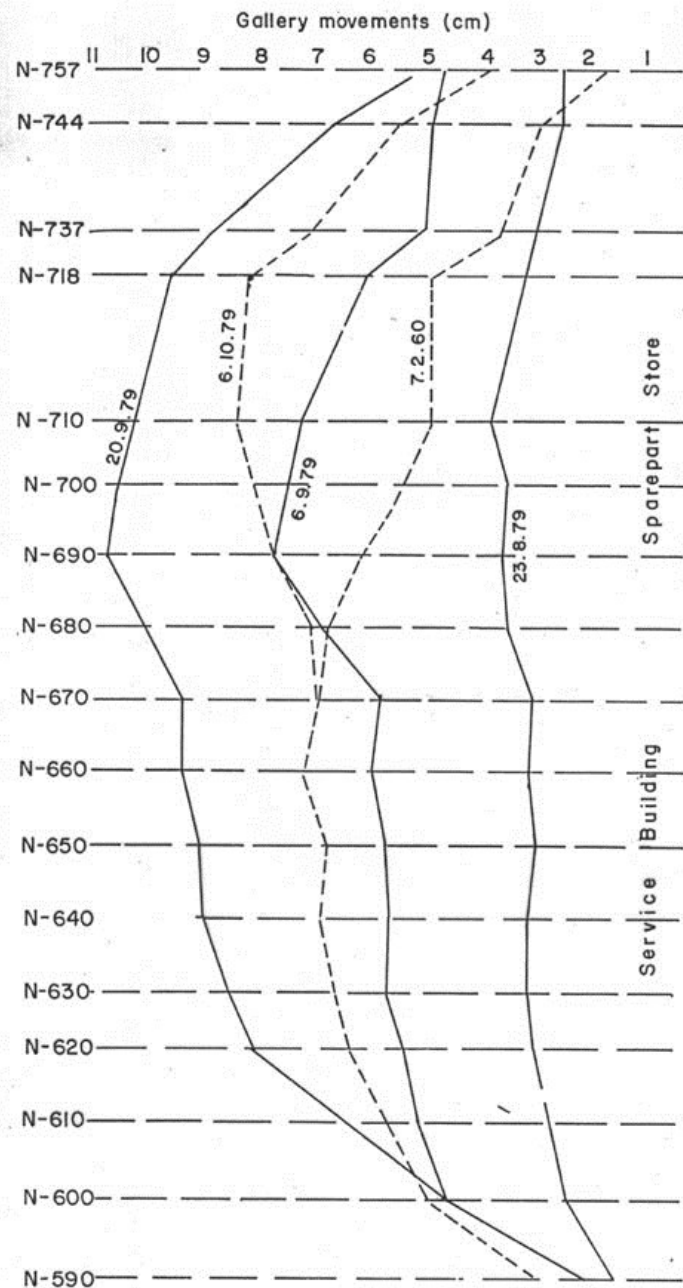




Measured and Predicted Excess Pore Water Pressure at Pile Surface







Scale :  
For Plan 1 : 750

of Sewice Gallery



Piling Sequence.

- 1) Piling on east from 20 th August to 20 September, 1979
- 2) Piling on West (Service Building) from 3rd Oct to 5 th Oct, 1979
- 3) Piling on West (Spare Parts Store) from 16th Jan to 7 th Feb, 1980

Workshop Area

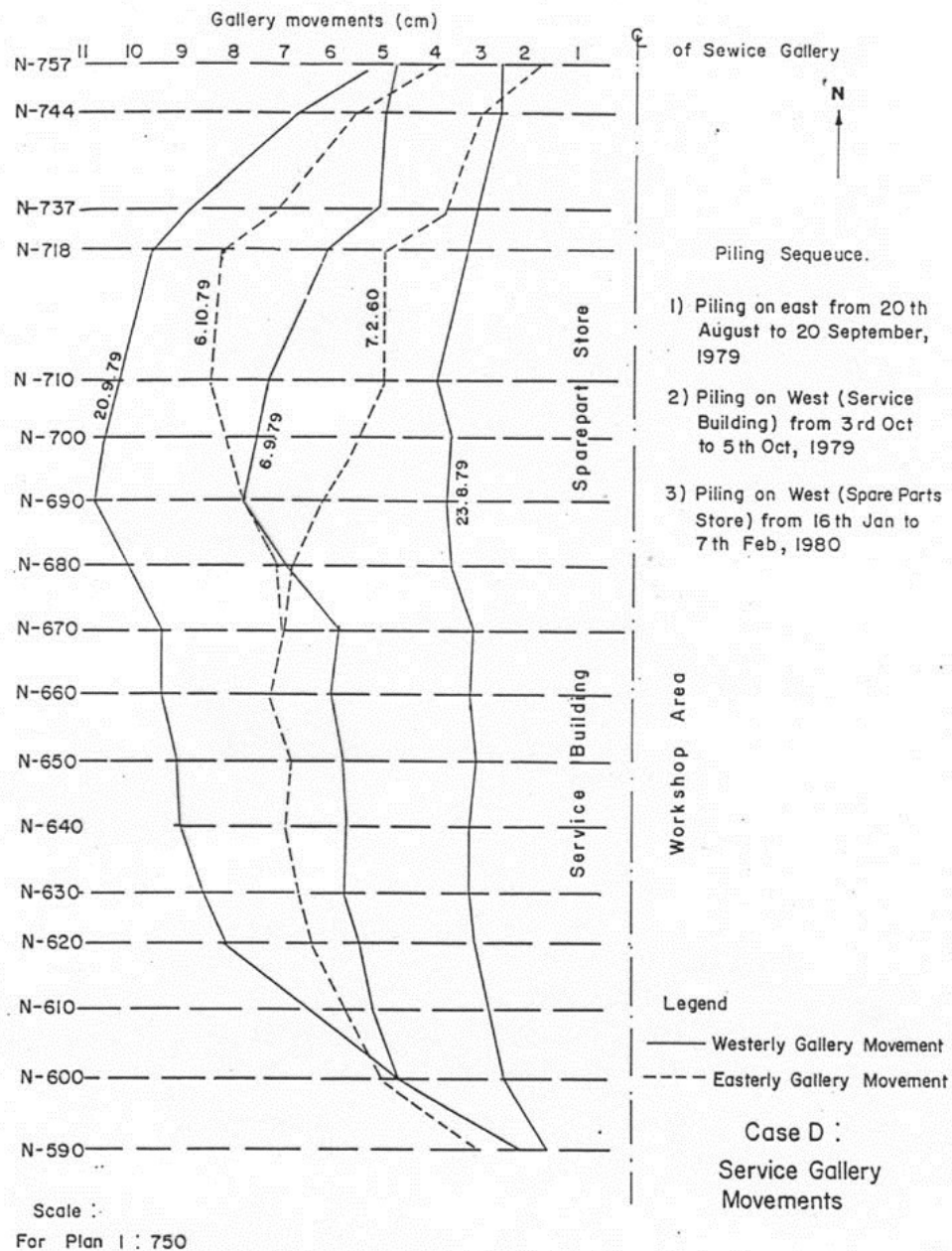
Legend

- Westerly Gallery Movement  
- - - - - Easterly Gallery Movement

Case D :  
Service Gallery  
Movements







**FIG. A.28: Service Gallery Movements**

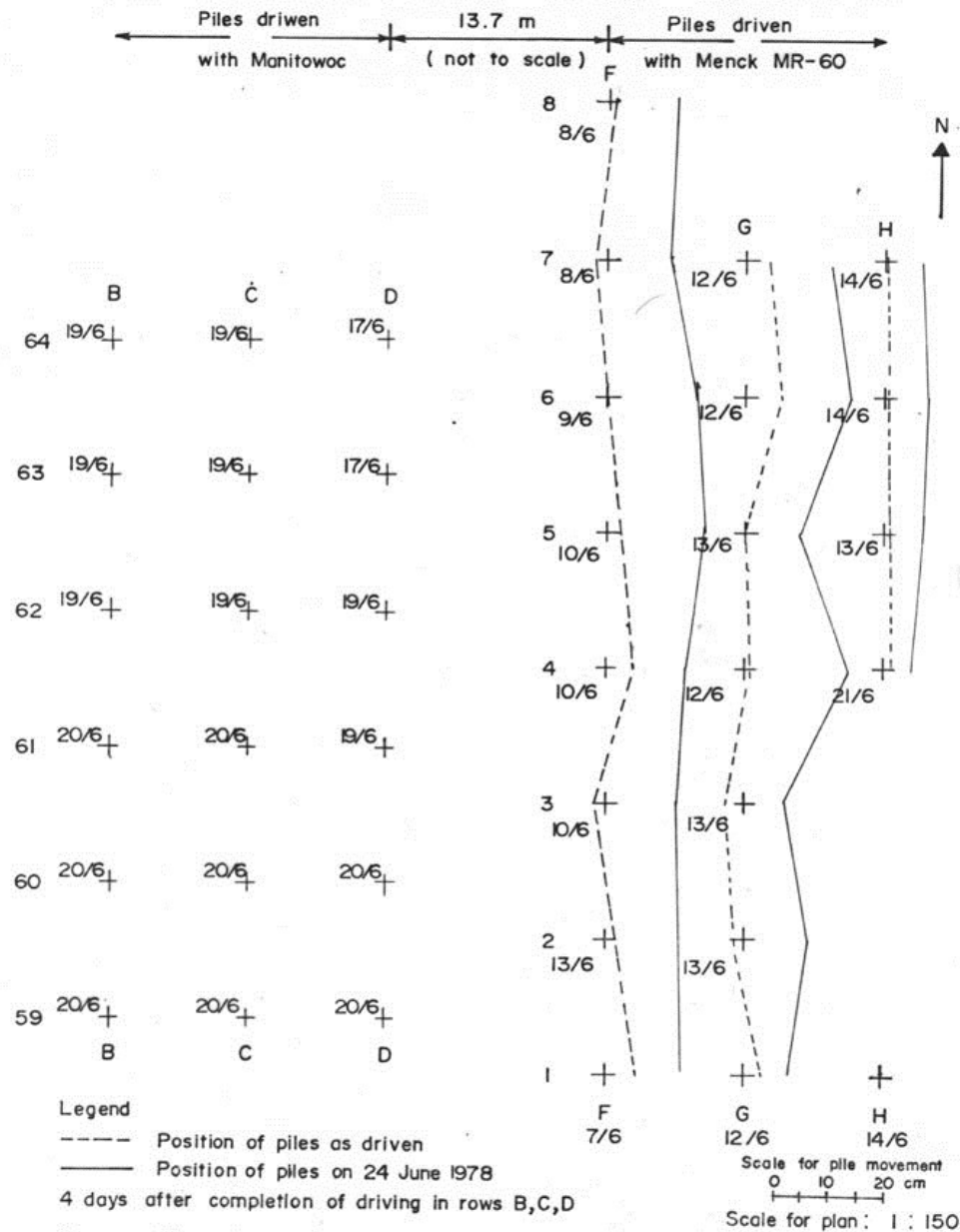
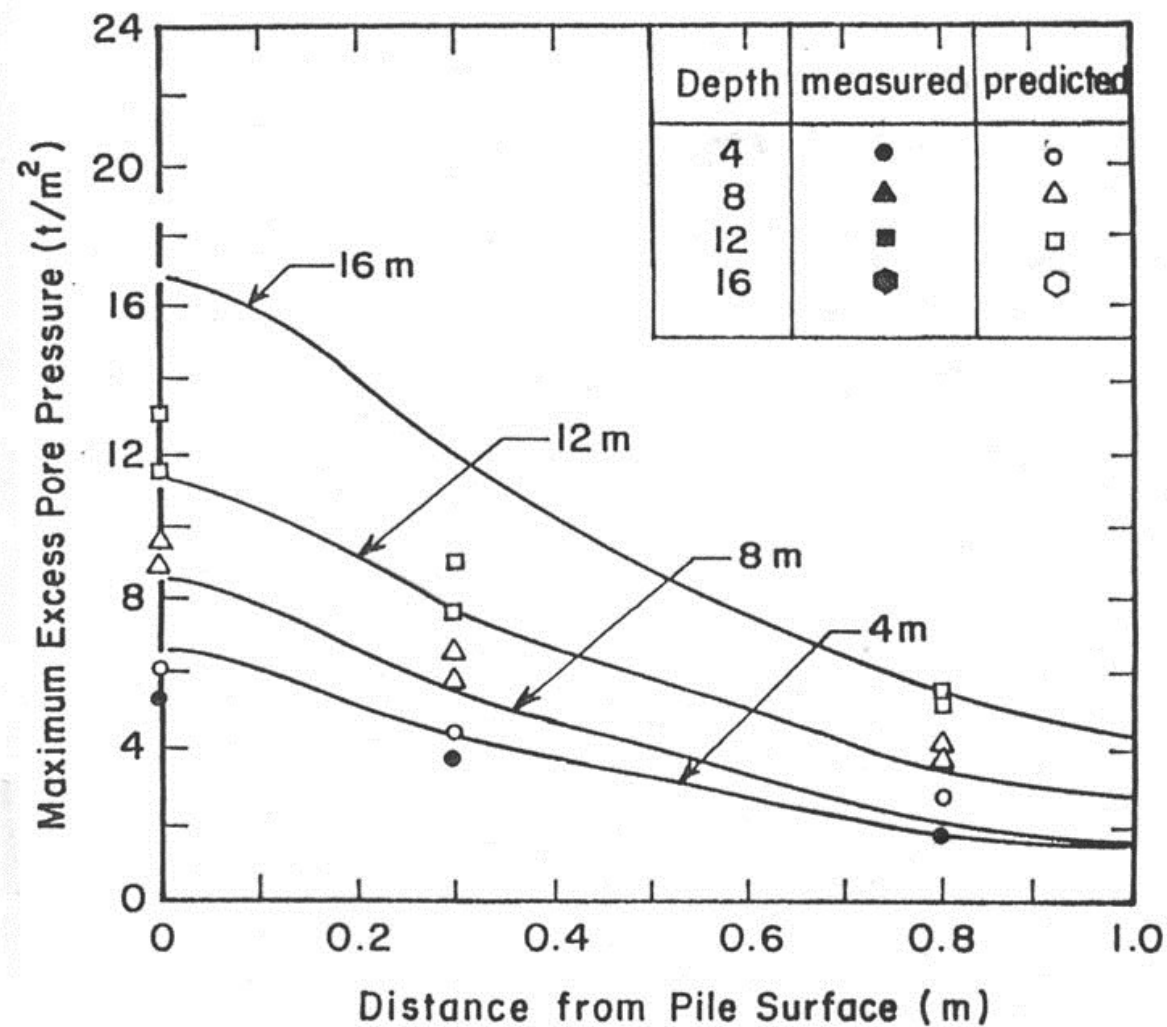


Fig. 7.3 Case A Movements of Piles in East Quay Area due to Piling in Adjacent Area





Measured and Predicted Excess  
Pore Water Pressure

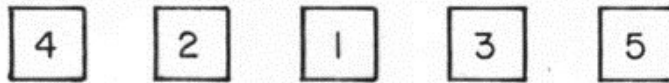


(a)

Fig.7.10 : Piling Sequences Adopted at Dockyard Site



(b)



(a)

Fig.7.11 : Alternate Piling Sequences for Reducing Pile Movements



(b)





# **Piling Practice in Sedimentary Soils-- Some Experiences**

**by**

**A.S.Balasubramaniam**

**Visiting Professor**

**Geotechnical and Transportation Engineering Division**

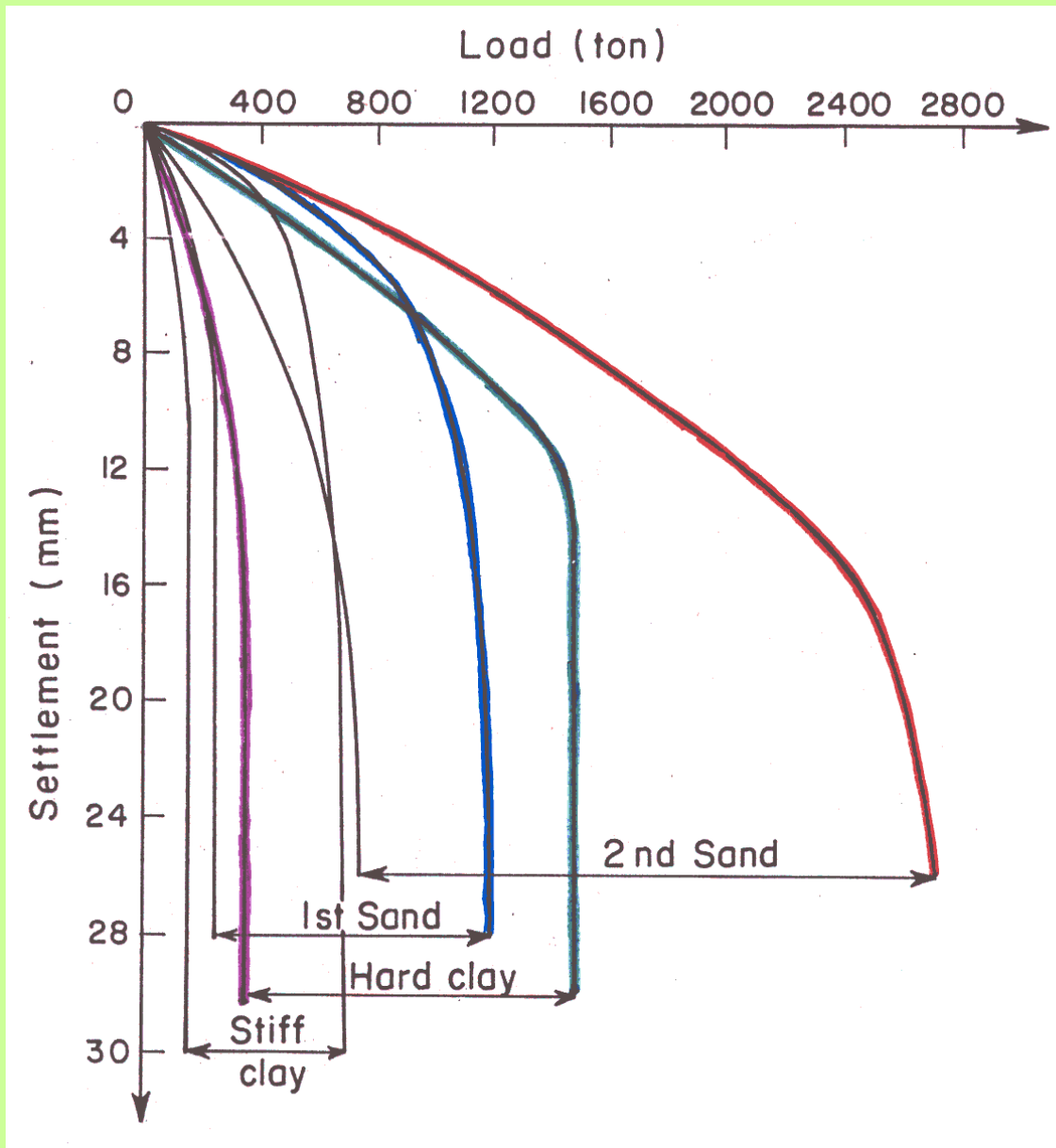
**School of civil and Environmental Engineering**

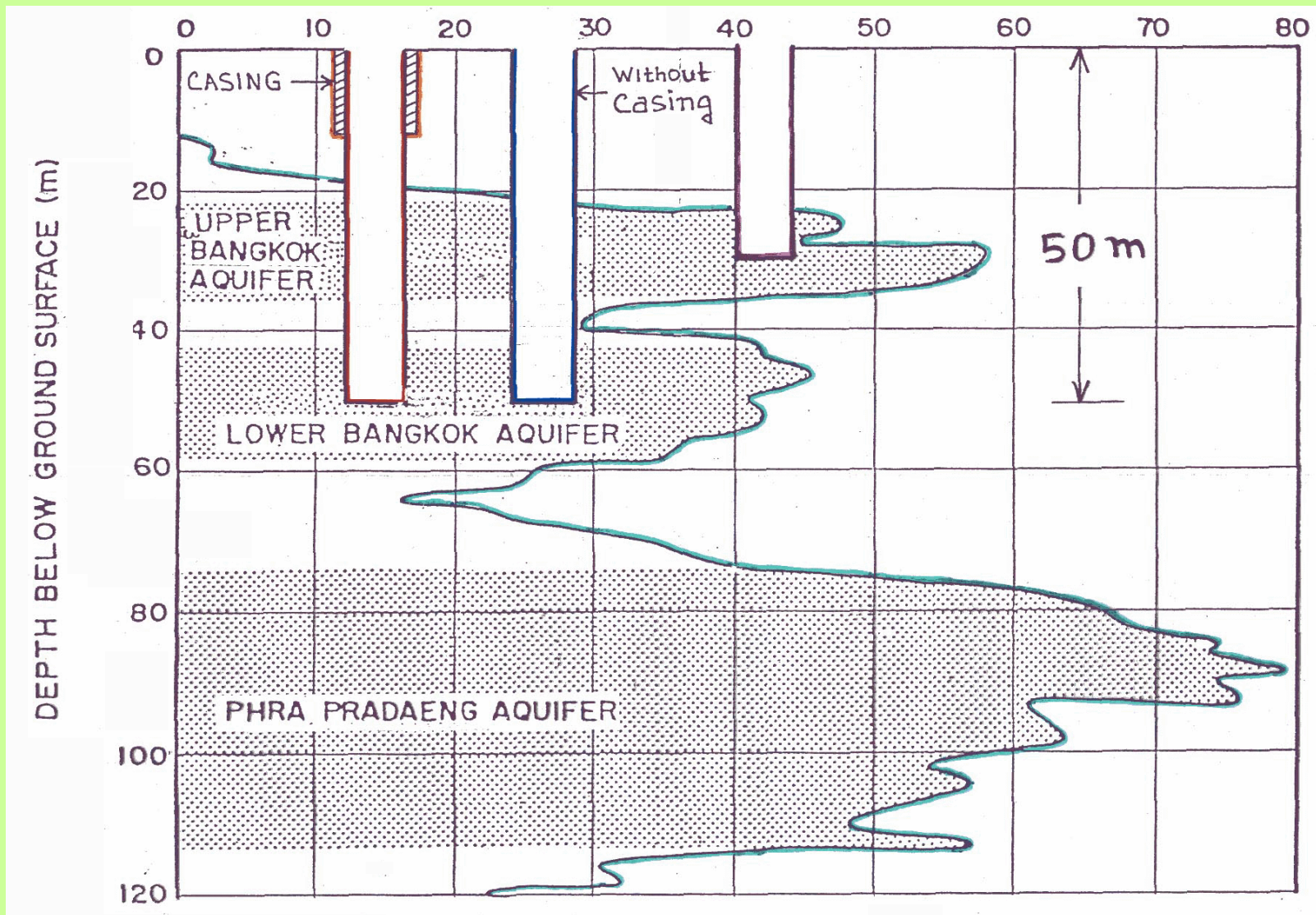
**Nanyang Technological University**

**Singapore**

**Higher load capacity with large diameter piles founded in deeper stiff layers**

**Load capacity of piles founded in different layers**





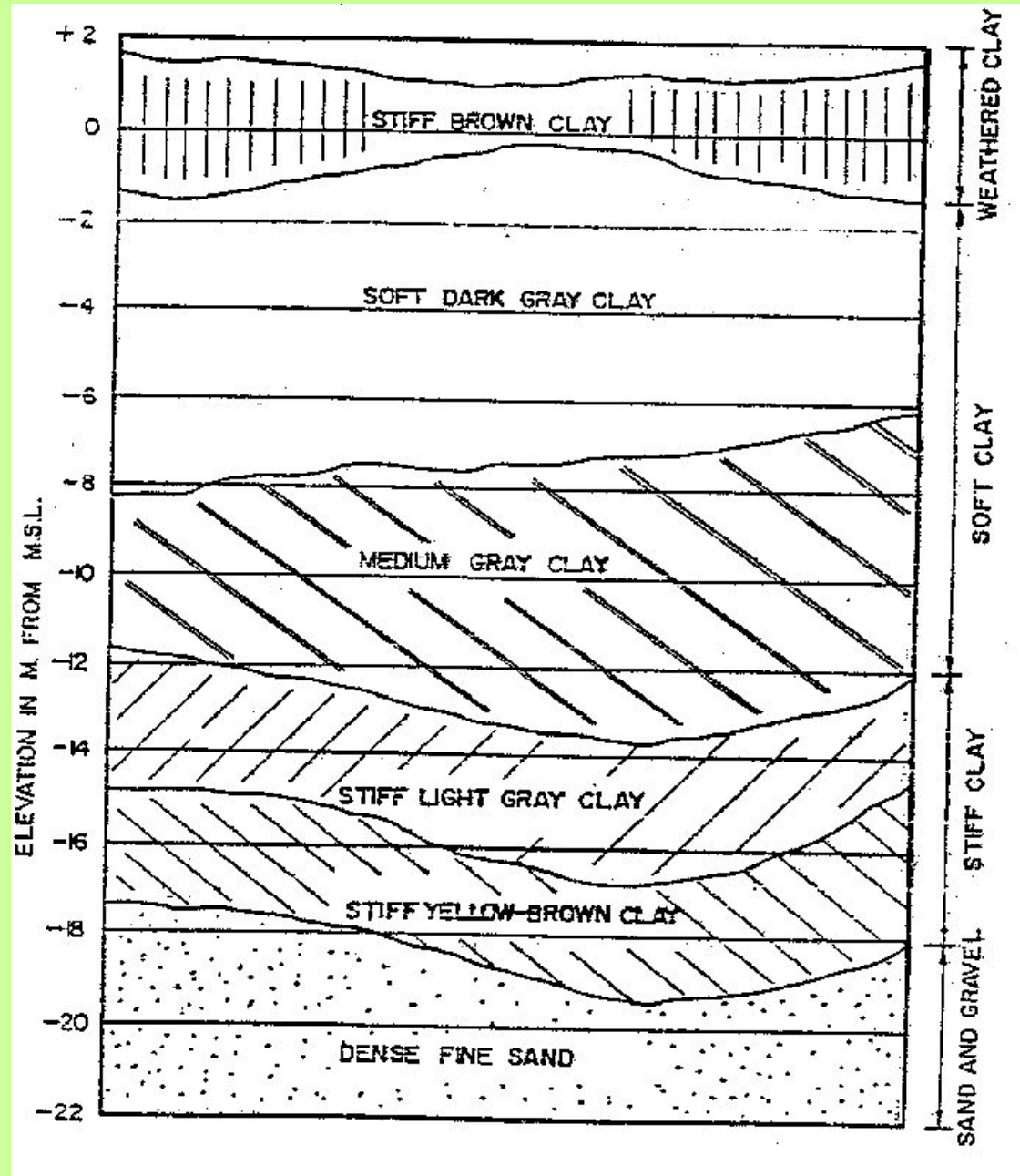
**Bored piles founded in second sand layer**



# Founding level before 1973

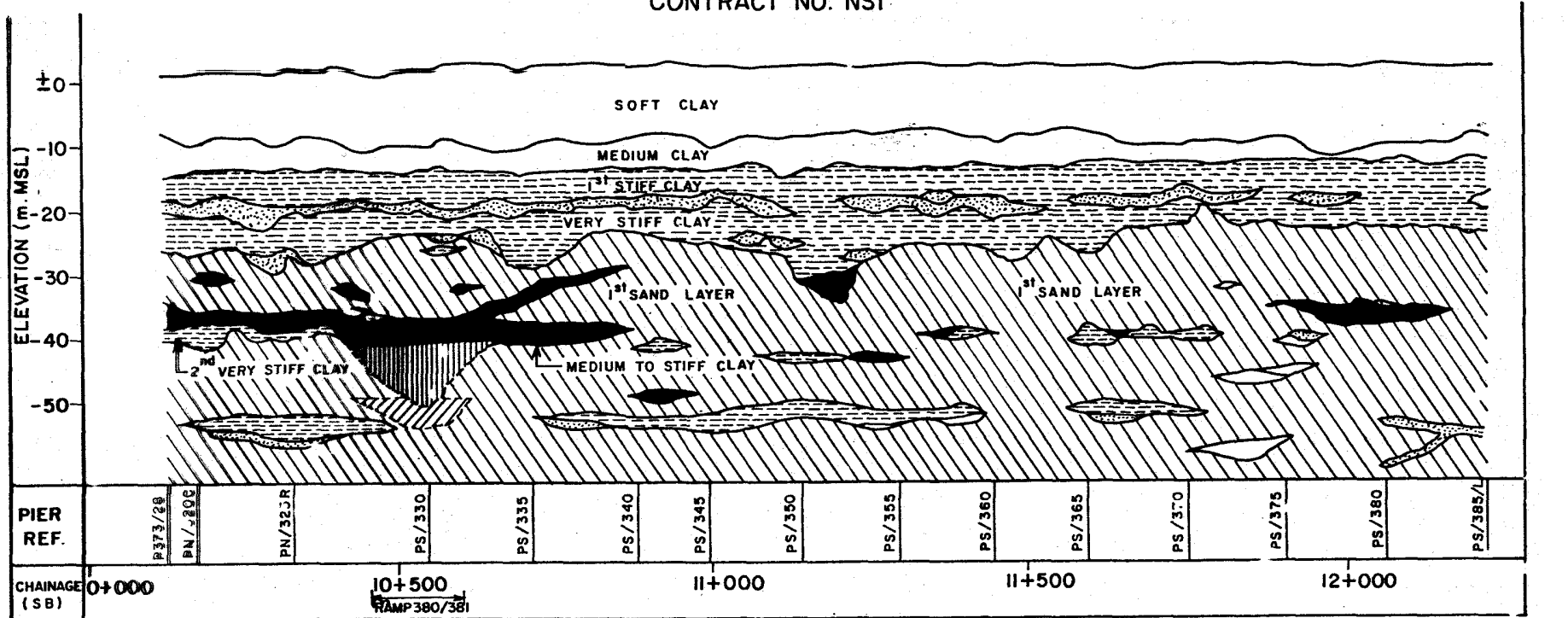
1. First stiff clay

2. First sand layer



# SOIL PROFILE ALONG MAINLINE (SOUTH BOUND)

CONTRACT NO. NSI



## LEGEND

- VERY STIFF CLAY
- MEDIUM TO STIFF CLAY
- SAND
- CLAYEY SAND/SANDY CLAY
- SOFT TO MEDIUM CLAY

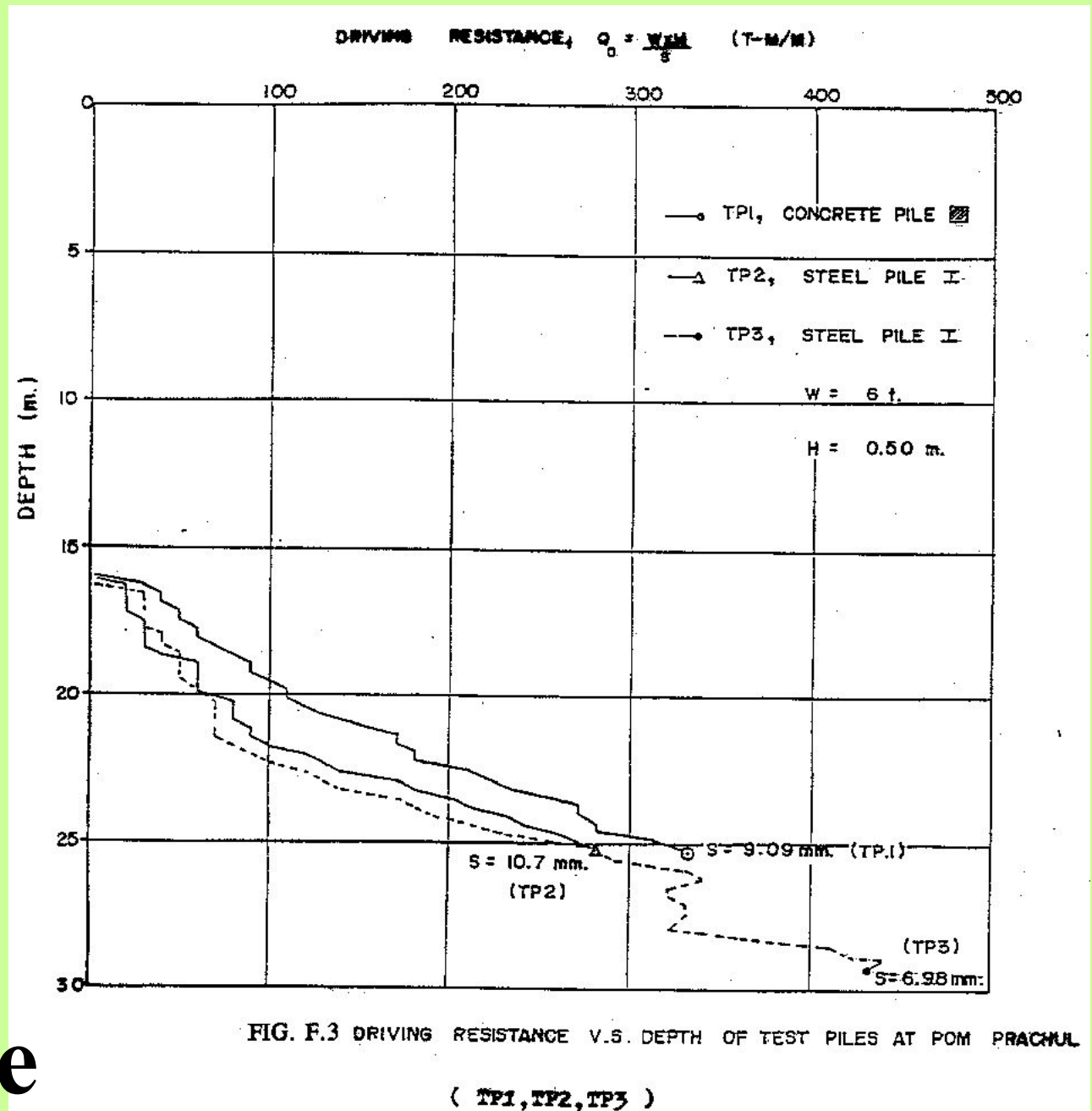
Longitudinal section of  
soil profile in the  
second stage  
expressway project

Investigator	$\alpha$				$\lambda$	
	Soft Clay	Medium Stiff Clay	Stiff Clay	Sand	Clay	sand
Pham, 1972	1.4	1.4	0.7	-	0.33	1.0
Juta-Sirivongse 1972	1.0	1.0	1.0	1.0	0.33	1.0
Chotivittaya-thanin, 1977	1.1	0.7	0.5	0.5	0.33	0.5
Phota-Yanuvat	1.0	0.7	0.5	0.8	0.33	0.5
Chukiat Phota-Yanuvat, 1979	1.0	0.7	0.5	0.8	0.33	0.5

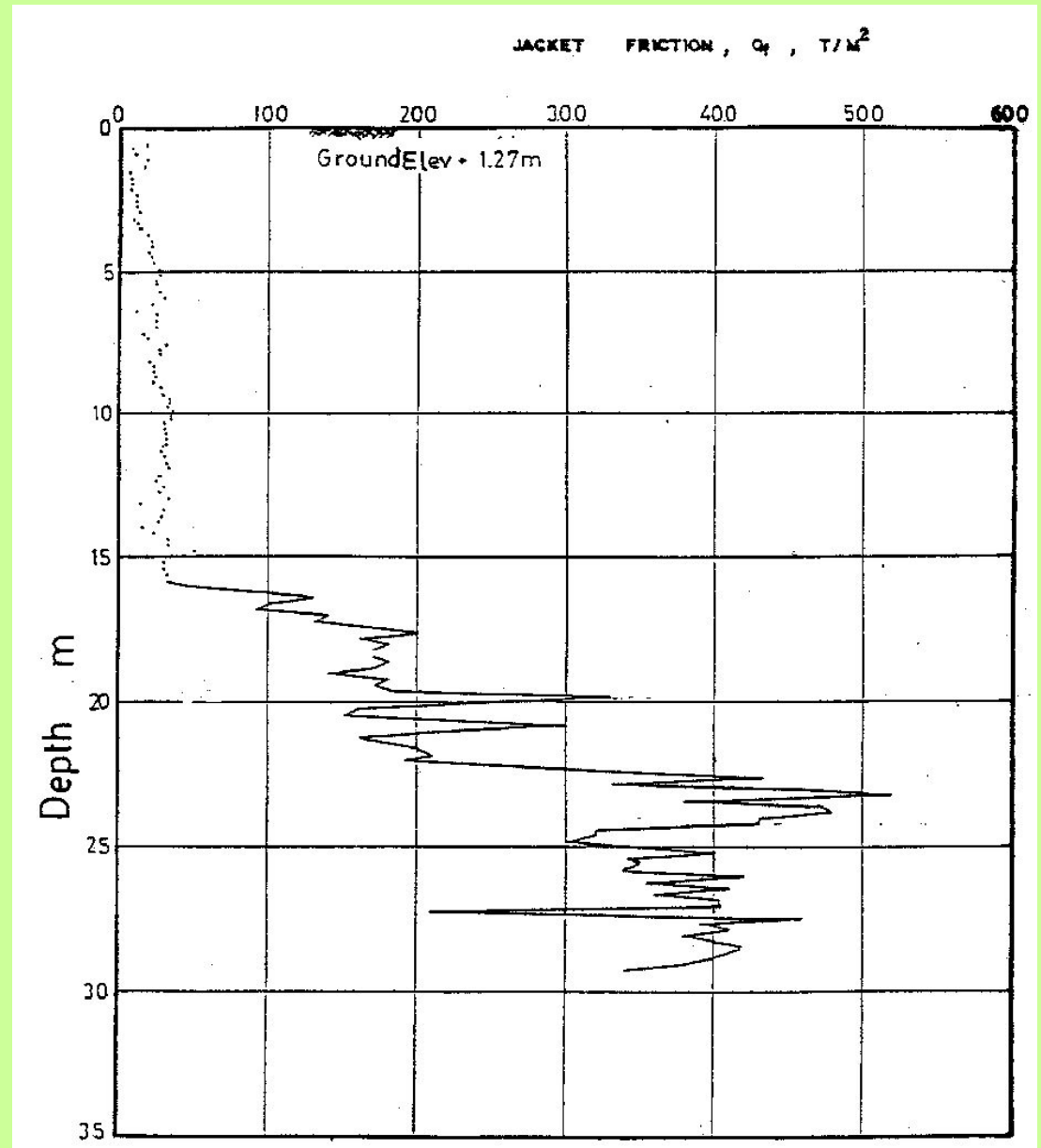
**Friction and end bearing factors for driven piles to be used with cone penetration test data**



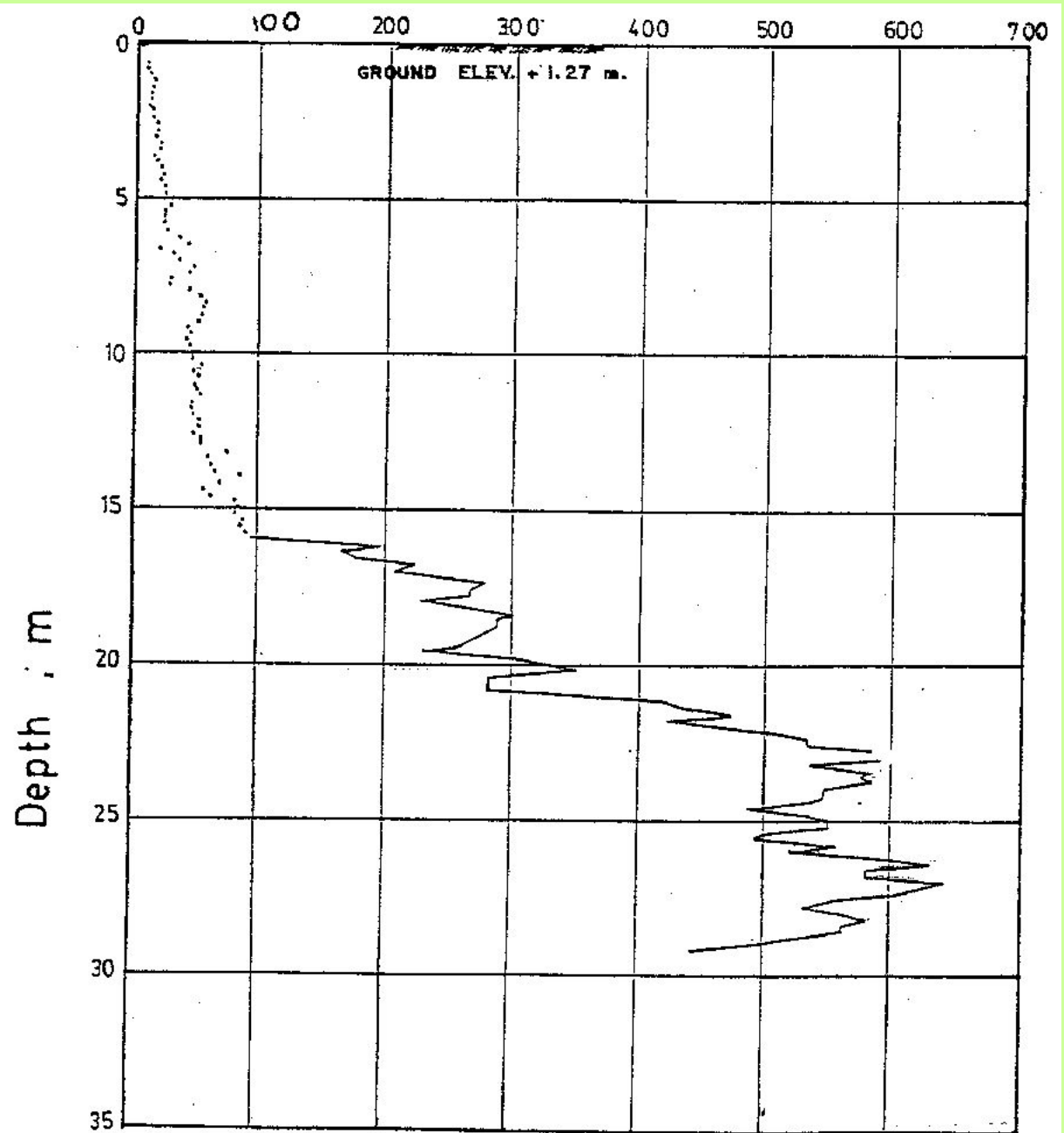
# Pile Driving Resistance



# Jacket friction in Cone penetration test

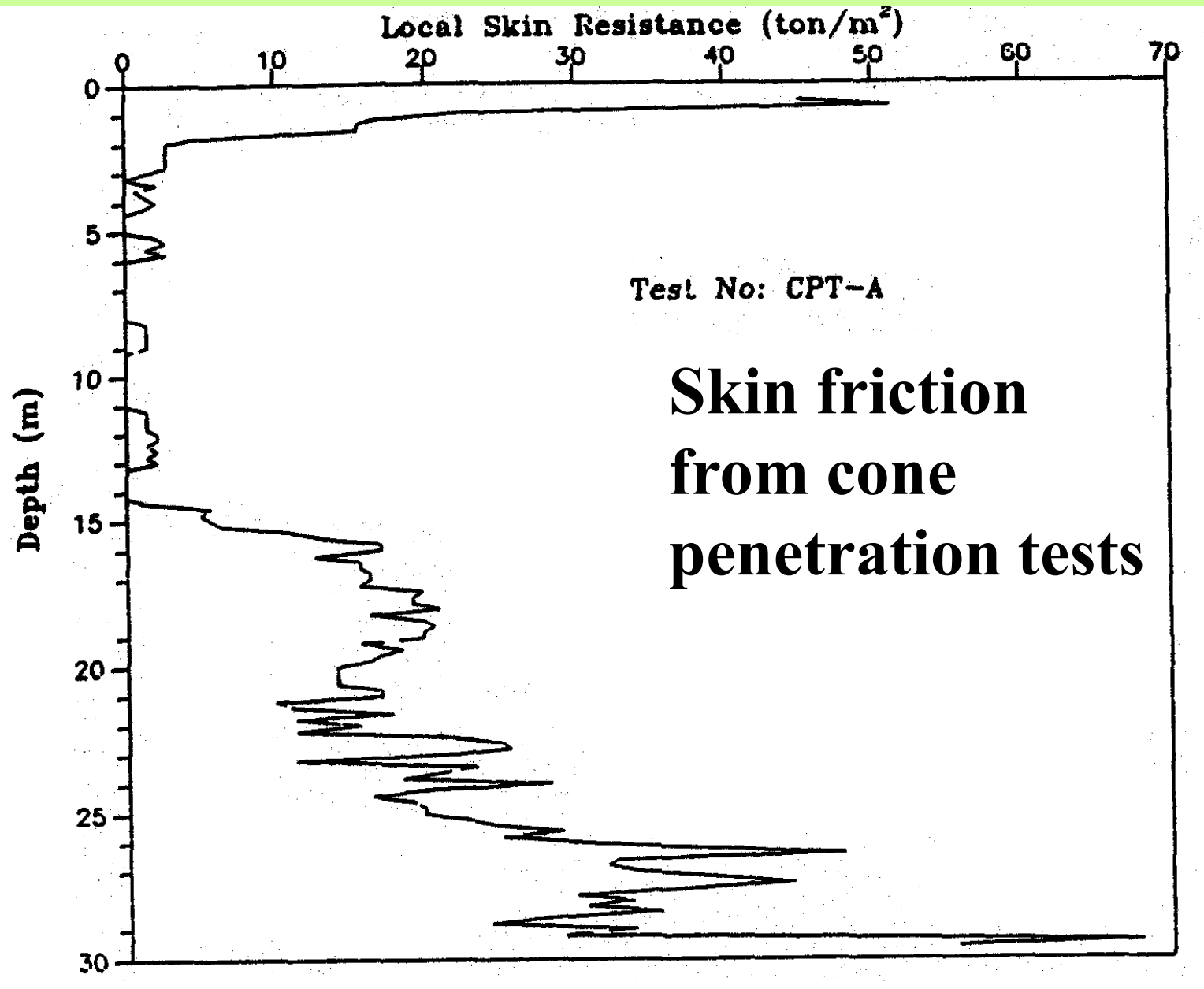


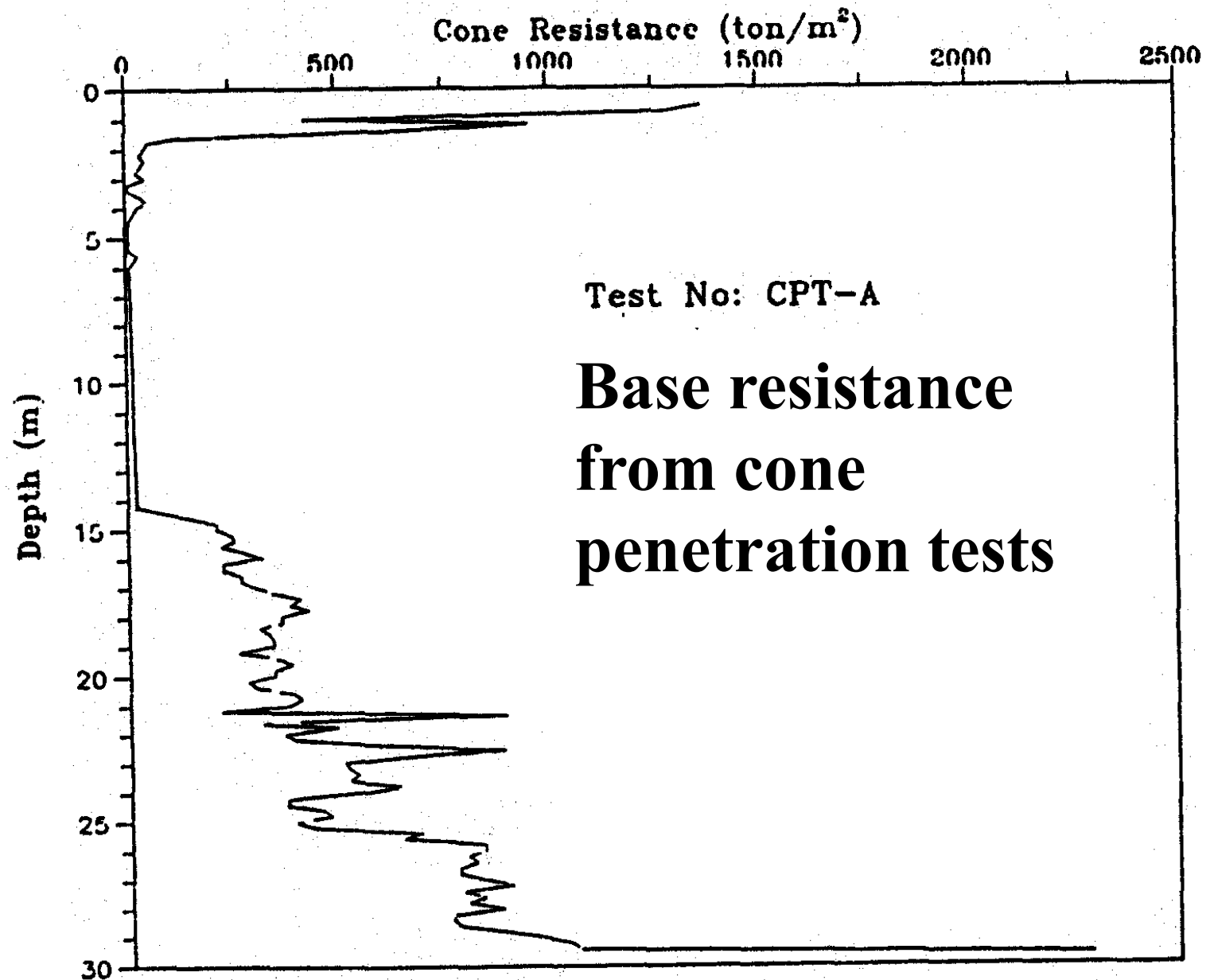
Cone resistance in  $\text{t/m}^2$



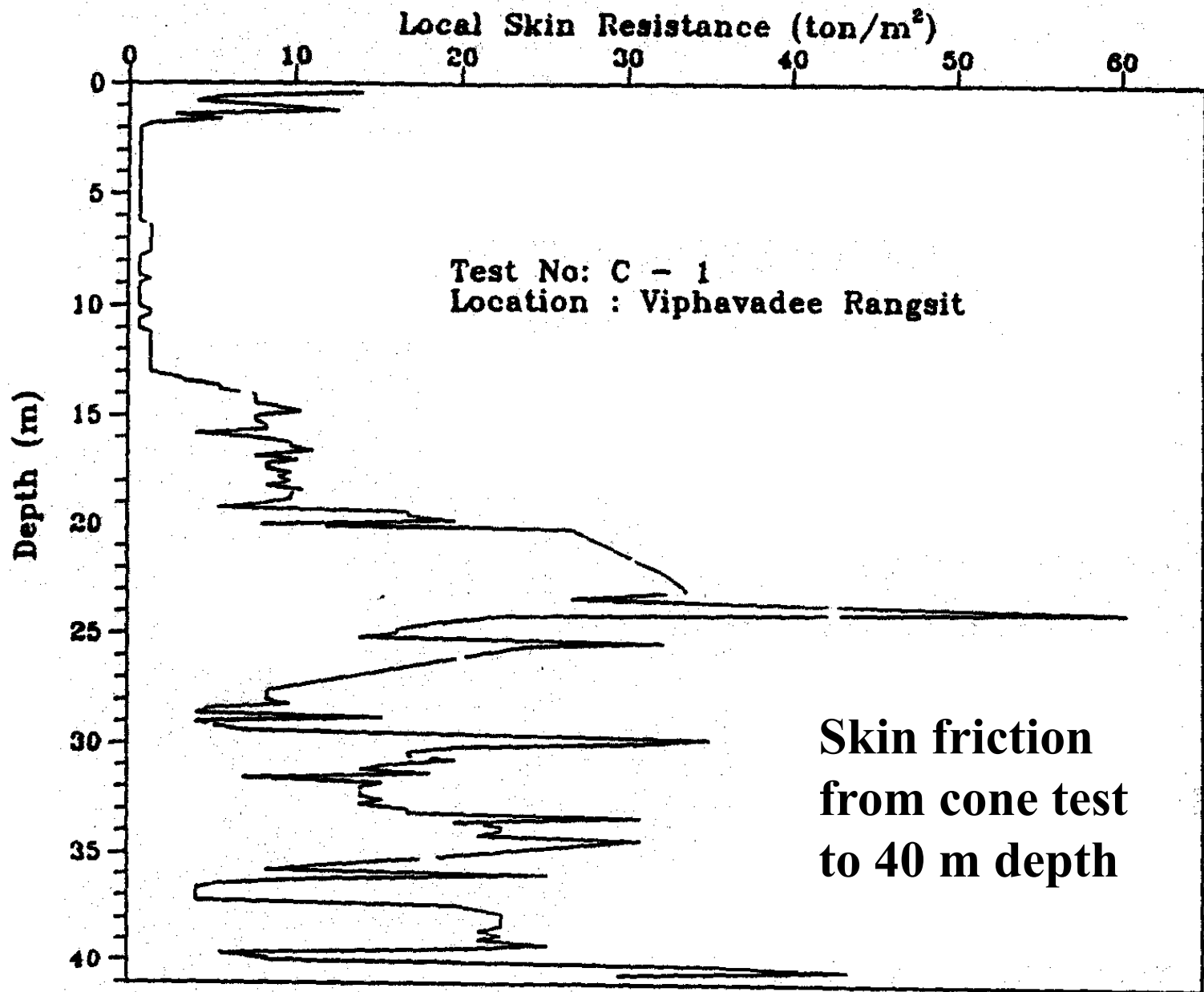
**Cone  
Resistance**







**Fig.3.3 CPT Profile for TP10 at Chatuchak Park  
Don Muang Project (0.8 m X 30 m)**





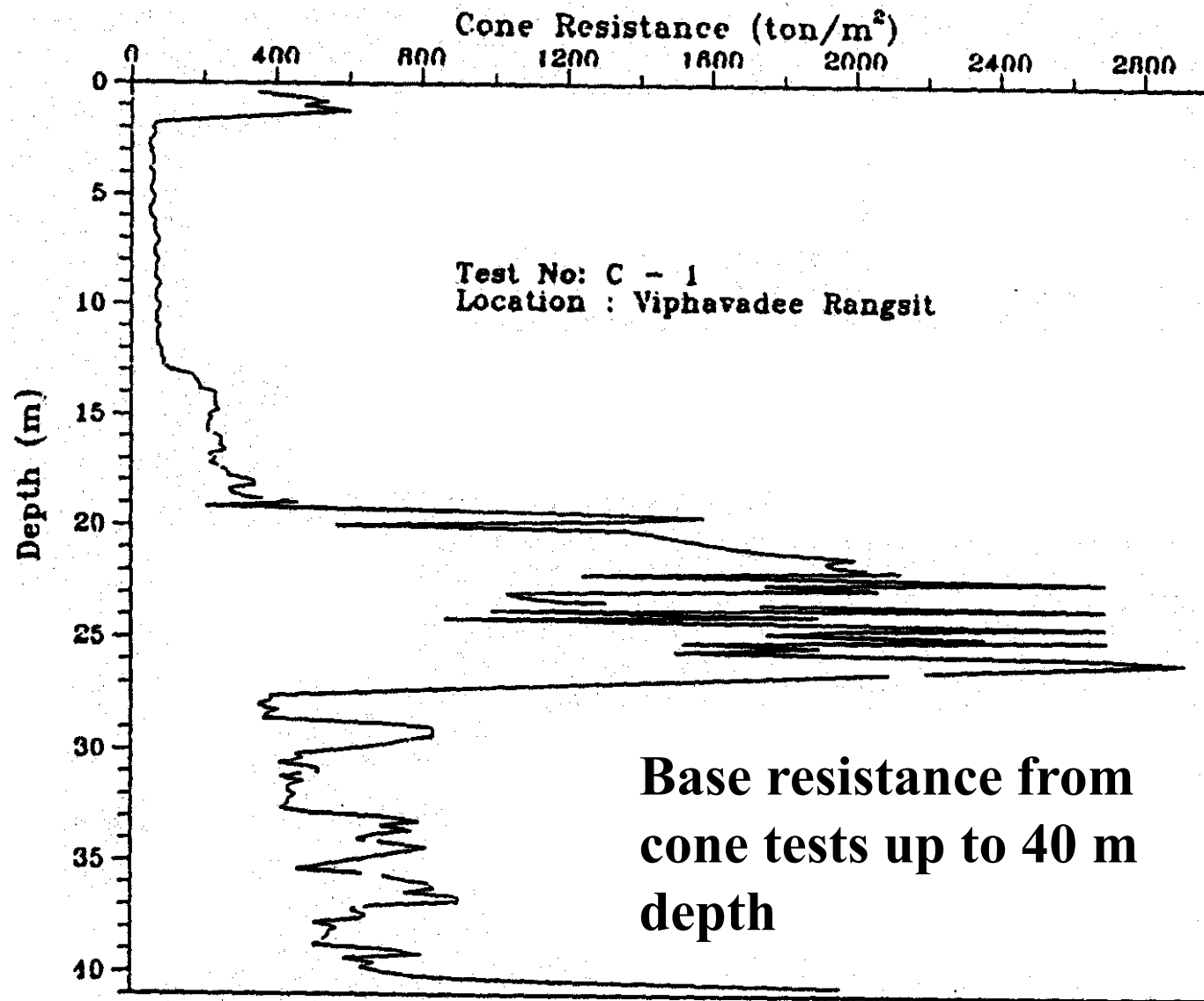
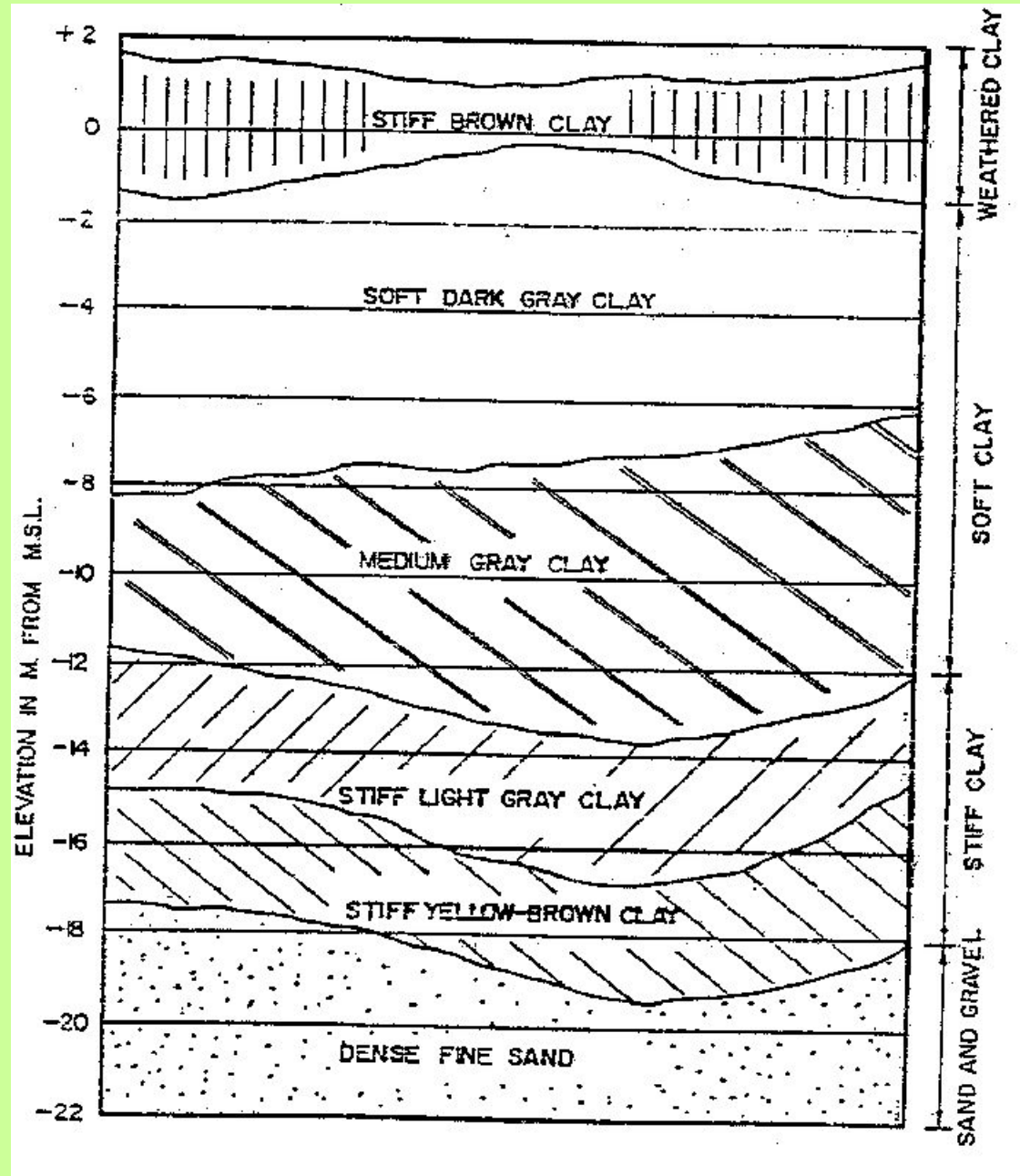


Fig. 3.5 CPT Profile for pile at 16+035  
Don Muang Project (0.8 m X 37.5 & 24.6 m)

# Founding level before 1973

1. First stiff clay

2. First sand layer



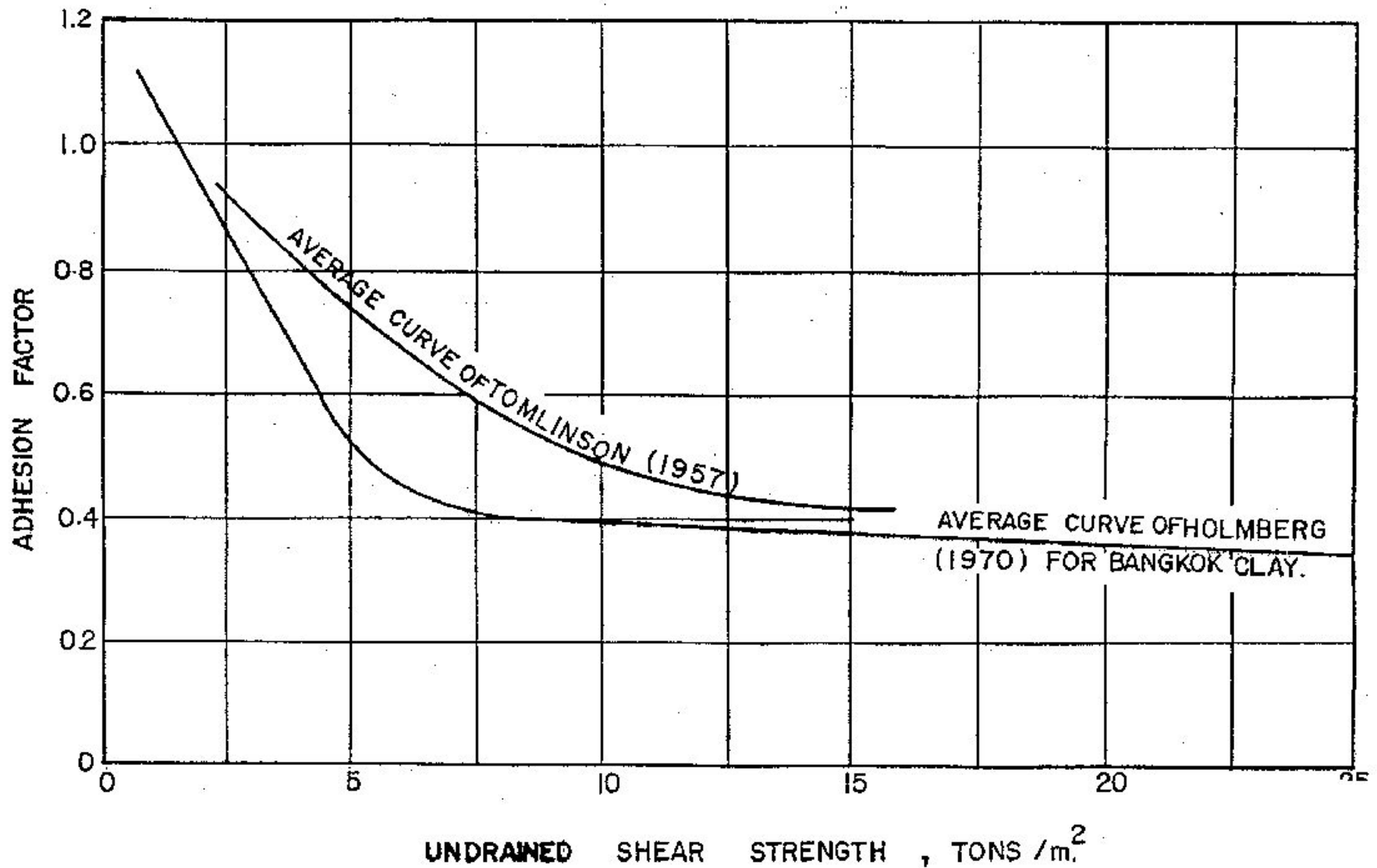
**\* Cone resistance**

**\* Driving Resistance**

**\* Ultimate Load  
measured**

PILE	Depth of Pile Tip (m)	Average cone Resistance $q_c; (t/m^2)$	Driving Resistance $Q_o; (t-m/m)$	Measured Ultimate Pile Loads $Q_u; (tons)$
TP1	25.26	545	330	210
TP2	25.32	525	280	165
TP3	29.33	518	430	210
TP17	27.55	780	840	360
TP18	26.95	689	1,110	360
TP19	27.05	615	1,050	360
TP20	22.40	430	117	90
TP21	28.025	402	385	180
TP22	18.50	415	183	78
TP23	20.50	535	293	82.5
TP29	20.70	366	66	67
TP30	25.00	759	1,250	270
TP31	22.30	403	350	143
TP32	18.20	265	260	71
TP33	18.30	275	280	86
TP34	18.40	260	240	67
TP35	24.40	403	470	122





**Adhesion factor  $\alpha$**

**Vane strength  
used**

**$\alpha$  Method  
short piles**

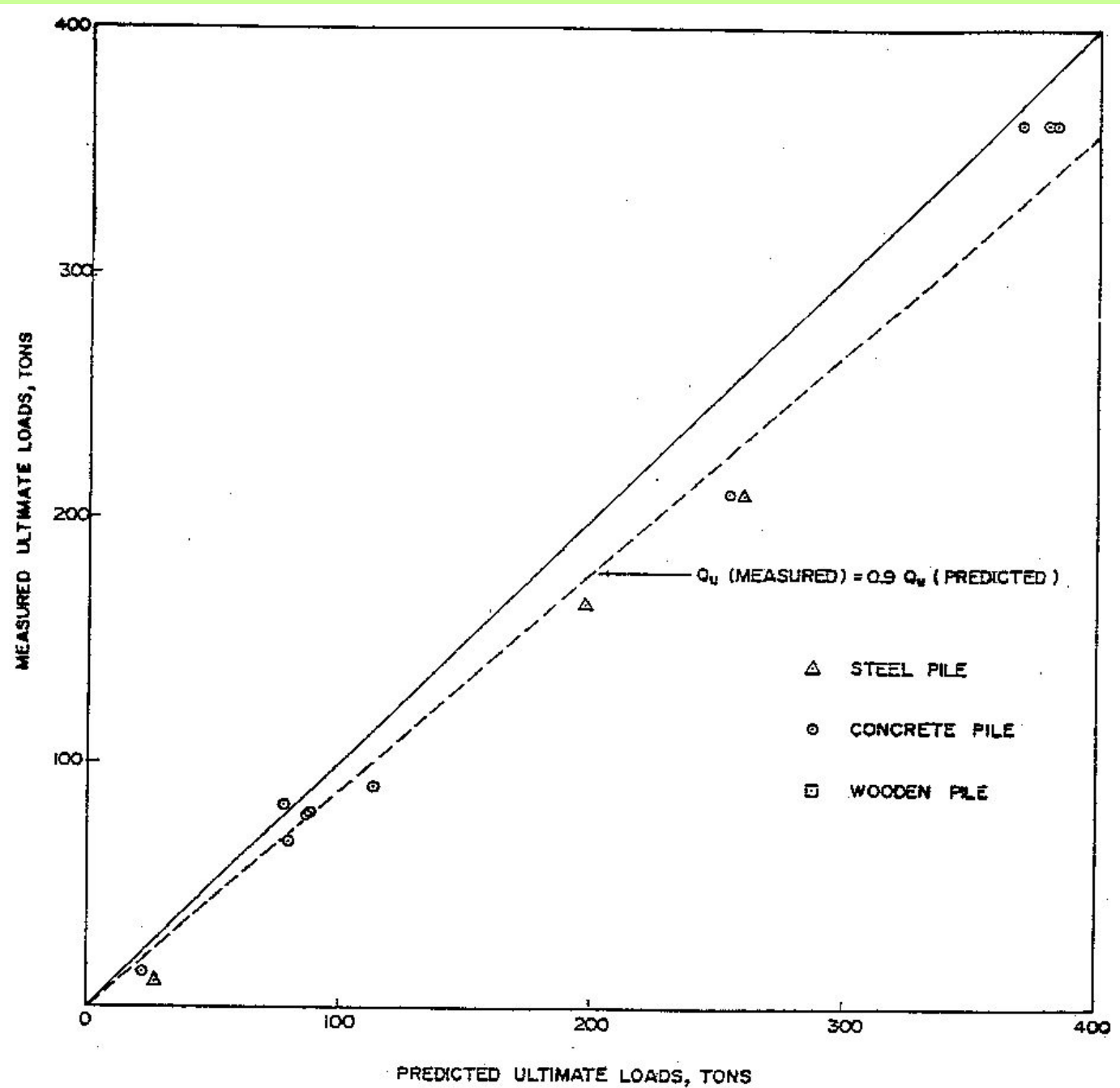
PILE	Ap (m <sup>2</sup> )	C (t/m <sup>2</sup> ) Vane	Nc	Qp (t)	P (m)	Embedded length (m)	$\alpha$	Su (t/m <sup>2</sup> )	Qs (t)	Qu (t)	Qu Load Tests (t)
TP4	-	-	-	-	1.445	5.33	1.0	1.20	9.2	9.2	4.7
TP5	-	-	-	-	1.445	11.3	0.97	1.73	27.4	27.4	10.3
TP6	0.018	2.65	10	0.47	0.471	6.0	0.88	2.42	6.0	6.47	3.5
TP7	0.018	2.65	10	0.47	0.471	6.0	0.88	2.42	6.0	6.47	3.5
TP8	0.108	2.65	10	0.47	0.471	6.0	0.88	2.42	6.0	6.47	4.5
TP9	0.018	2.65	10	0.47	0.471	6.0	0.88	2.42	6.0	6.47	4.5
TP10	0.018	2.65	10	0.47	0.471	6.0	0.88	2.42	6.0	6.47	4.5
TP11	0.019	2.60	10	0.49	0.497	4.0	0.89	2.31	4.1	5.59	2.24
TP12	0.018	2.60	10	0.49	0.471	4.0	0.89	2.31	3.9	4.39	2.10
TP13	0.019	2.60	10	0.49	0.497	4.0	0.89	2.31	4.1	4.59	2.16
TP14	0.018	2.60	10	0.49	0.471	4.0	0.89	2.31	3.9	4.39	2.10
TP15	0.022	2.65	10	0.58	0.523	7.5	0.85	2.56	8.5	9.08	6.5
TP16	0.022	2.65	10	0.58	0.523	6.0	0.88	2.42	6.7	7.28	5.5
TP24	0.0193	2.0	10	0.40	0.72	9.9	1.0	1.30	9.3	9.70	9.0
TP25	0.0324	2.0	10	0.65	0.92	9.6	1.0	1.25	11.0	11.65	9.0
TP26	0.0324	3.9	10	1.26	0.92	10.6	0.87	2.46	20.9	22.16	14.3
TP27	0.0225	2.2	10	0.50	0.70	12.65	0.95	1.95	16.4	16.90	12.0
TP28	0.0324	2.15	10	0.70	0.85	10.7	0.96	1.90	16.6	17.30	12.0

PILE	Depth of Pile Tip (m)	BASE				SHAFT																			Qu (t)	Qu (t)	
		Ap (m <sup>2</sup> )	N <sub>c</sub>	C (t/m <sup>2</sup> )	Qp (t)	p (m)	Soft Clay				Medium Stiff Clay				Stiff Clay				Sand								Total Qs (t)
							Su (t/m <sup>2</sup> )	α	L (m)	Qs (t)	Su (t/m <sup>2</sup> )	α	L (m)	Qs (t)	Su (t/m <sup>2</sup> )	α	L (m)	Qs (t)	K	Avg. σ <sub>v</sub> (t/m <sup>2</sup> )	φ (deg)	L (m)	Qs (t)				
TP1	25.26	.2025	10	38	77	1.80	1.6	0.98	8.6	24.8	3.0	0.80	7.5	33.2	20.9	0.35	9.16	120.6	-	-	-	-	-	178	256	210	
TP2	25.32	.133	10	38	51	1.46	1.6	0.98	8.6	20.1	3.0	0.80	7.5	27	20.9	0.35	9.22	98.5	-	-	-	-	-	146	197	165	
TP3	29.33	.133	10	42	56	1.46	1.6	0.98	8.6	20.1	3.0	0.80	7.5	27	24.0	0.34	13.2	157.3	-	-	-	-	-	204	260	210	
TP21	20.025	.0676	10	18.6	12.5	1.36	2.1	0.92	13.6	36	5.5	0.48	3.0	11	15.5	0.39	3.43	28	-	-	-	-	-	76	88	80	
TP22	18.50	.0676	10	16.8	11.4	1.29	3.2	0.76	10	31	4.5	0.57	5.0	17	16.8	0.37	3.5	28	-	-	-	-	-	76	87	78	
TP23	20.50	.0676	10	18.4	12.4	1.29	1.25	1.0	13	21	5.4	0.49	4.0	14	18.4	0.37	3.5	31	-	-	-	-	-	66	78	82.9	
TP29	20.70	.0676	10	15.0	10.0	1.21	2.4	0.87	13	33	5.0	0.53	4.5	14	15.0	0.38	3.2	22	-	-	-	-	-	69	79	67	
			σ <sub>v</sub> (t/m <sup>2</sup> )	φ (deg)	Nq																						
TP17	27.55	.157	23.0	34	46	1.885	2.16	0.9	11.0	40.	.8	0.54	4.0	19.5	15.8	0.38	10.2	116	1.0	22.0	25.5	2/35	46	221	383	360	
TP18	26.95	.157	11.5	34	46	1.885	2.16	0.91	11.0	40.8	4.8	0.54	4.0	19.5	15.8	0.38	10.2	116	1.0	22.0	25.5	1.75	35	210	369	360	
TP19	27.05	.157	19.0	36	56	1.885	2.6	0.85	11.5	48	6.1	0.53	4.5	7.6	10.2	0.40	8.2	63	1.0	16.5	27.0	5.85	93	212	379	360	
TP20	22.40	.0404	15.5	35	43	1.19	2.7	0.84	15.0	41	-	-	-	-	7.1	0.42	3.8	14	1.0	14.5	26.3	3/6	31	86	113	98	

**Total stress method-- long piles**



# Total stress method long piles



PILE	Depth of Pile Tip  (m)	BASE				SHAFT																	Weight of Pile (t)	Qu (t)	Qu Load Test (t)	
		Ap (m <sup>2</sup> )	q <sub>c</sub> (t/m <sup>2</sup> )	λ	Q <sub>p</sub> (t)	P (m)	Soft Clay				Medium Stiff Clay				Stiff Clay				Sand							Q <sub>s</sub> (t)
							L (m)	q <sub>TF</sub> (t/m)	α	Q <sub>s</sub> (t)	L (m)	q <sub>TF</sub> (t/m)	α	Q <sub>s</sub> (t)	L (m)	q <sub>TF</sub> (t/m)	α	Q <sub>s</sub> (t)	L (m)	q <sub>TF</sub> (t/m)	α	Q <sub>s</sub> (t)				
T21	25.26	.2025	545	0.33	36.4	1.80	8.6	10	1.0	18	7.5	15	0.7	18.9	9.16	164	0.5	147.6	-	-	-	-	184.5	12.64	208	210
T22	25.32	.133	525	0.33	23.0	1.46	8.6	11	1.0	16	7.5	20.5	0.7	21	9.22	144	0.5	105	-	-	-	-	142	3.36	162	165
T23	29.33	.133	518	0.33	22.7	1.46	8.6	11	1.0	16	7.5	17	0.7	17.4	13.2	242	0.5	176.6	-	-	-	-	210	3.87	229	210
TP21	20.025	.0676	402	0.33	8.9	1.36	13.5	19.5	1.0	26.5	3.0	14.5	0.7	13.8	3.43	50	0.5	34	-	-	-	-	74.3	2.42	81	80
TP22	18.50	.0676	415	0.33	9.3	1.29	10	16	1.0	20.6	5.0	18	0.7	16.3	3.5	52	0.5	33.5	-	-	-	-	70.4	2.09	78	78
TP23	20.50	.0676	535	0.33	11.9	1.29	13	15	1.0	19.4	4.0	9	0.7	8.1	3.5	71	0.5	45.8	-	-	-	-	73.3	2.09	83	82.5
TP29	20.70	.0676	366	0.33	8.2	1.21	13	18	1.0	21.8	4.5	32	0.7	27.1	3.2	26	0.5	15.7	-	-	-	-	64.6	2.61	70	67
TP17	27.55	.157	780	0.5	61	1.885	11	16	1.0	30.1	4.0	9	0.7	11.9	10.2	159	0.5	150	2.35	72	0.8	108.6	300.6	10.55	351	360
TP18	26.95	.157	689	0.5	54	1.885	11	12	1.0	22.6	4.0	31	0.7	40.9	10.2	190	0.5	179	1.75	83	0.8	80	322.5	10.92	366	360
TP19	27.05	.157	615	0.5	48	1.885	11.5	15	1.0	28.3	1.5	2.5	0.7	3.3	8.2	100.5	0.5	94.7	5.85	132	0.8	199	325.3	10.92	362	360
TP20	22.40	.0404	430	0.5	8.7	1.19	15	24.5	1.0	29.2	-	-	-	-	3.8	30.5	0.5	18.1	3.6	40	0.8	38.1	85.4	2.04	92	90

**Dutch cone test used in pile capacity determination**

# Sand Drain







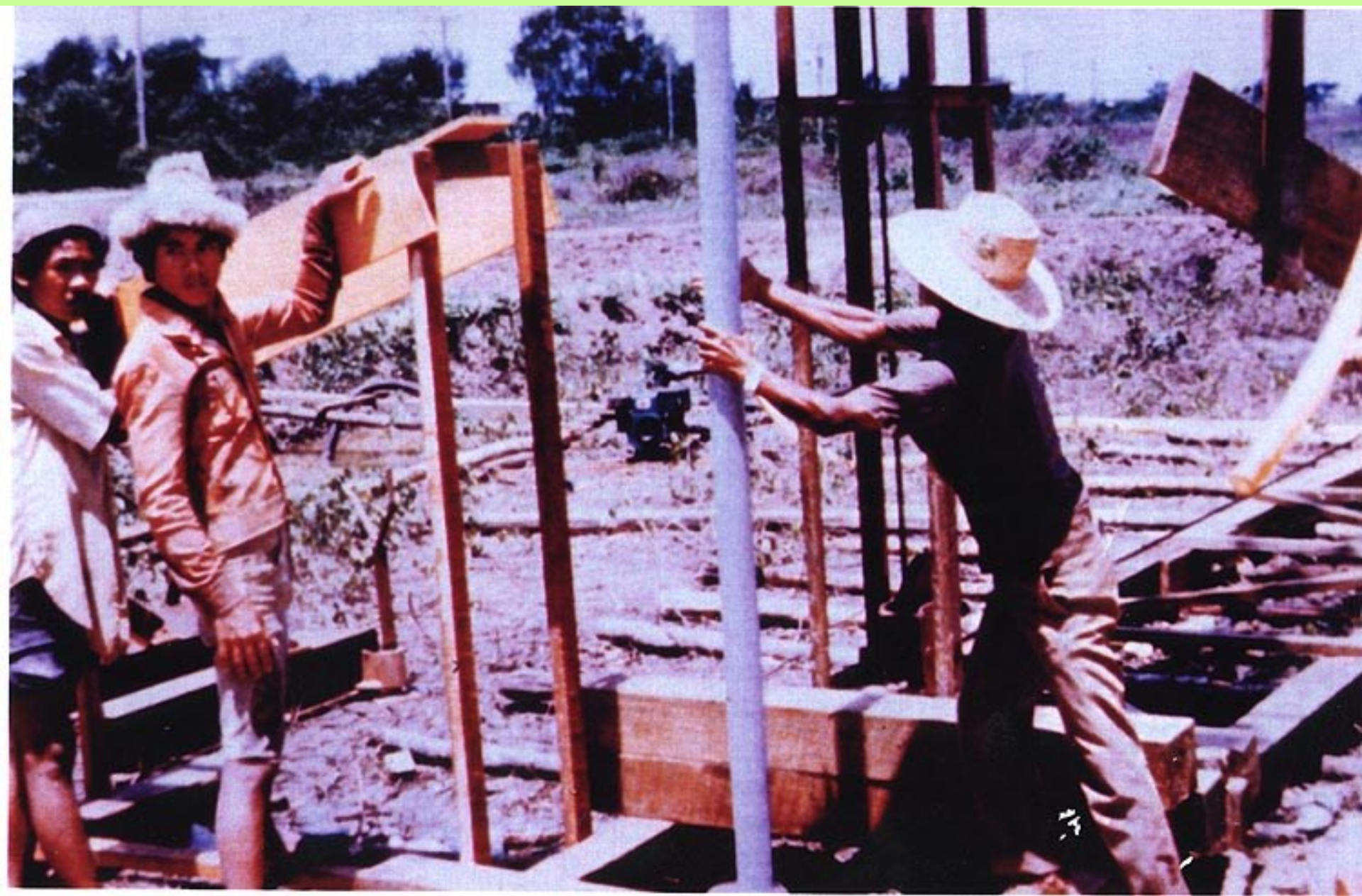




















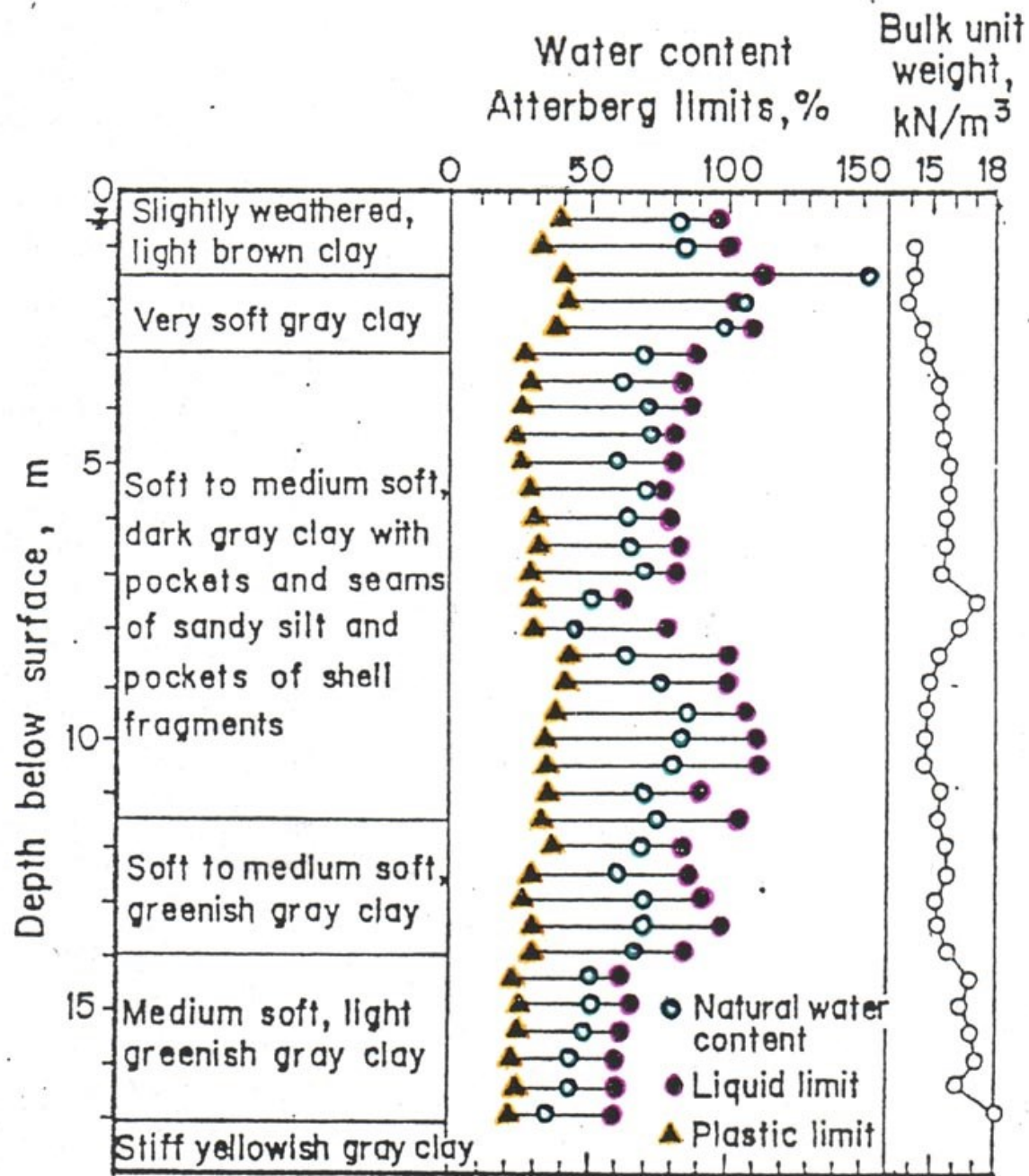
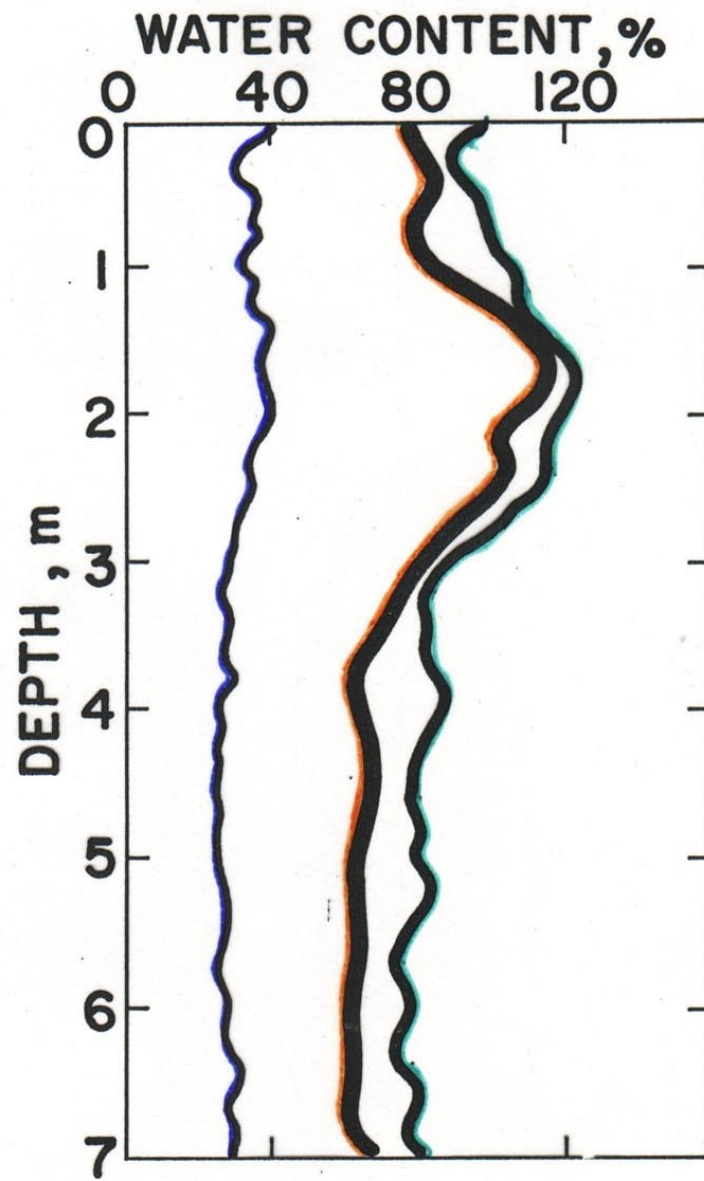
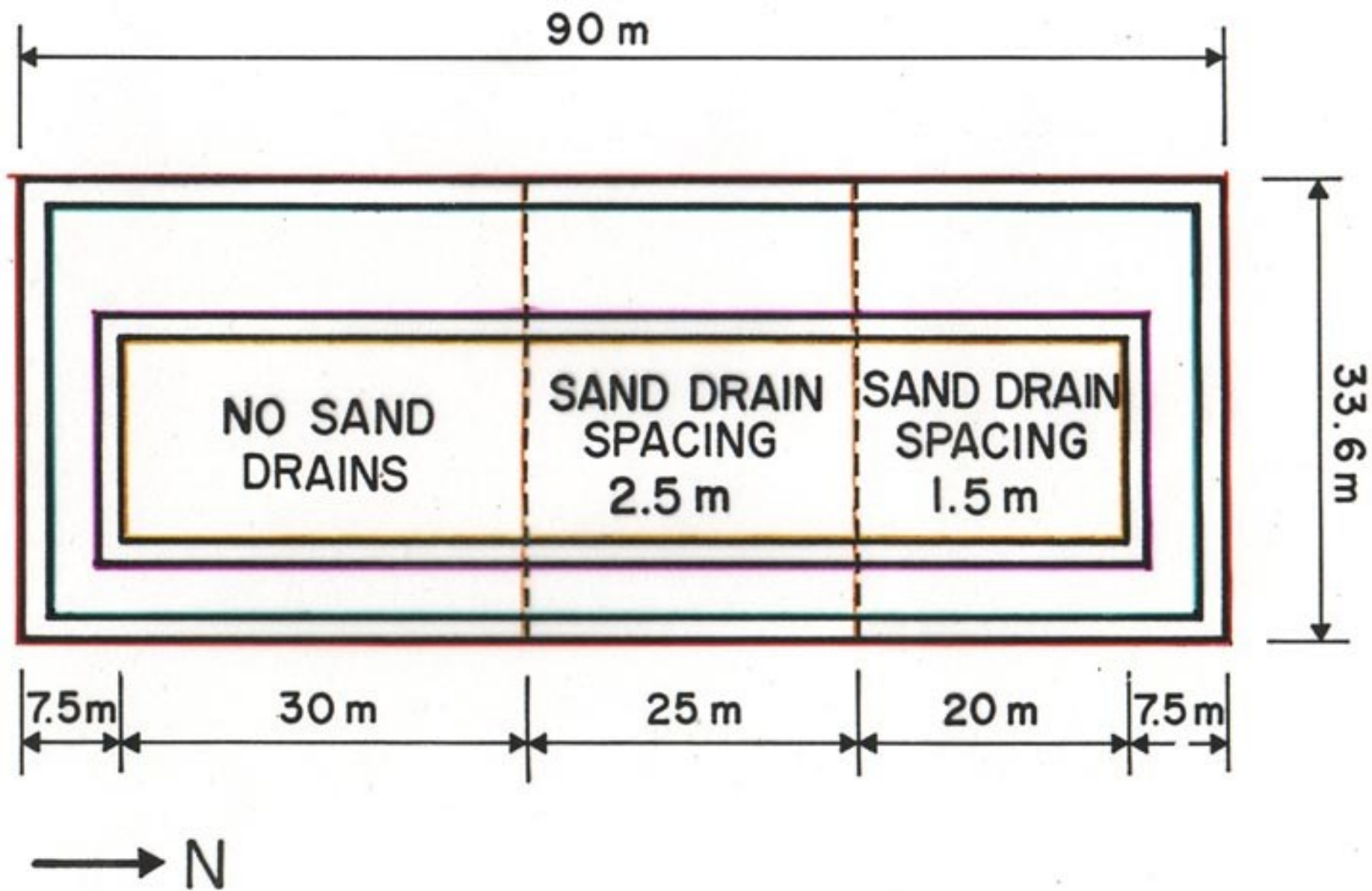


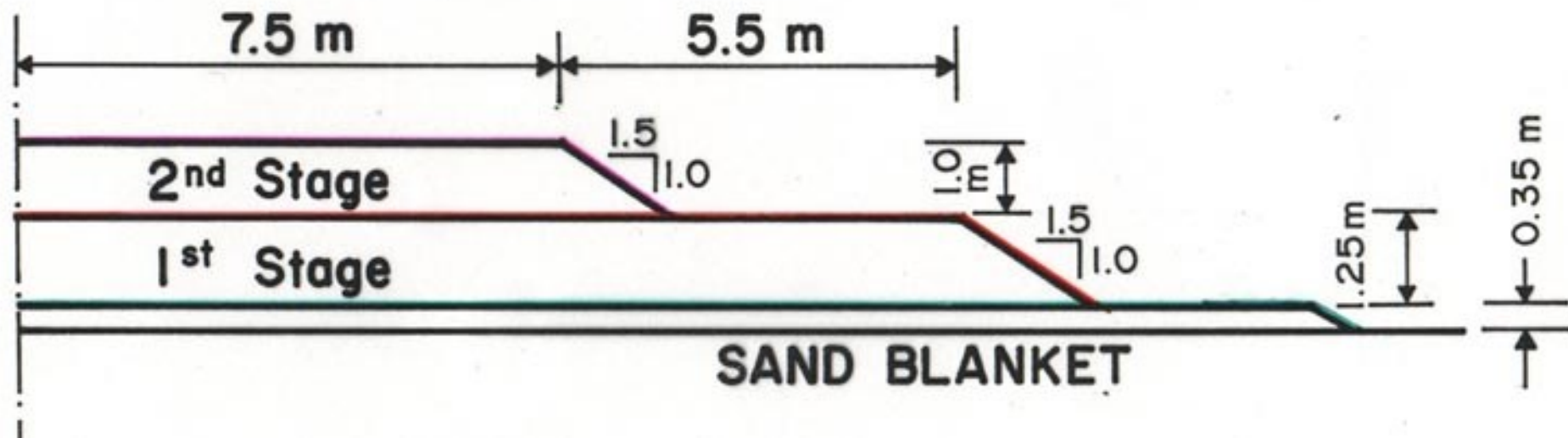
Fig. 4 Soil Profile for Pom Prachul Site

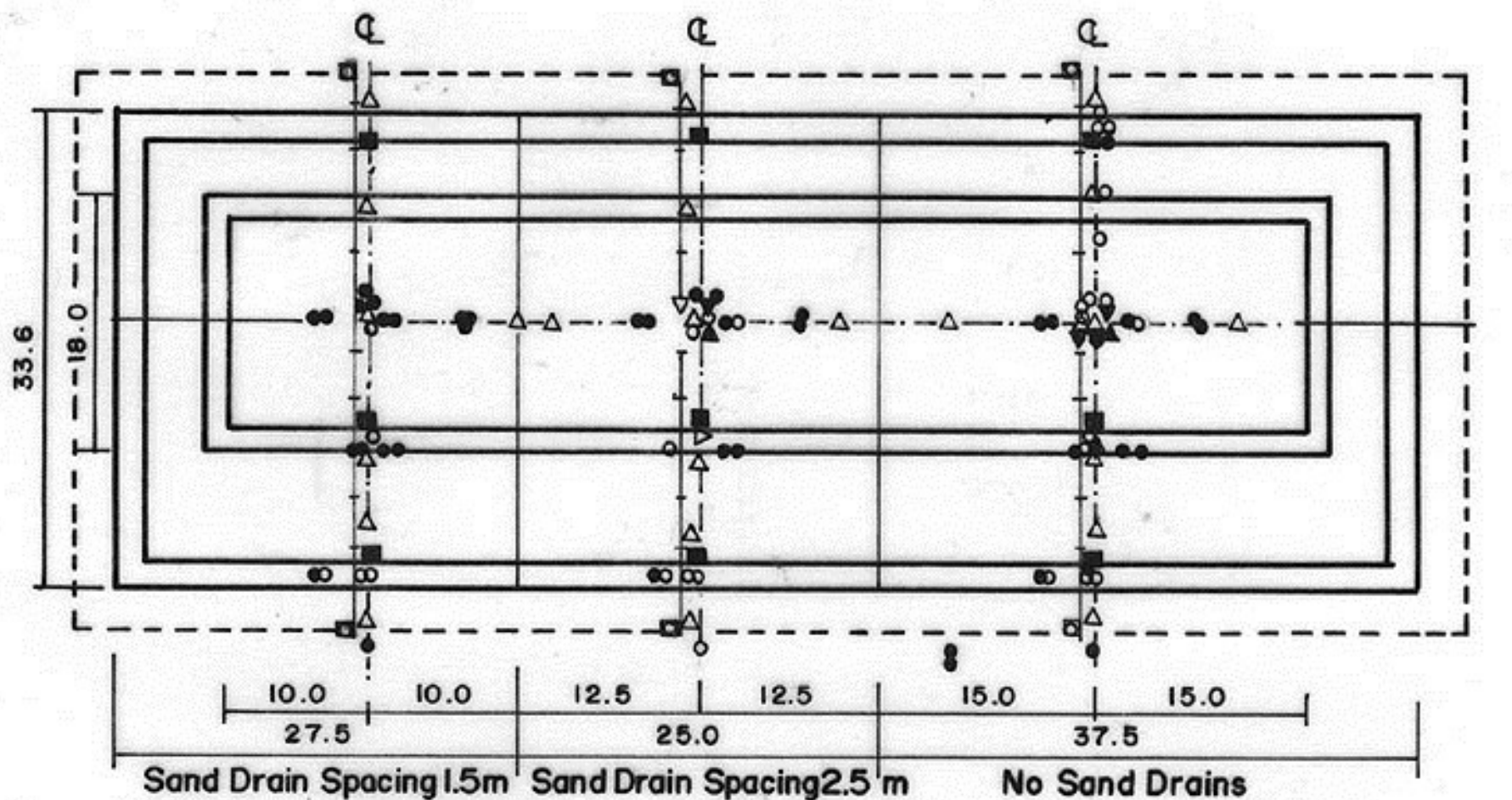


— PL  
— W  
— LL









### Legend Settlement Gauges

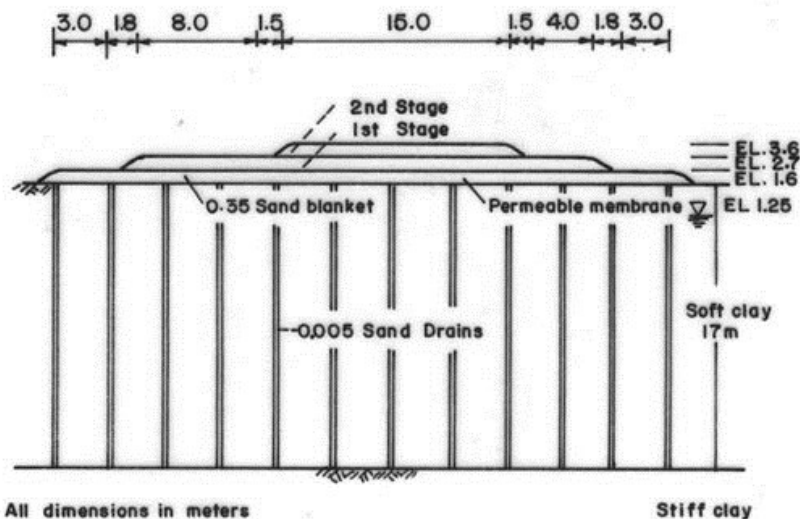
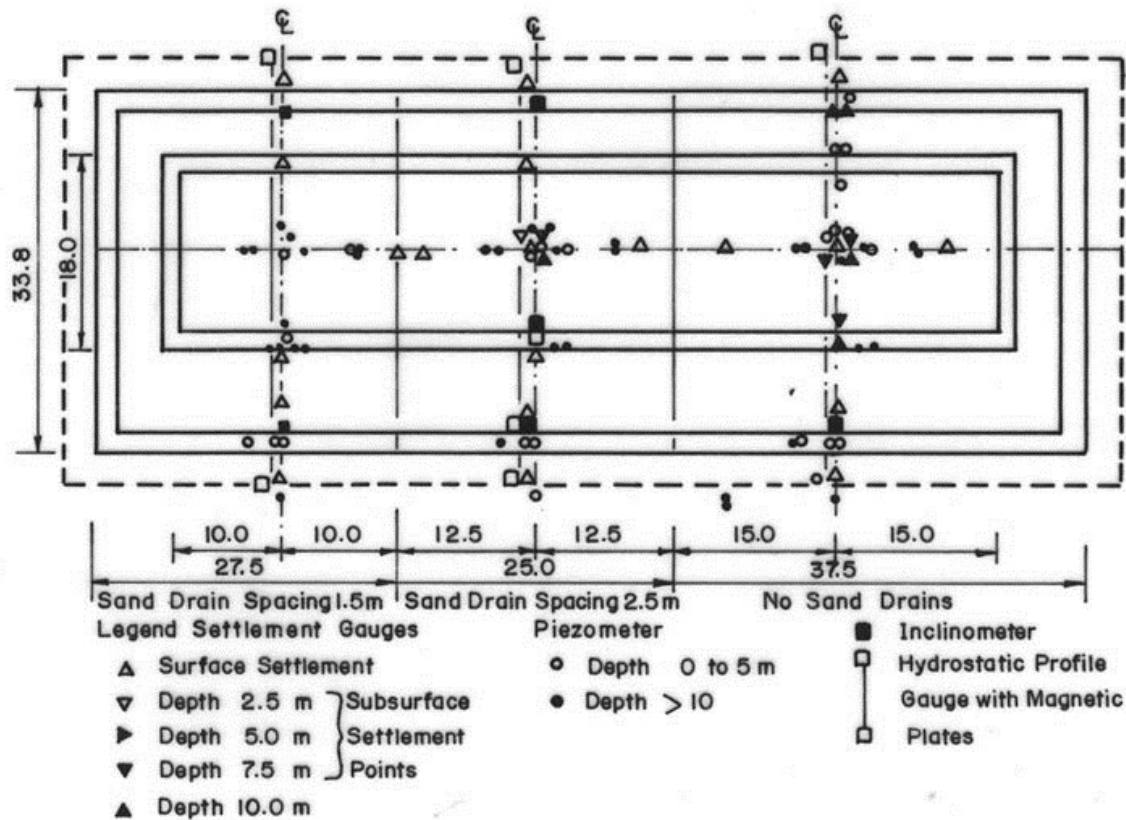
- △ Surface Settlement
- ▽ Depth 2.5 m } Subsurface
- Depth 5.0 m } Settlement
- ▼ Depth 7.5 m } Points
- ▲ Depth 10.0 m

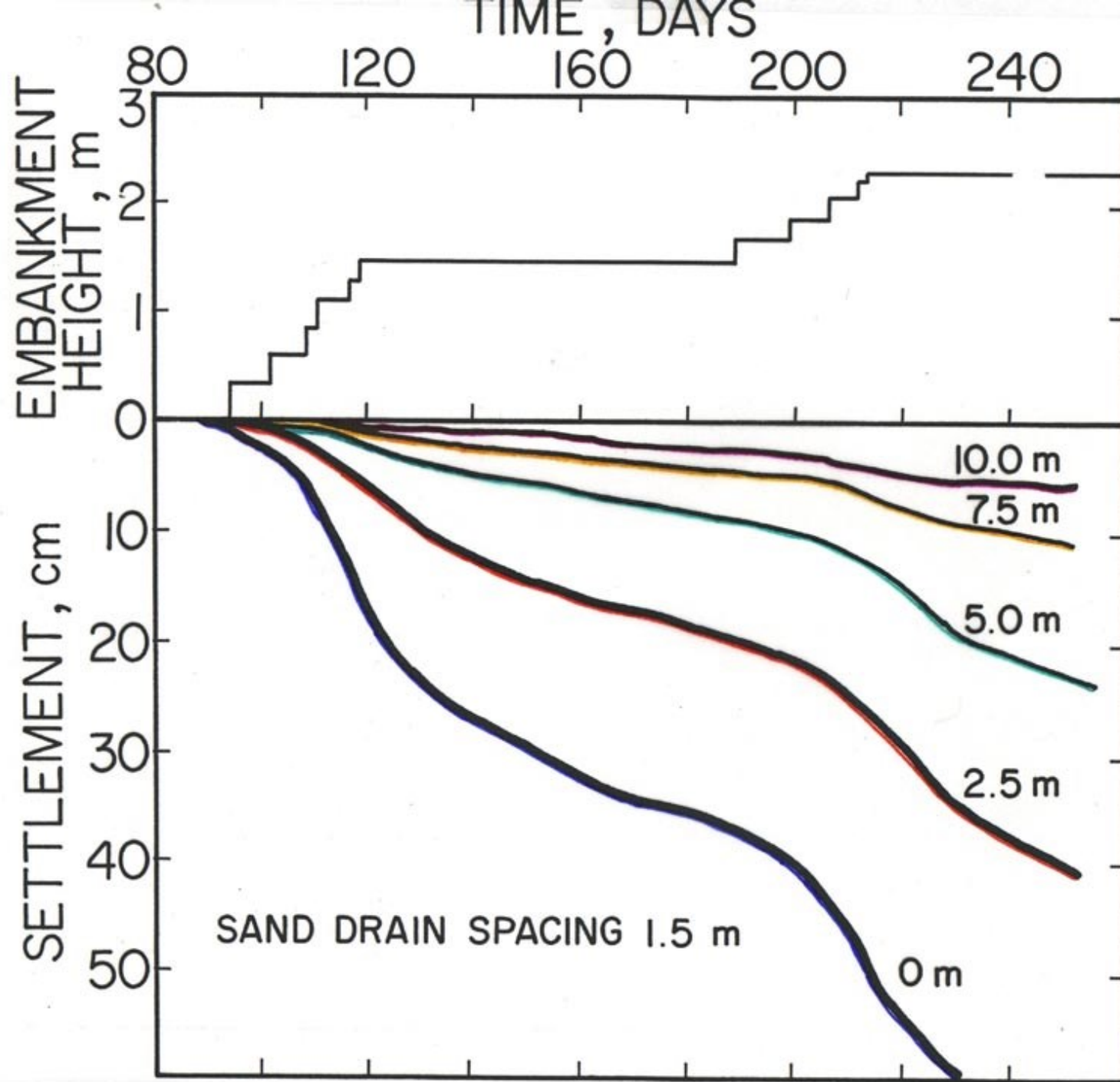
### Piezometers

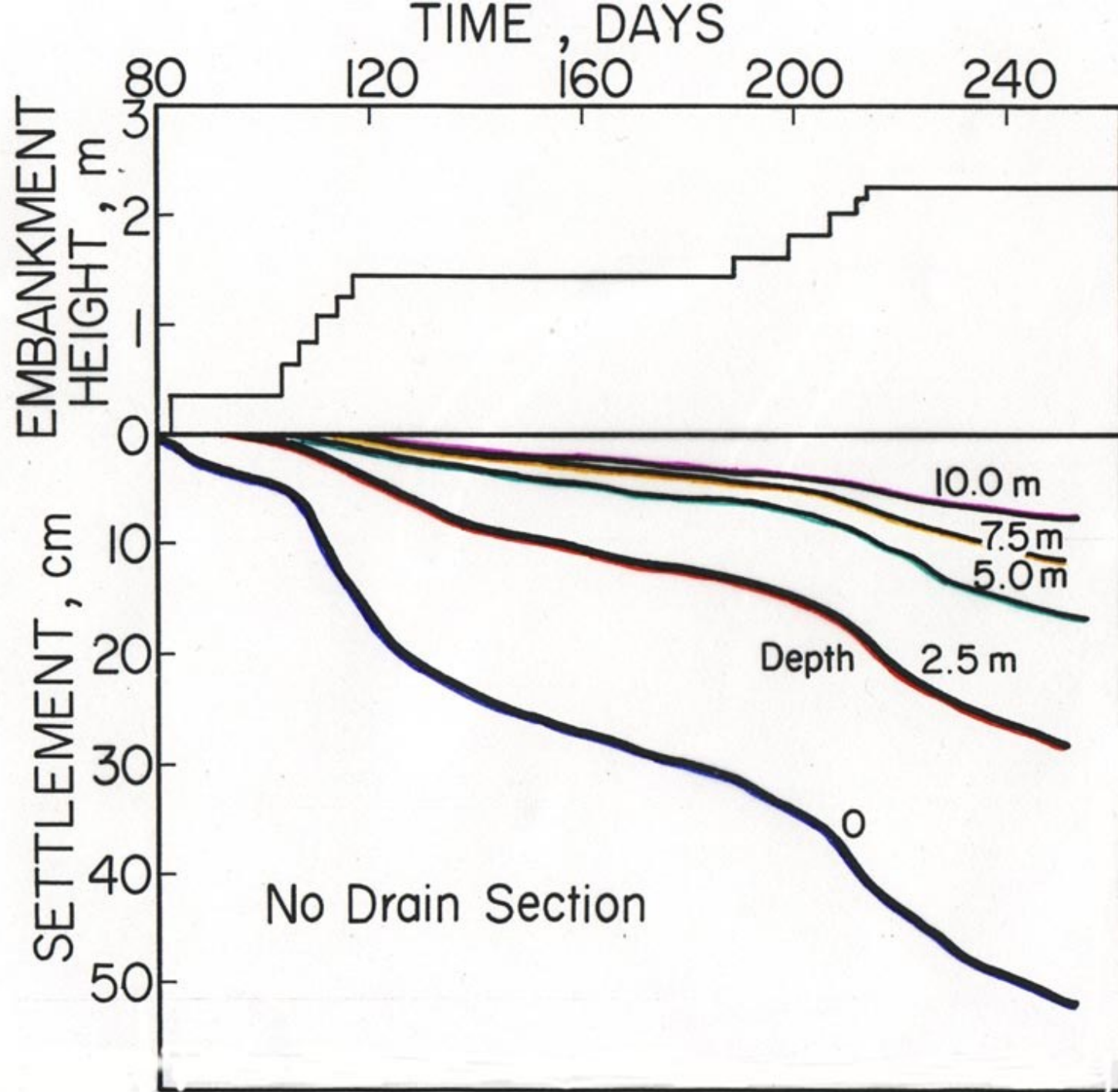
- Depth 0 to 5 m
- ◉ Depth > 5 to 10 m
- Depth > 10 m

- Inclinator
- Hydrostatic Profile Gauge with Magnetic Plates

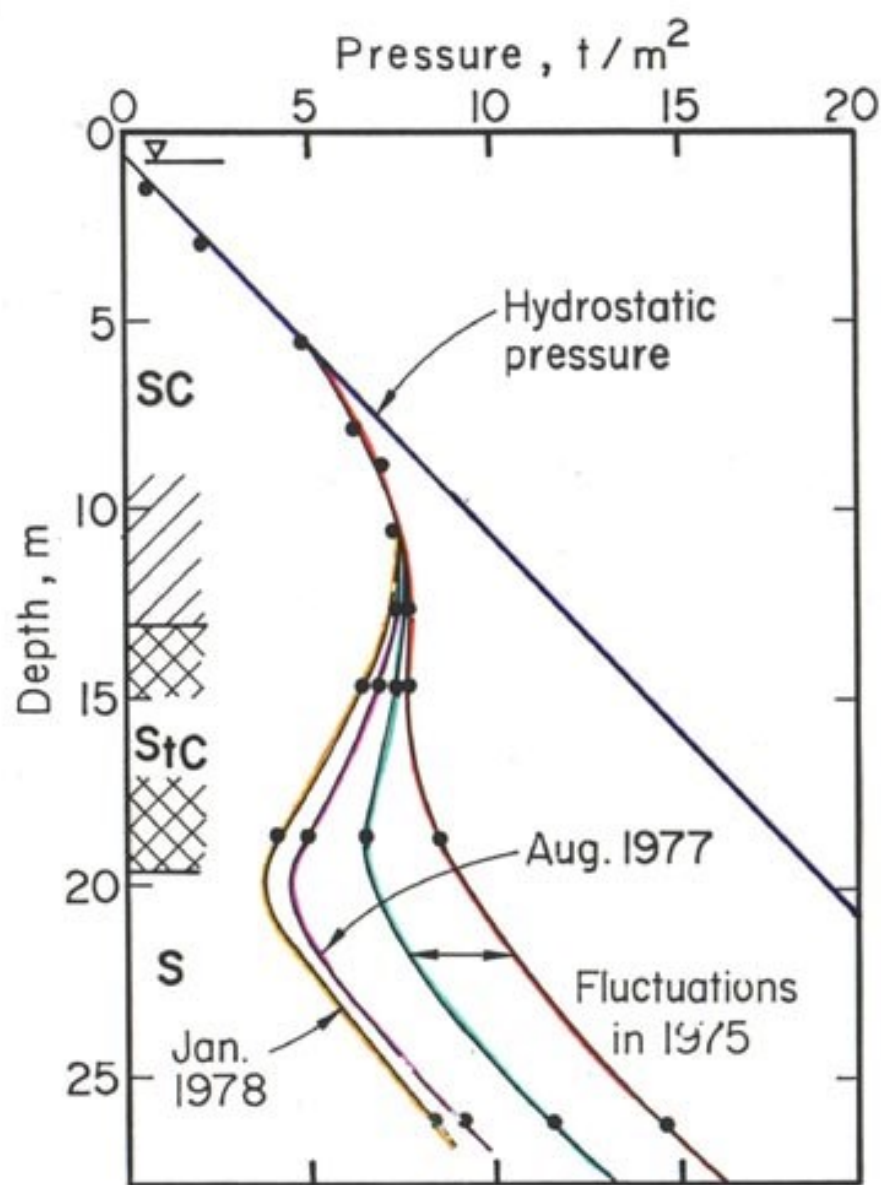




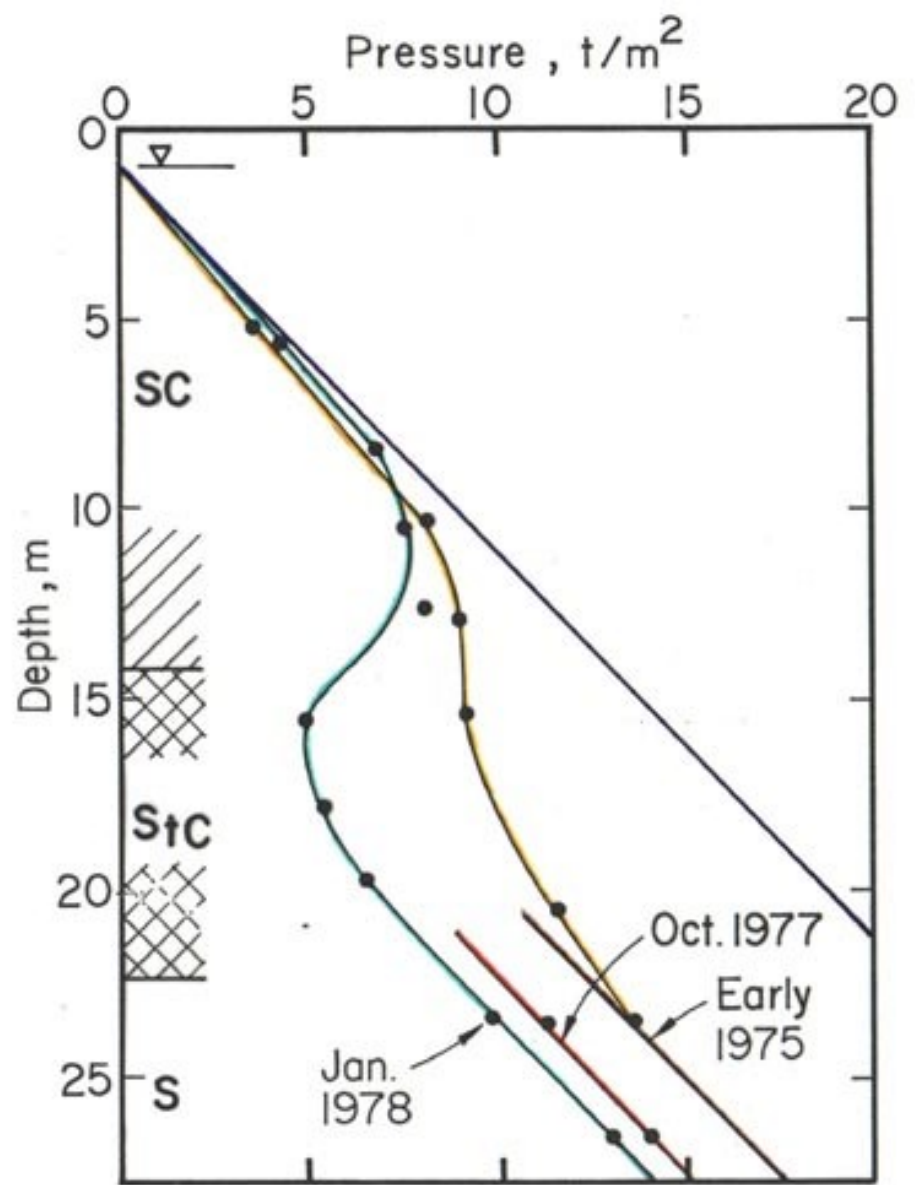








(a) Chulalongkorn University



(b) Nong Ngoo Hao

Water Pressure Declines in Surface Clay Layer