

# CG 11

## HARDENING SOIL MODEL

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- **Introduction (why advanced model?)**
- **Short description of Hardening Soil Model**
- **Parameters of Hardening Soil Model**
- **Comparison with experimental data**
- **Influence of important parameters**
- **Summary**

## INTRODUCTION

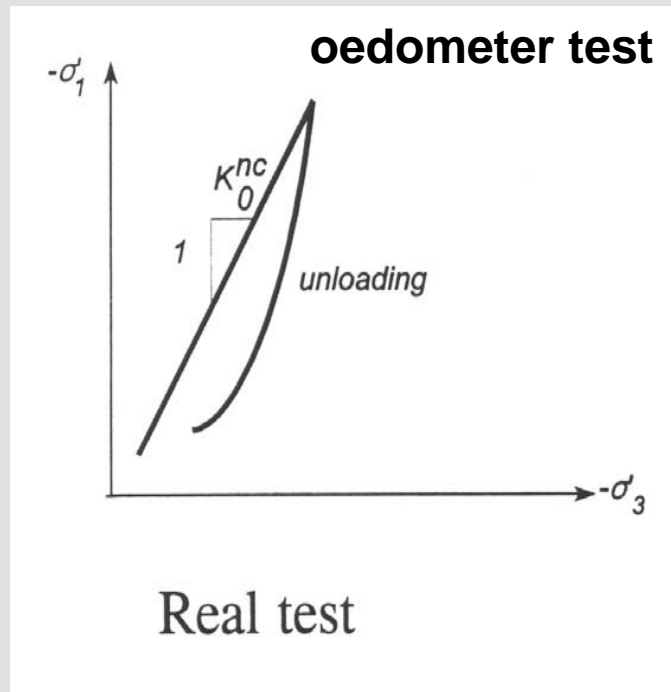
**Soil behaviour includes:**

- **difference in behaviour for primary loading – reloading/unloading**
- **nonlinear behaviour well below failure conditions**
- **stress dependent stiffness**
- **plastic deformation for isotropic or  $K_0$ -stress paths**
- **dilatancy is not constant**
- **small strain stiffness**  
(at very low strains and upon stress reversal)
- **influence of density on strength and stiffness**

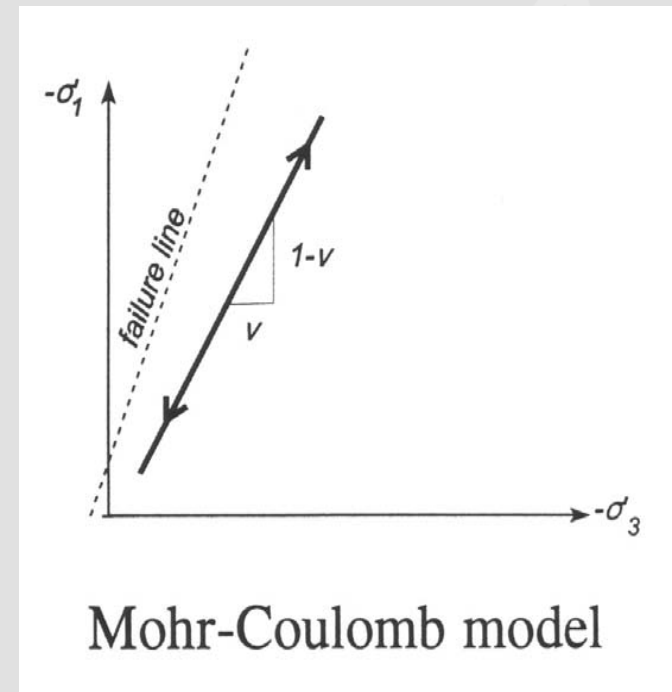
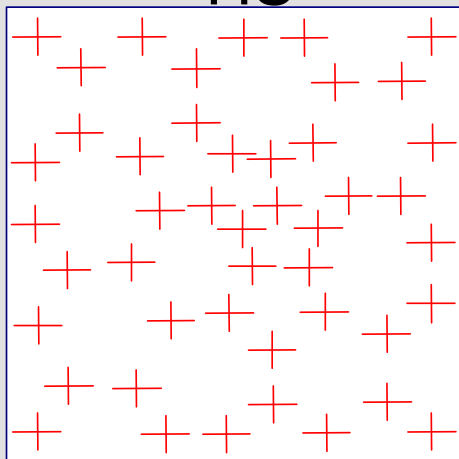


**cannot be accounted for with simple elastic-perfectly plastic constitutive models**

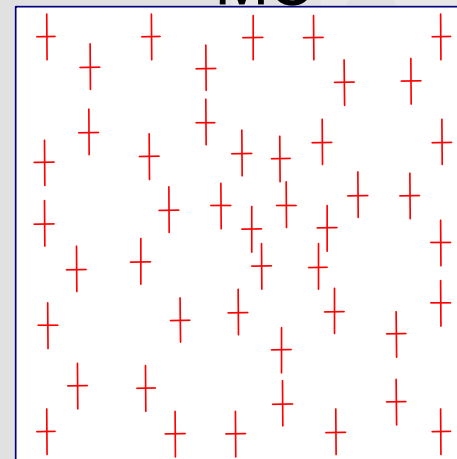
## INTRODUCTION



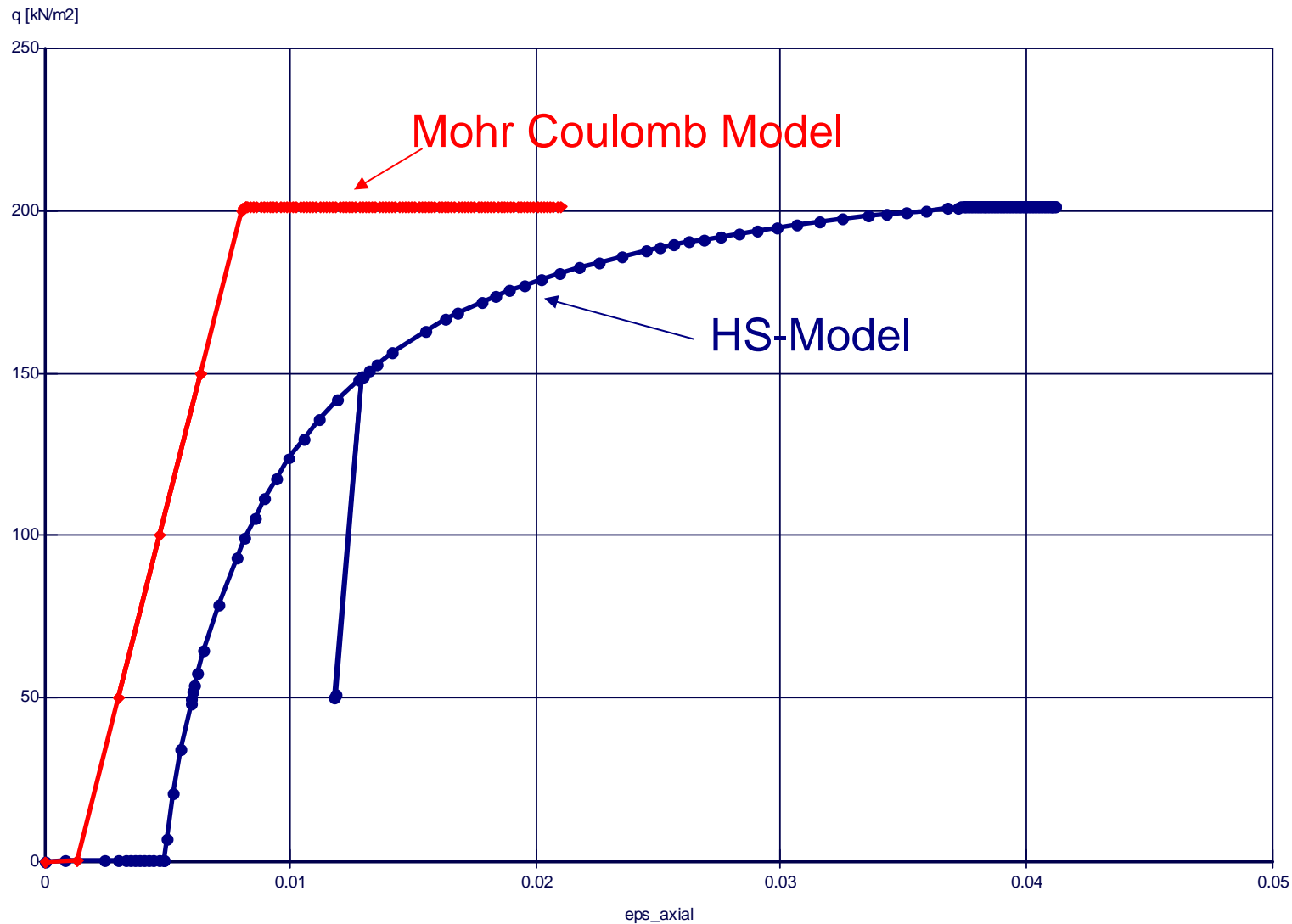
HS



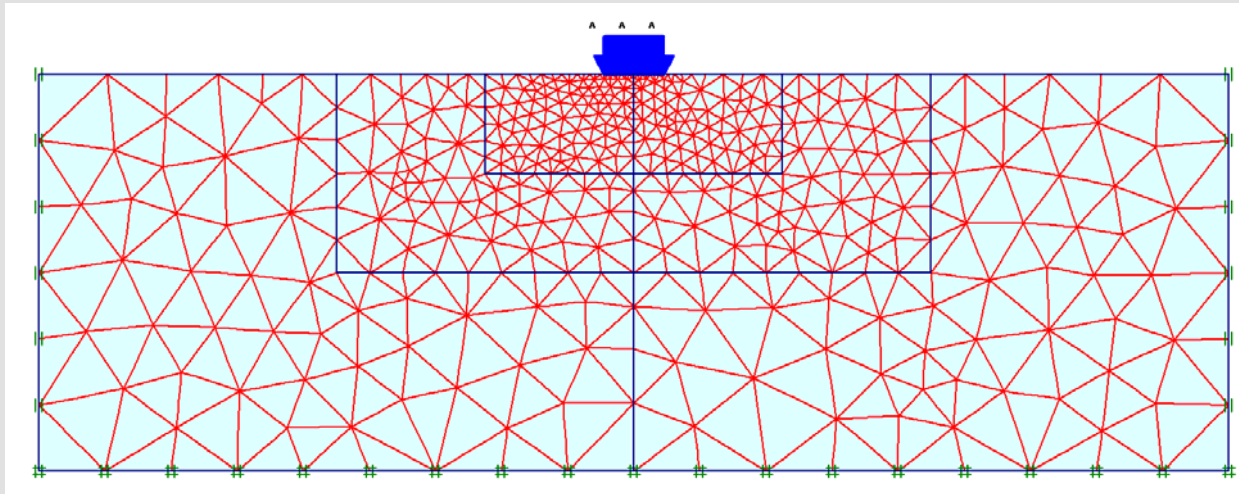
MC



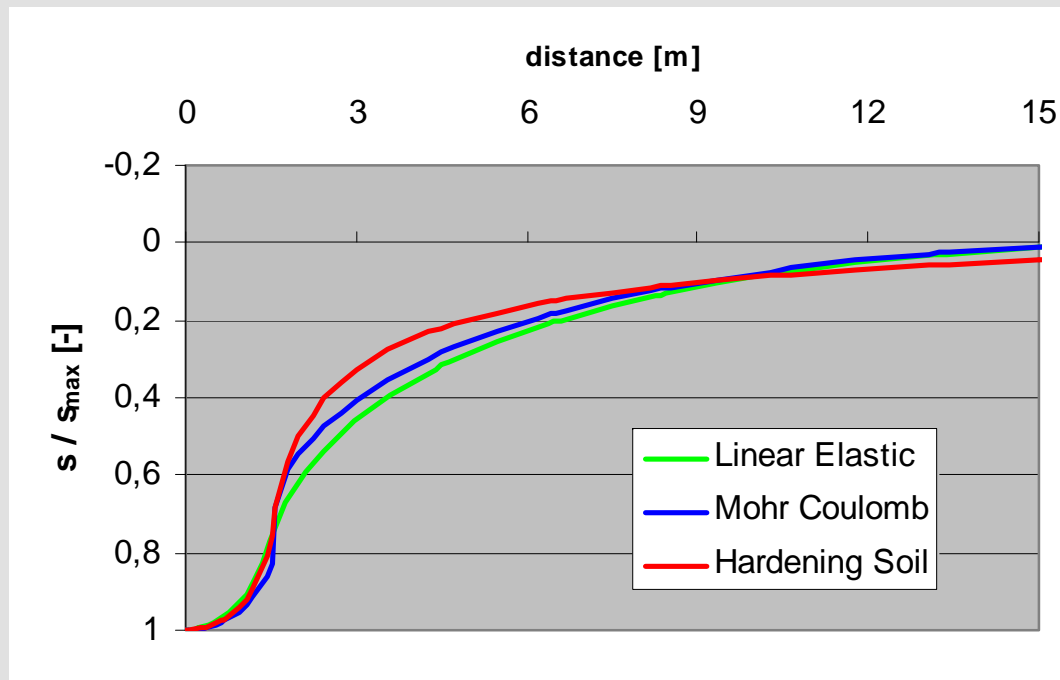
## INTRODUCTION



## INTRODUCTION



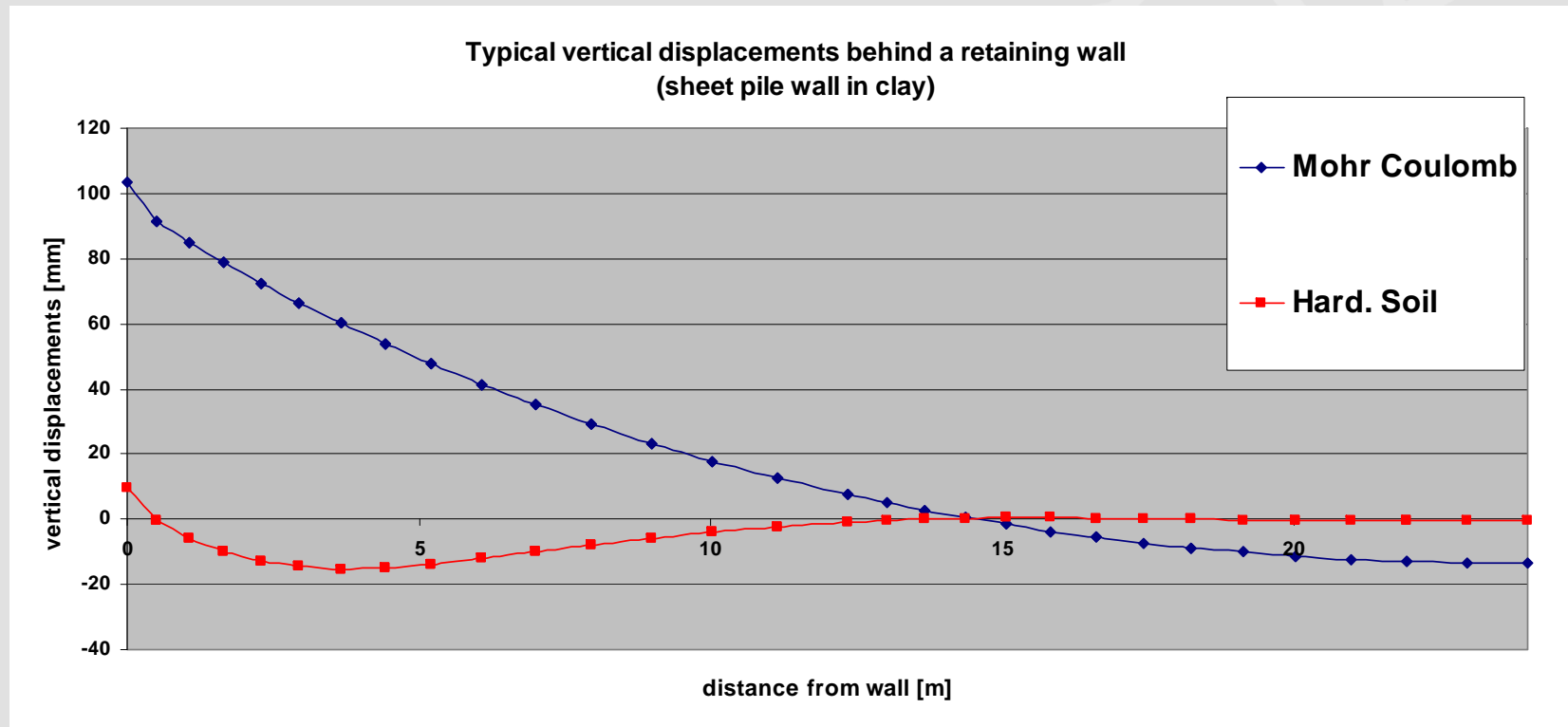
model	$s_{\max}$ [mm]
LE	33
MC	36
HS	60



- All models calculate **settlements**
- Differences in shape of trough and maximum values

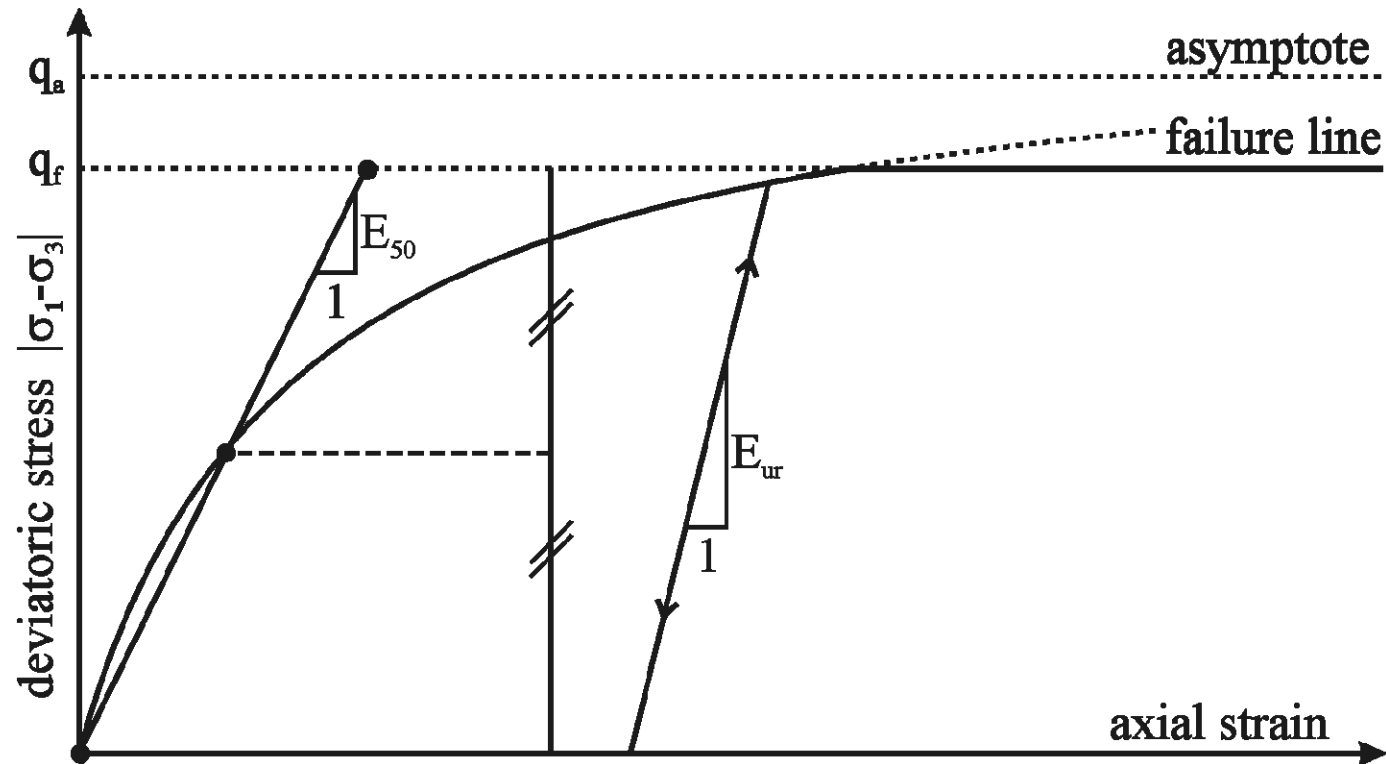
## INTRODUCTION

### Example for vertical displacements behind a retaining wall



- > Hardening Soil Model calculates **Settlements**
- > Mohr-Coulomb Model calculates **Heave**

## DESCRIPTION OF HARDENING SOIL MODEL



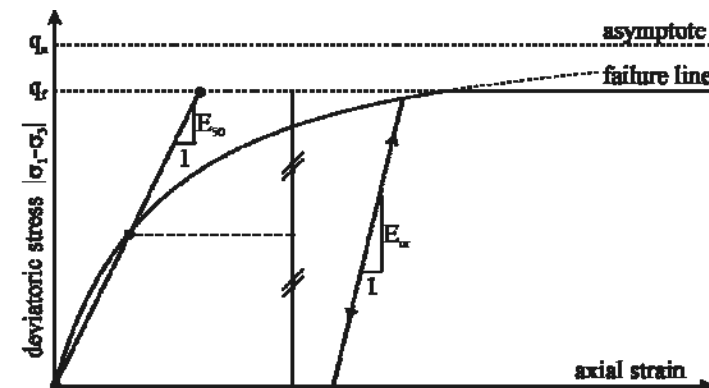
## DESCRIPTION OF HARDENING SOIL MODEL

$$-\varepsilon_1 = \frac{1}{2 E_{50}} \cdot \frac{q}{1 - q/q_a} \quad \text{for } q < q_f$$

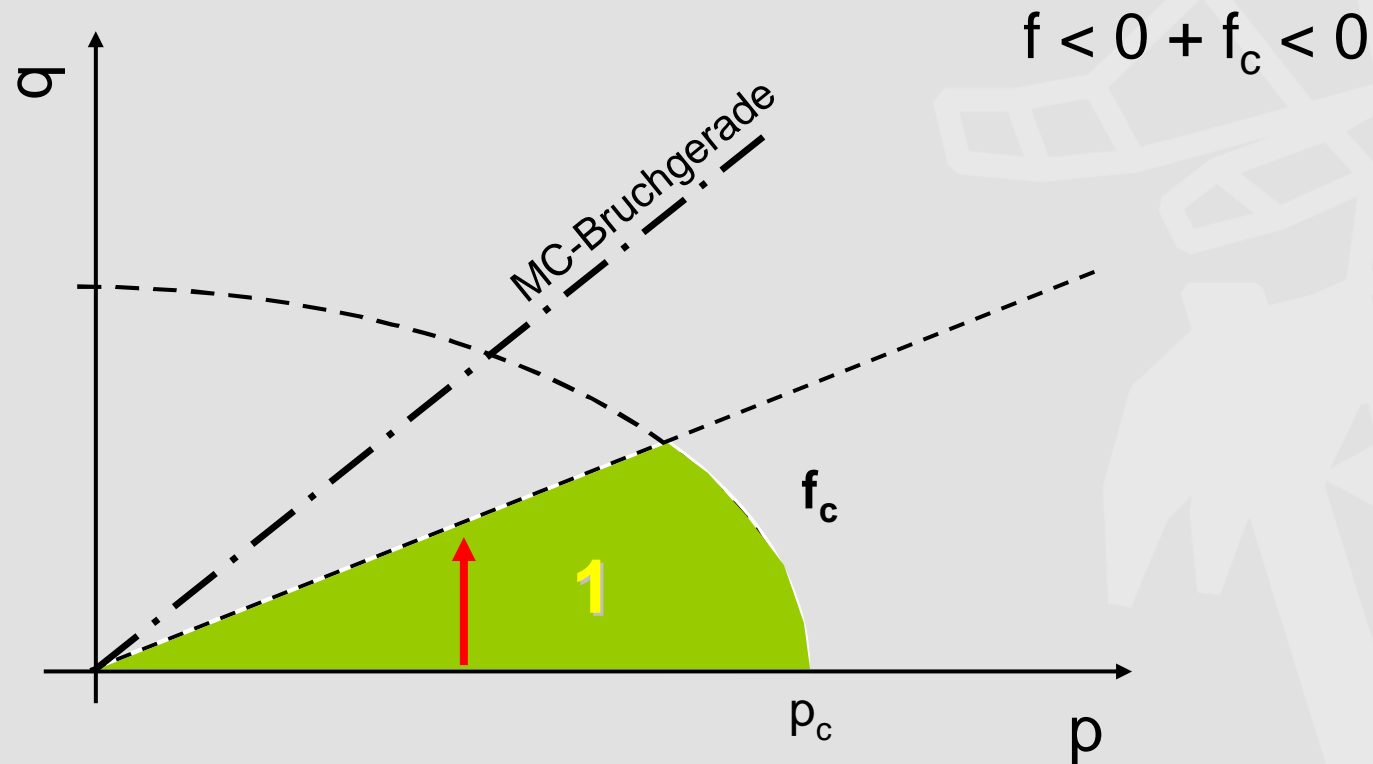
$q_a$  ..... asymptotic value for shear strength

$$q_a = \frac{q_f}{R_f}$$

$$q_f = (c \cdot \cot \varphi - \sigma'_3) \frac{2 \sin \varphi}{1 - \sin \varphi}$$

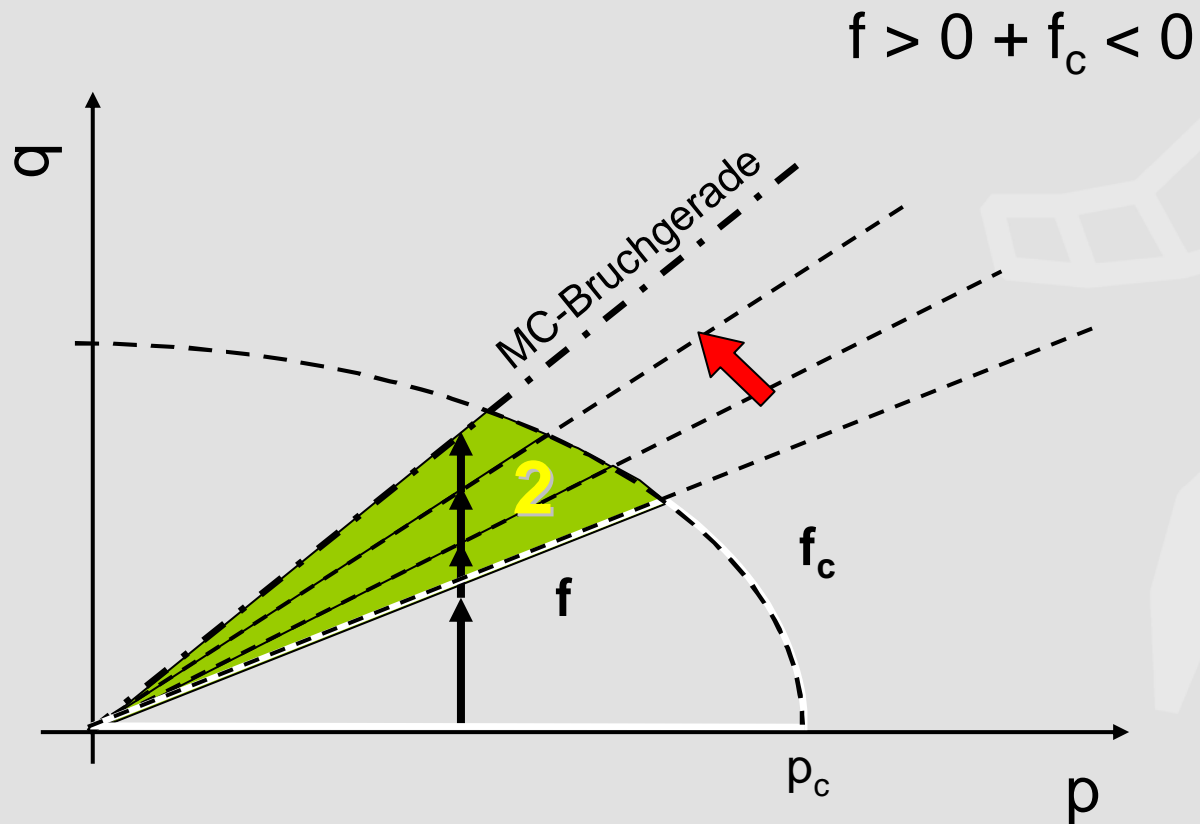


## DESCRIPTION OF HARDENING SOIL MODEL



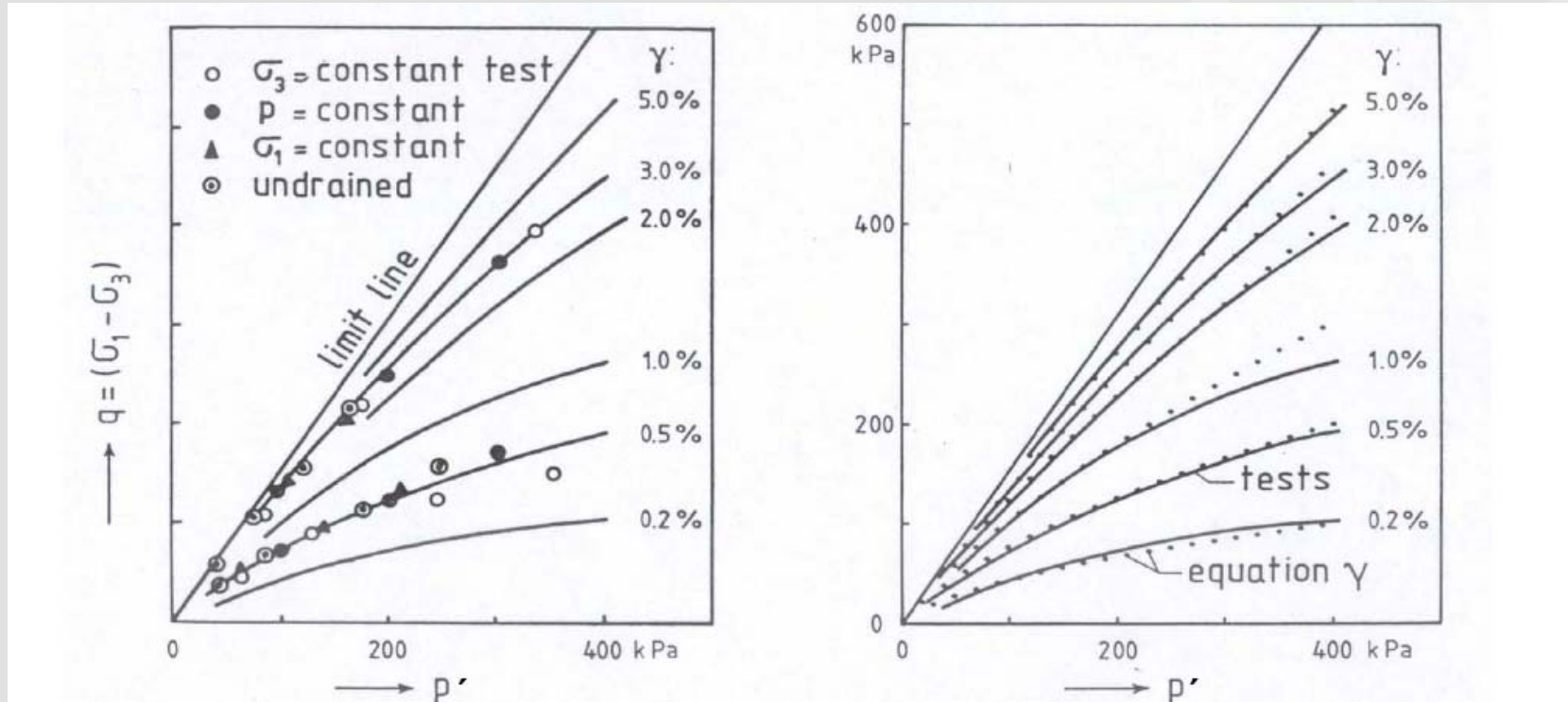
REGION 1  
no yield surface active > elastic

## DESCRIPTION OF HARDENING SOIL MODEL



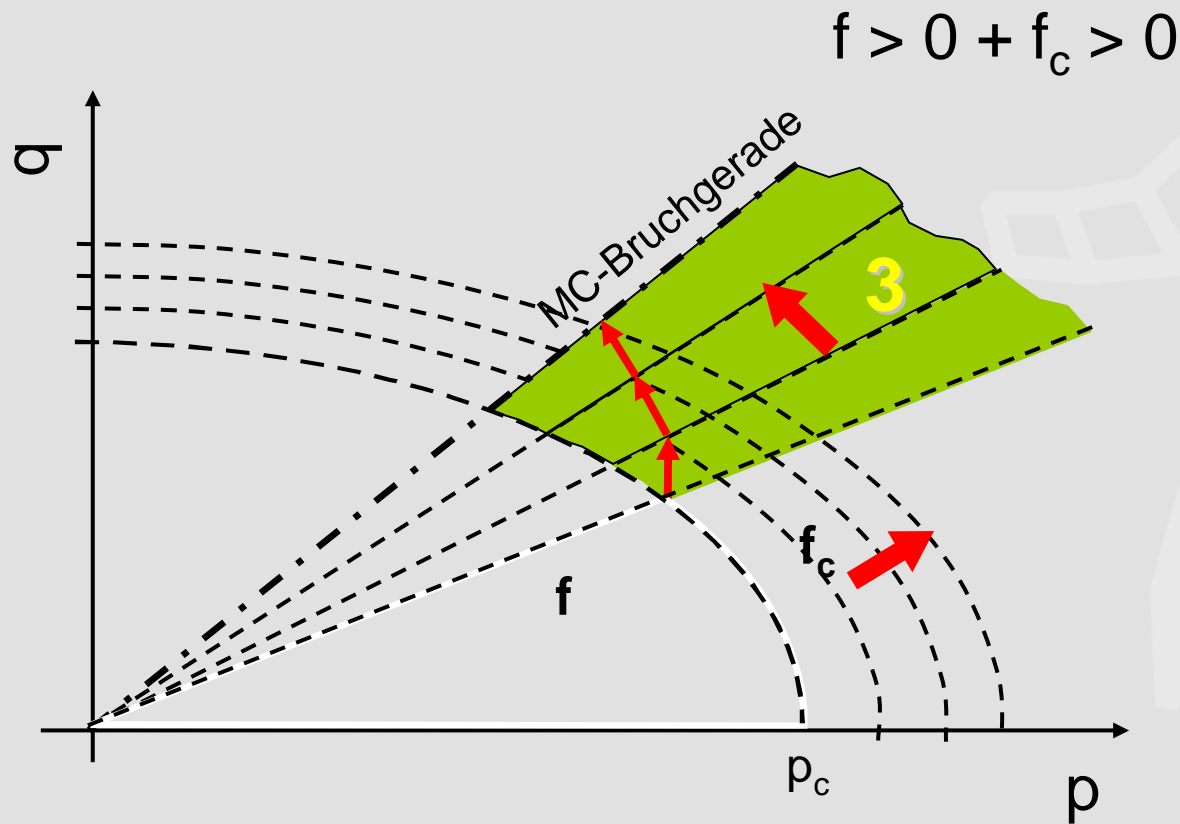
REGION 2  
shear hardening surface active

## DESCRIPTION OF HARDENING SOIL MODEL



**Deviatoric yield surface: lines of equal shear strains in triaxial test**

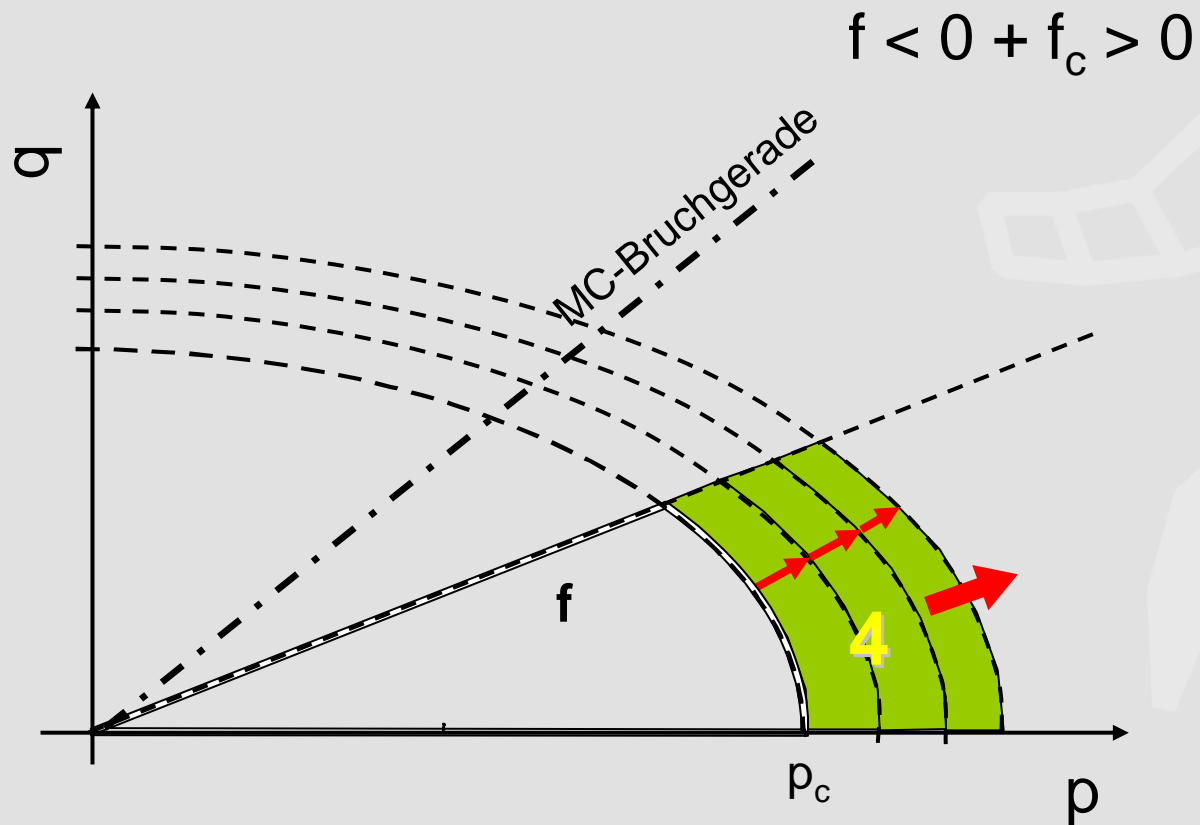
## DESCRIPTION OF HARDENING SOIL MODEL



## REGION 3

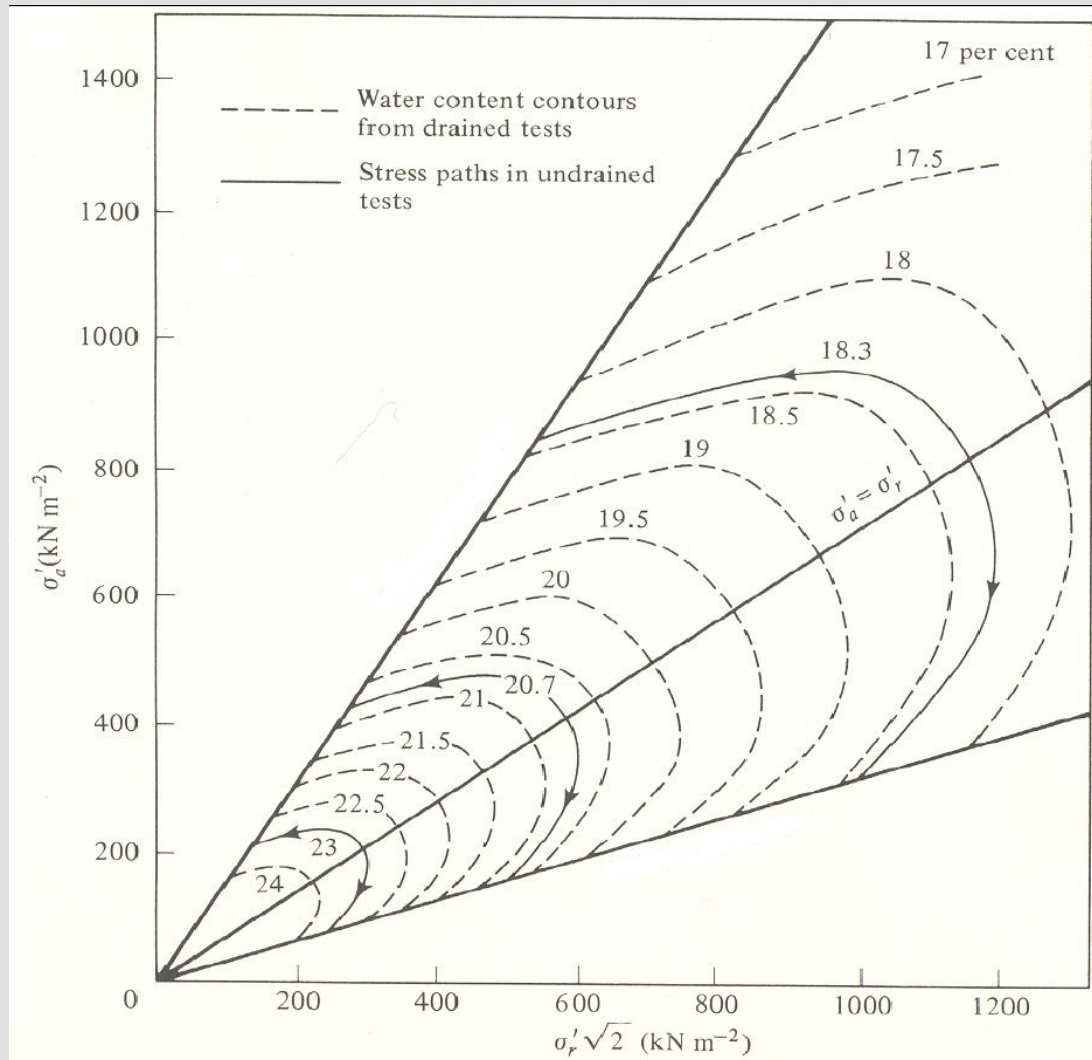
shear hardening and volumetric hardening surfaces active

## DESCRIPTION OF HARDENING SOIL MODEL



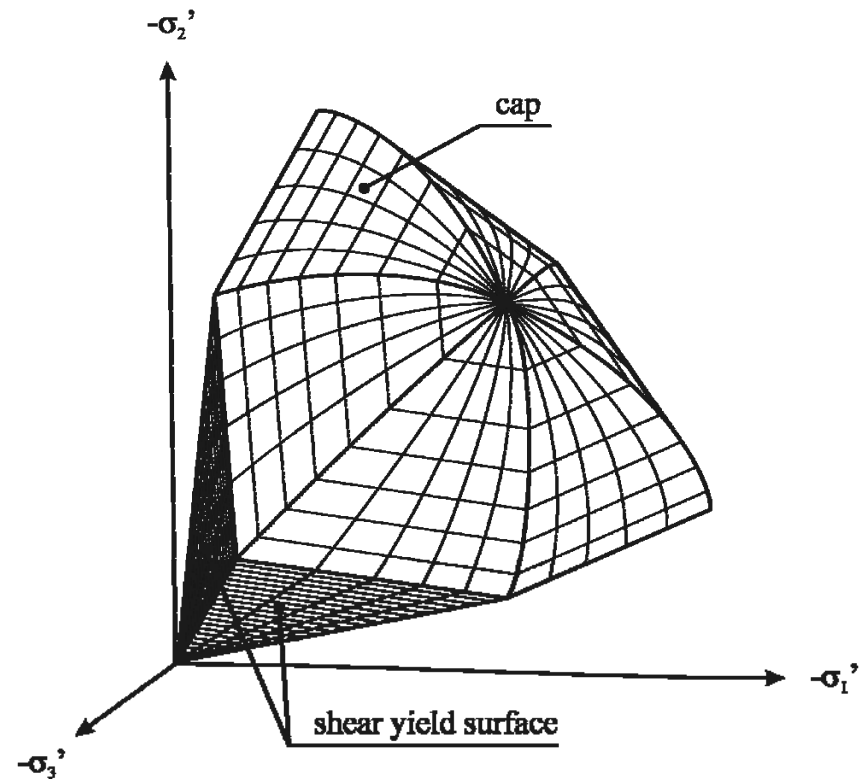
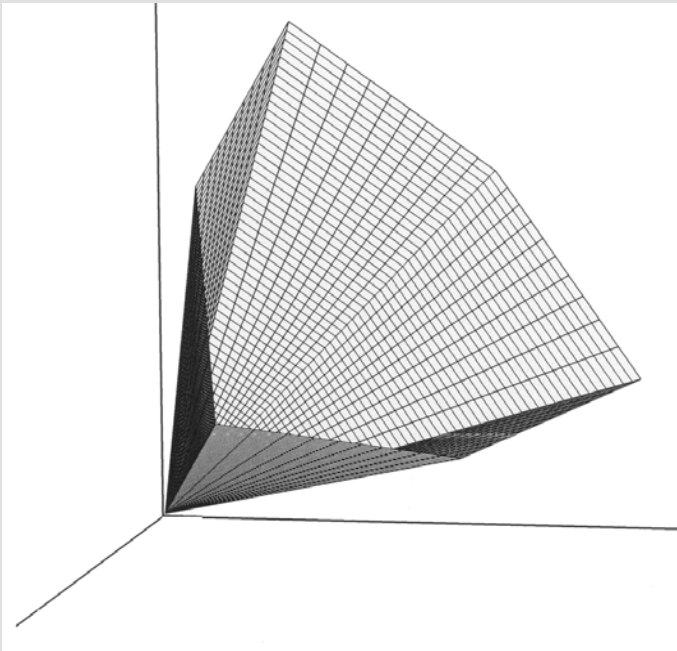
REGION 4  
volumetric hardening surface active

## DESCRIPTION OF HARDENING SOIL MODEL



**Volumetric yield surface:  
lines of equal volumetric strains in  
triaxial test**

## DESCRIPTION OF HARDENING SOIL MODEL



## DESCRIPTION OF HARDENING SOIL MODEL

$$E_{50} = E_{50}^{ref} \cdot \left( \frac{c \cdot \cot \varphi + \sigma'_3}{c \cdot \cot \varphi + p^{ref}} \right)^m$$

$$E_{ur} = E_{ur}^{ref} \cdot \left( \frac{c \cdot \cot \varphi + \sigma'_3}{c \cdot \cot \varphi + p^{ref}} \right)^m$$

$$E_{oed} = E_{oed}^{ref} \cdot \left( \frac{c \cdot \cot \varphi + \sigma'_1}{c \cdot \cot \varphi + p^{ref}} \right)^m$$

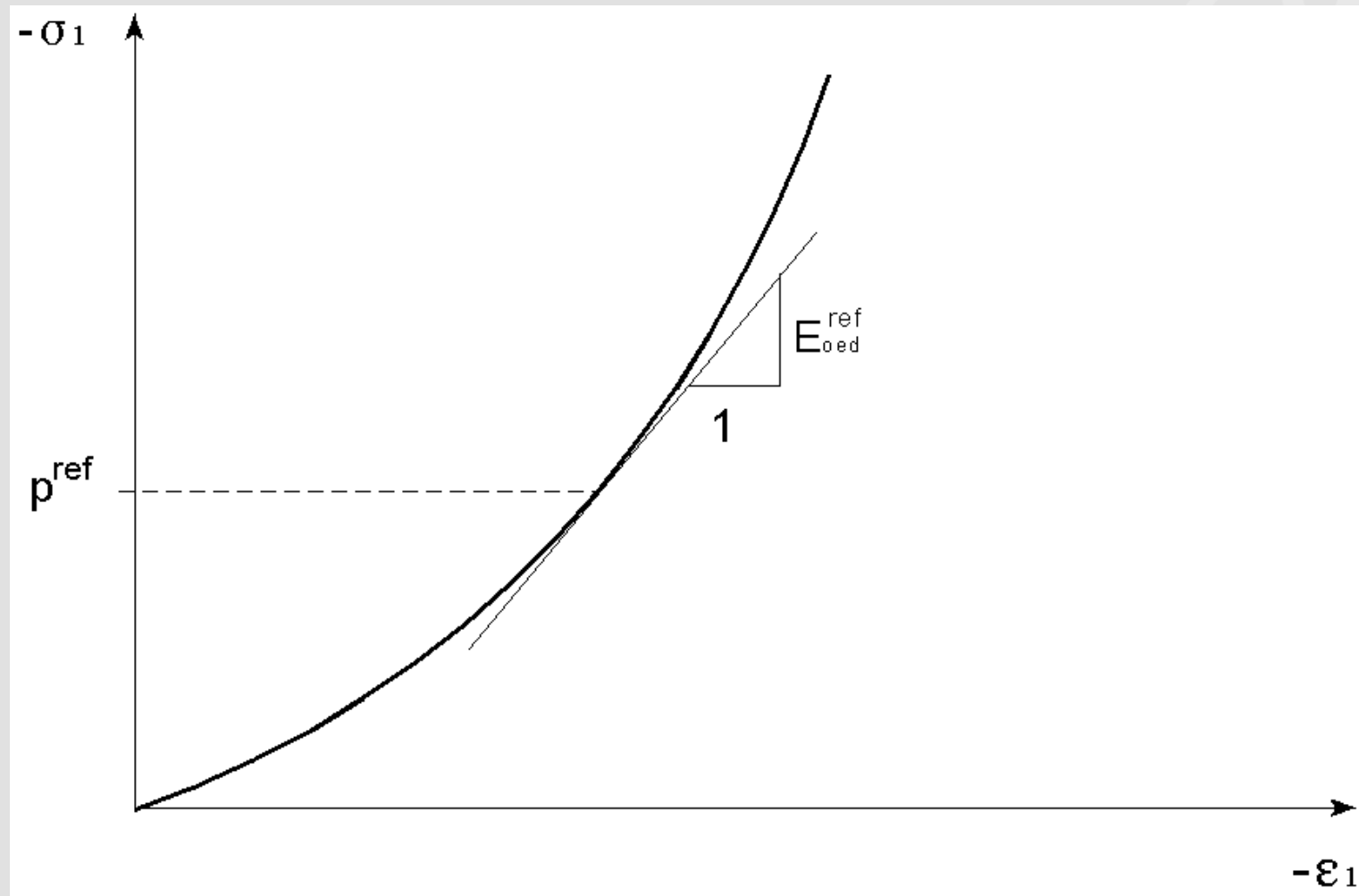
← holds strictly for  $K_0$ -stress paths only

**$p^{ref}$ :**

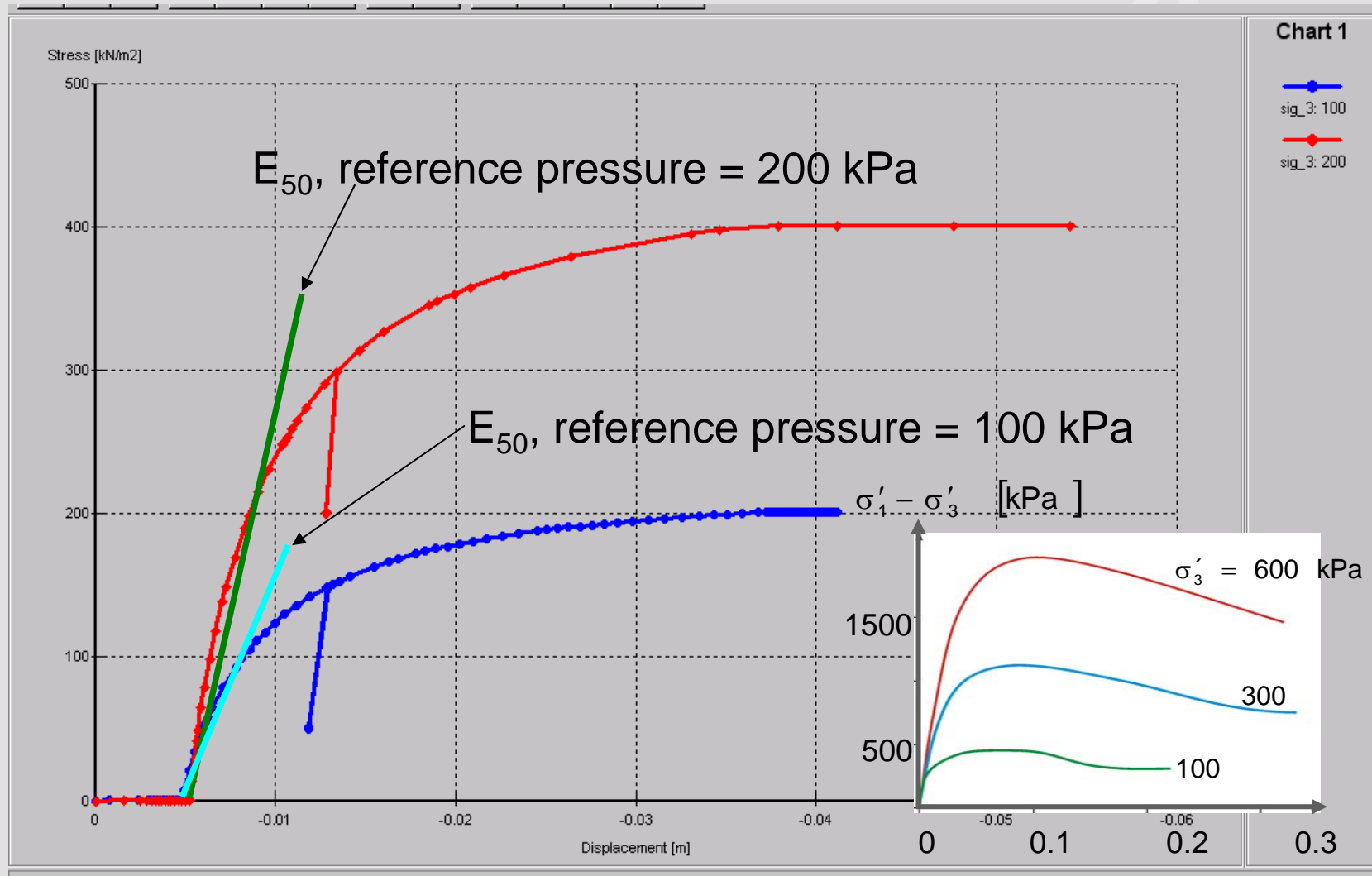
$\sigma_3$  for  $E_{50}$

$\sigma_1$  for  $E_{oed}$

## DESCRIPTION OF HARDENING SOIL MODEL



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### Volumetric behaviour

#### "stress dilatancy theory" (Rowe, 1962)

$$\dot{\varepsilon}_v^P = \sin \psi_m \dot{\gamma}^P$$

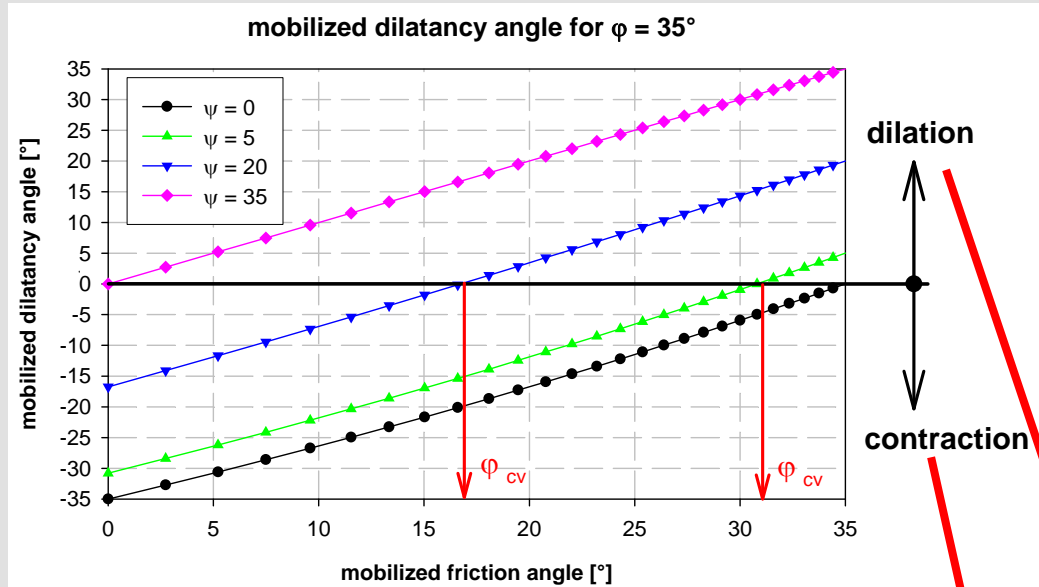
dilatancy angle > non-associated flow rule

$$\sin \psi_m = \frac{\sin \varphi_m - \sin \varphi_{cv}}{1 - \sin \varphi_m \sin \varphi_{cv}}$$

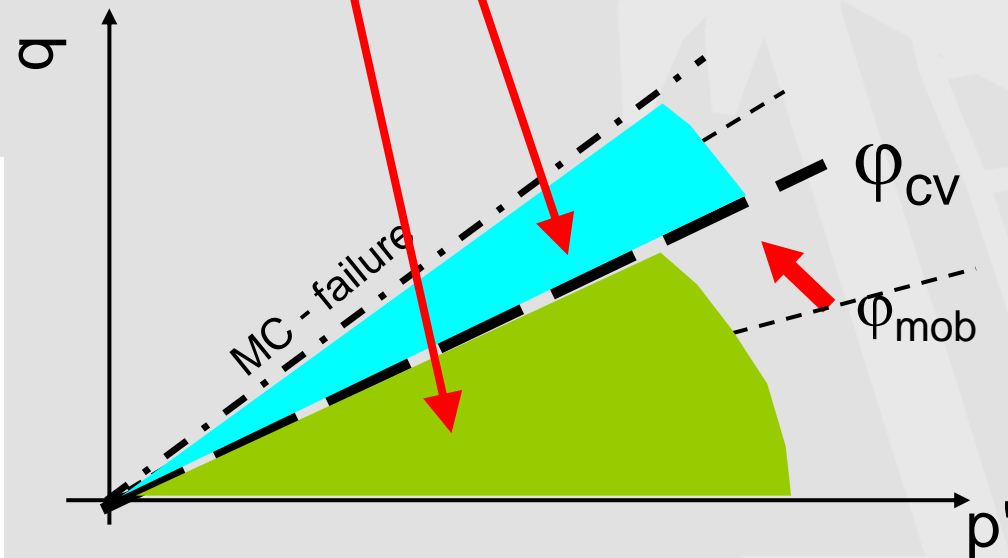
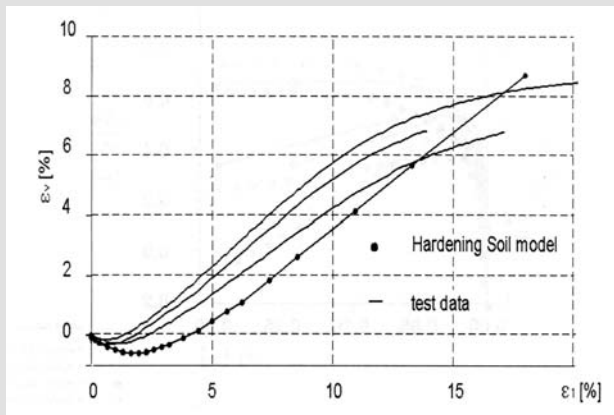
$$\sin \varphi_m = \frac{\sigma_1' - \sigma_3'}{\sigma_1' + \sigma_3' - 2c \cdot \cot \varphi}$$

$$\sin \varphi_{cv} = \frac{\sin \varphi - \sin \psi}{1 - \sin \varphi \sin \psi}$$

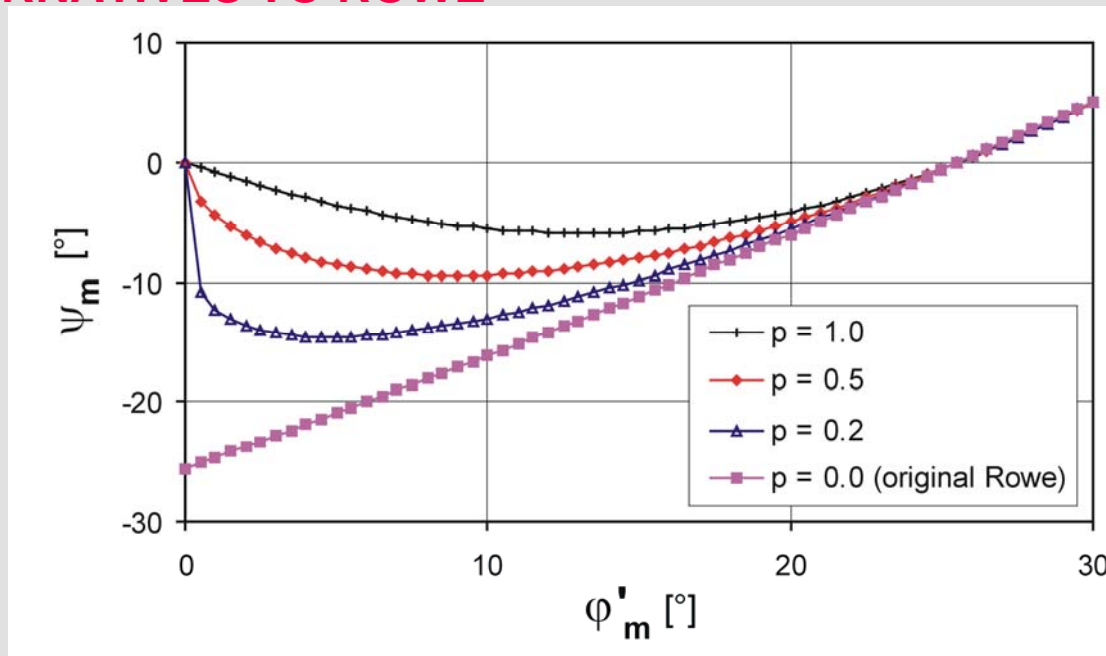
# DESCRIPTION OF HARDENING SOIL MODEL



in reality negative values of  $\psi$  are cut-off in Plaxis

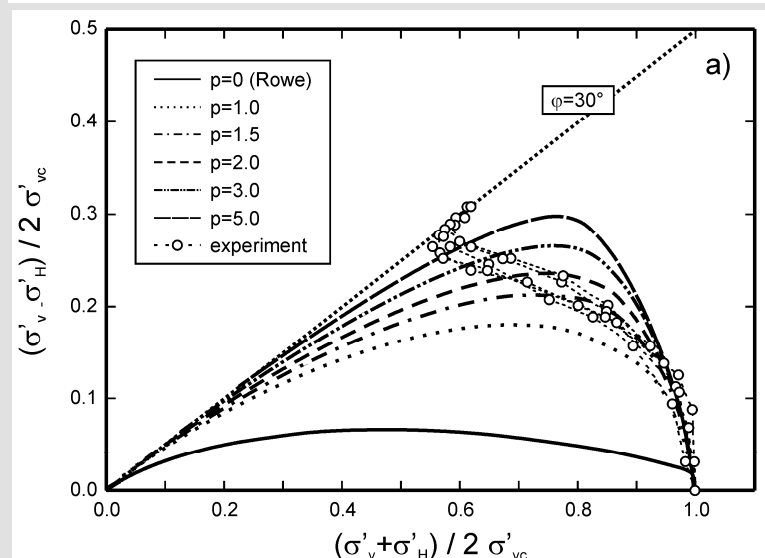


## ALTERNATIVES TO ROWE



$$\sin \hat{\psi}_m = \sin \psi_m \left( \frac{\sin \phi'_m}{\sin \phi'} \right)^p$$

**e.g. SOREIDE 2003**



**consequence of flow rule in  
undrained triaxial compression  
stress path**

## PARAMETERS OF HARDENING SOIL MODEL

$\varphi'$  friction angle  
 $c'$  cohesion  
 $\psi'$  dilatancy angle

$E_{50}^{ref}$  **secant modulus from triaxial test** (controls deviatoric hardening)

$E_{oed}^{ref}$  **tangential modulus from oedometer test**  
(controls volumetric hardening)

$E_{ur}^{ref}$  **unloading / reloading modulus**

default:  $E_{ur}^{ref} = 3 E_{50}^{ref}$

$m$  **power for stress dependency of stiffness**

## PARAMETERS OF HARDENING SOIL MODEL

$\nu_{ur}$  **Poisson ratio for unloading / reloading** (default  $\nu_{ur} = 0.2$ )

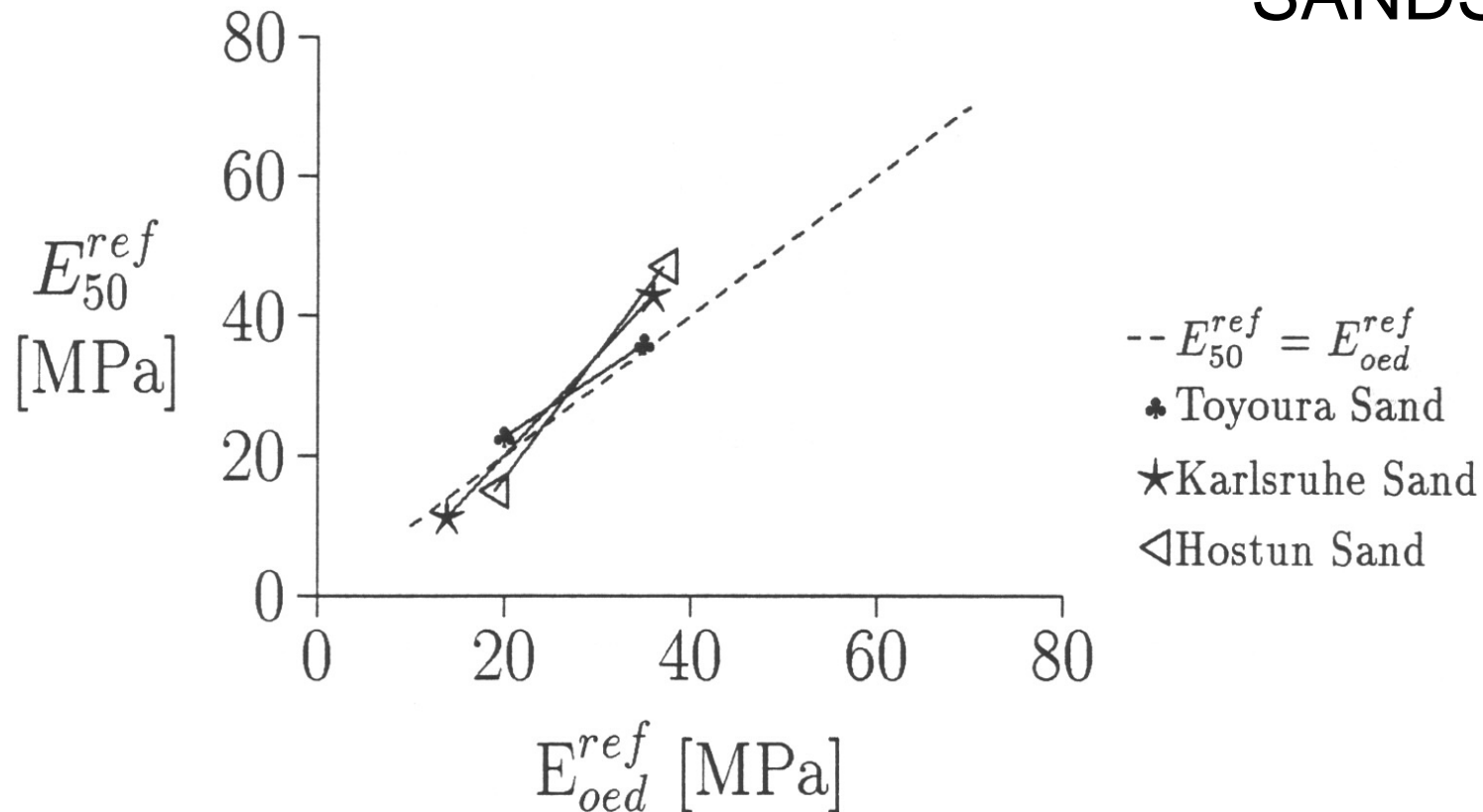
$p^{ref}$  **reference stress**  
(default  $p^{ref} = 100$  stress units)

$K_0^{nc}$   **$K_0$ -value for normal consolidation** (default  $= 1 - \sin\phi$ )  
(controls volumetric hardening)

$R_f = q_f / q_a$  (default  $R_f = 0.9$ )

## PARAMETERS OF HARDENING SOIL MODEL

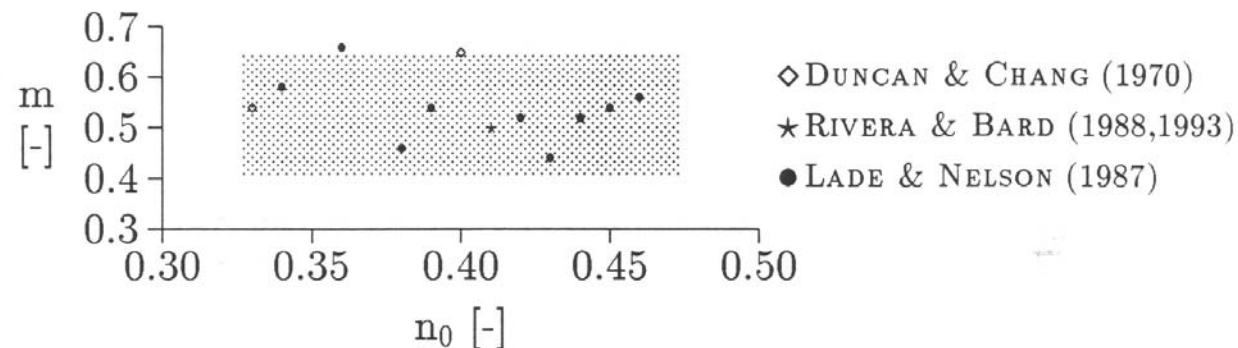
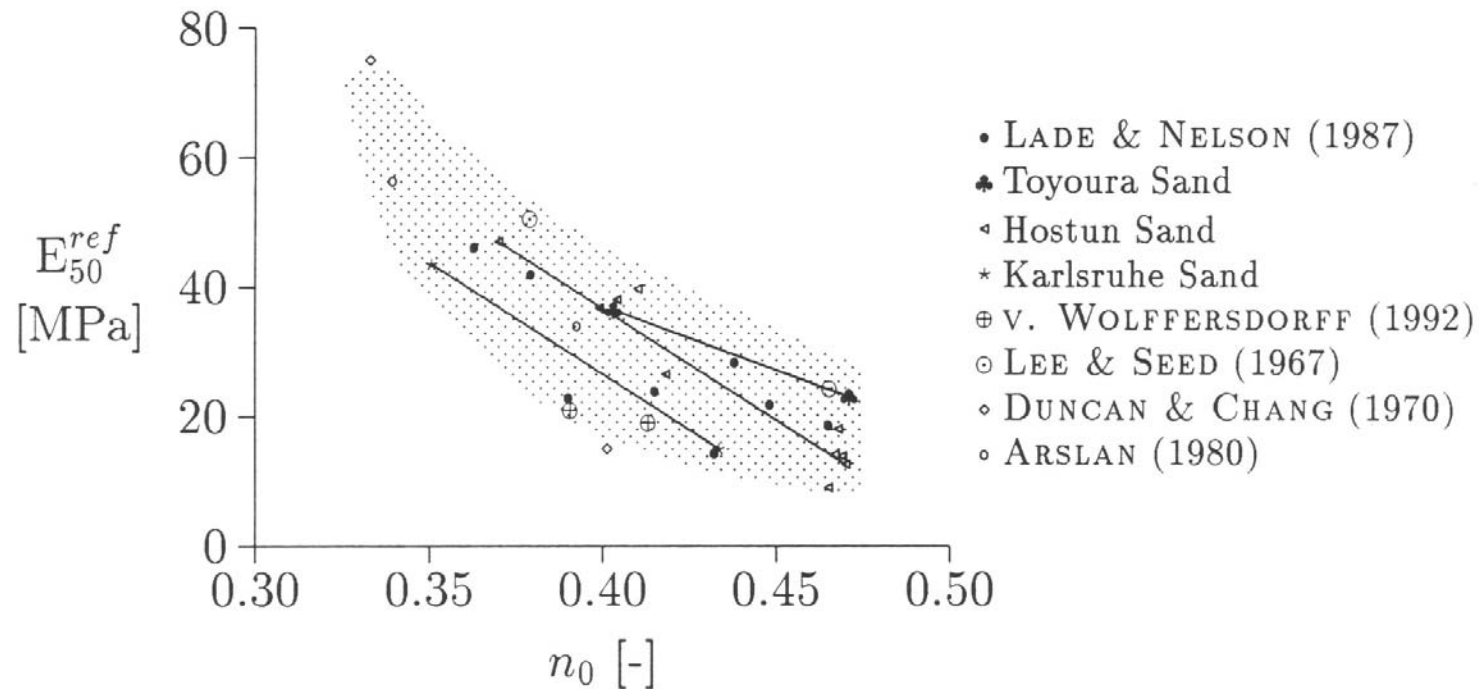
### SANDS



$$E_{oed}^{ref} \approx I_D \bullet 60MPa$$

Correlation for  $p^{ref}=100$  kPa  
(Lengkeek)  
 $I_D$  = relative density

## PARAMETERS OF HARDENING SOIL MODEL



## PARAMETERS OF HARDENING SOIL MODEL

For normally consolidated clays ( $m=1$ ):

$$E_{oed}^{ref} \approx \frac{1}{2} E_{50}^{ref}$$

Order of magnitude (very rough)

$$E_{oed}^{ref} \approx \frac{50000 \text{ kPa}}{I_p}$$

Correlation with  $I_p$  for  $p^{ref} = 100 \text{ kPa}$

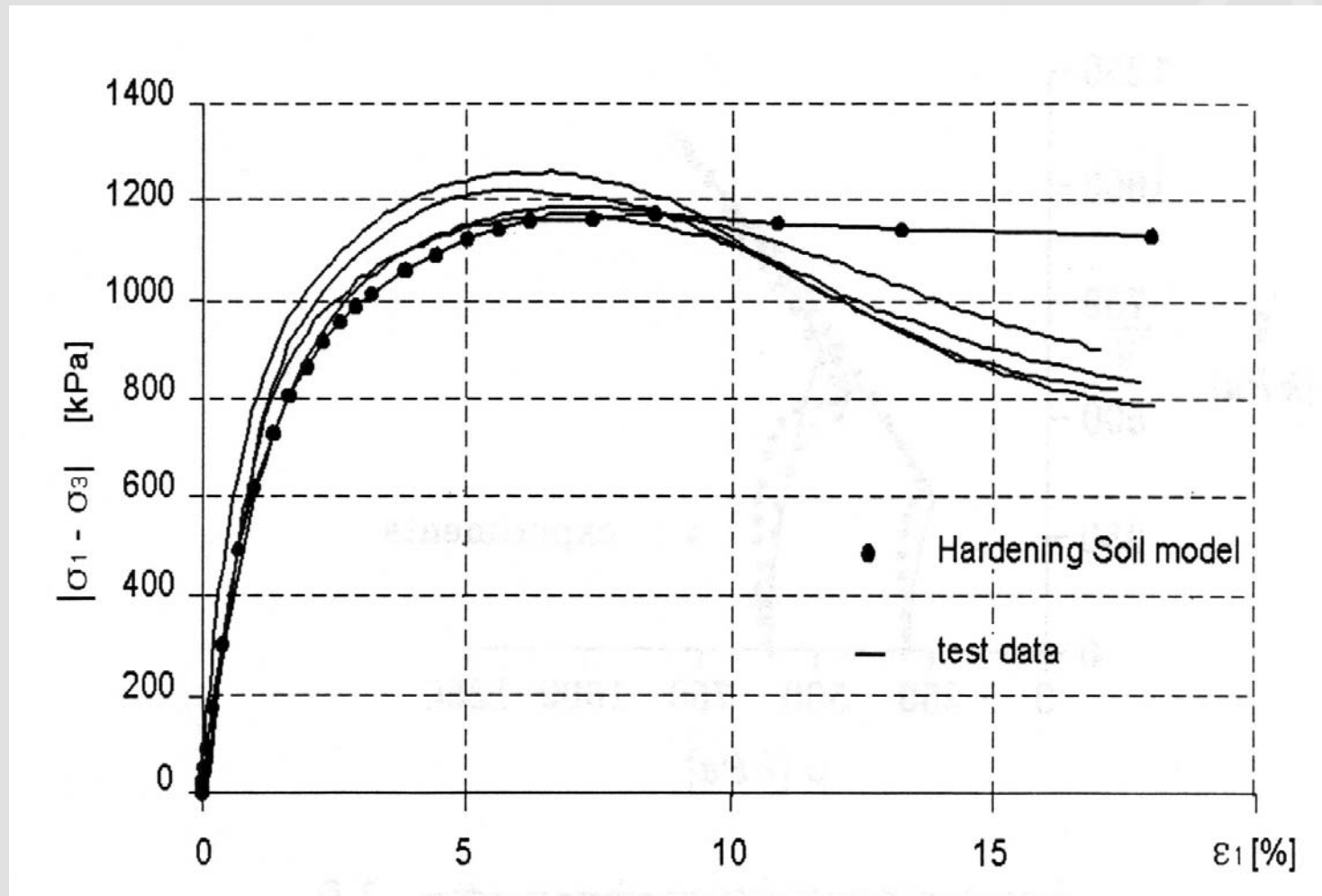
$$E_{oed}^{ref} \approx \frac{500 \text{ kPa}}{w_L - 0.1}$$

Correlation by Vermeer

$$E_{oed}^{ref} \approx p^{ref} / \lambda^*$$

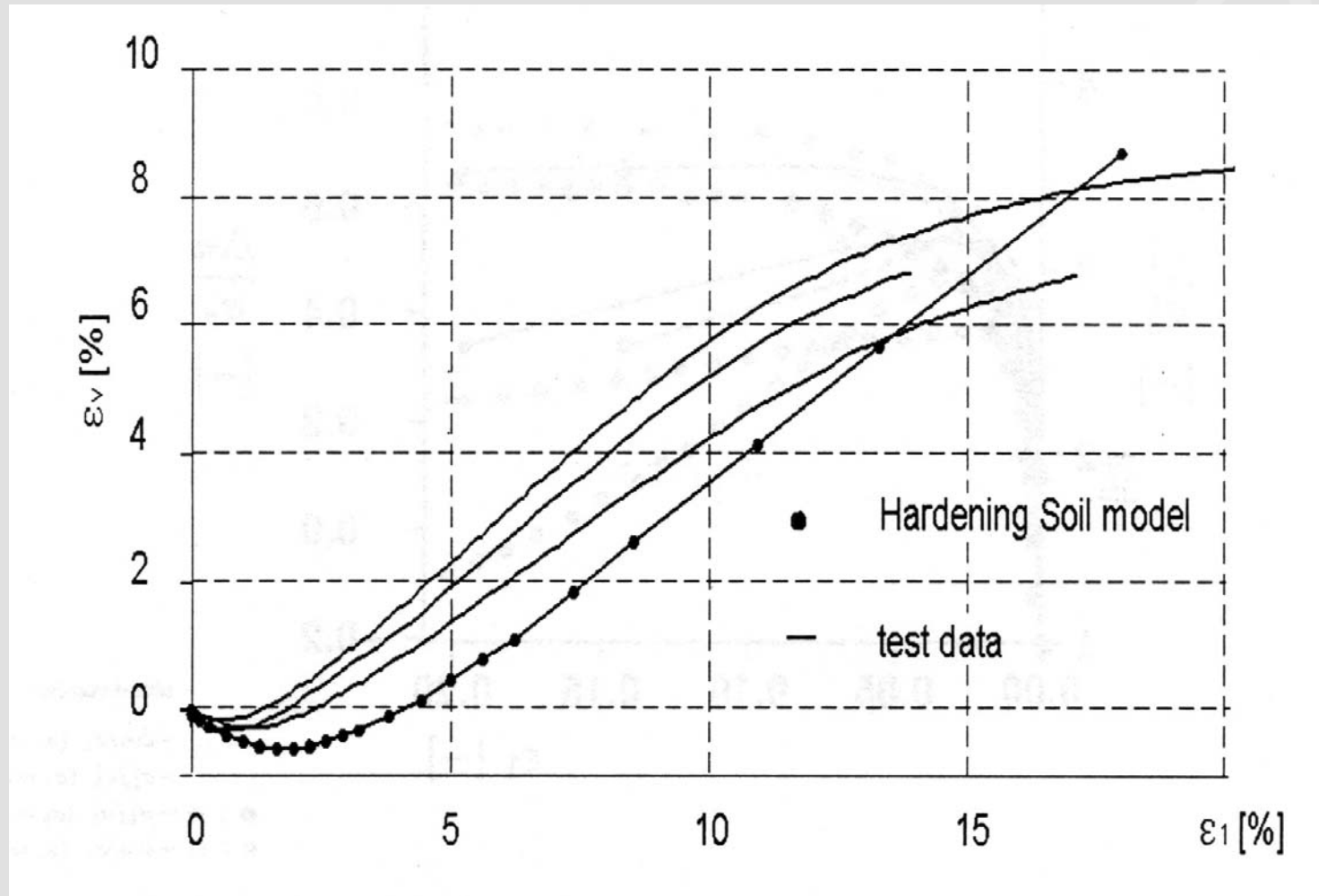
Relation with Soft Soil model

## COMPARISON WITH EXPERIMENTAL DATA



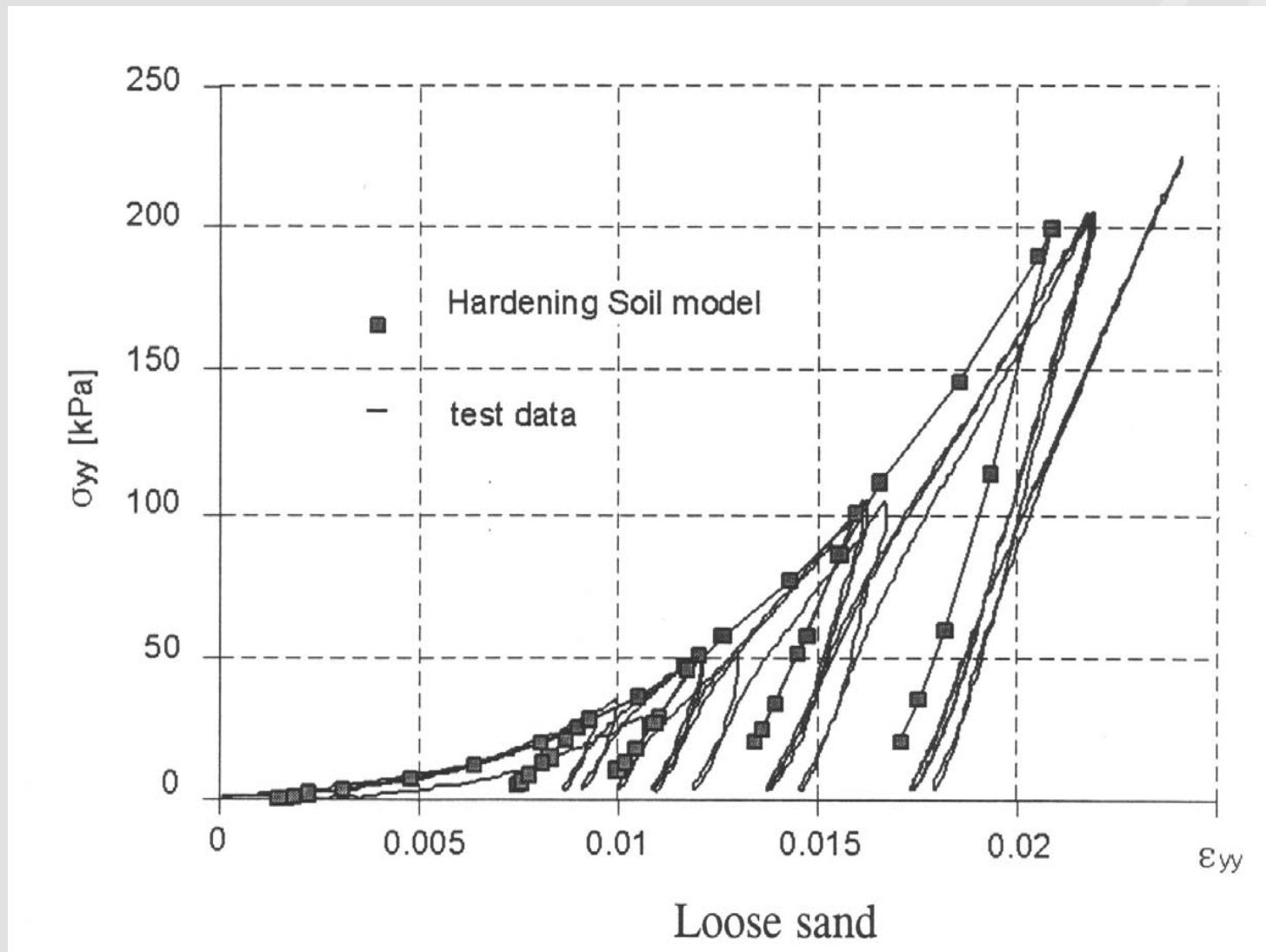
**dense Hostun sand**

## COMPARISON WITH EXPERIMENTAL DATA

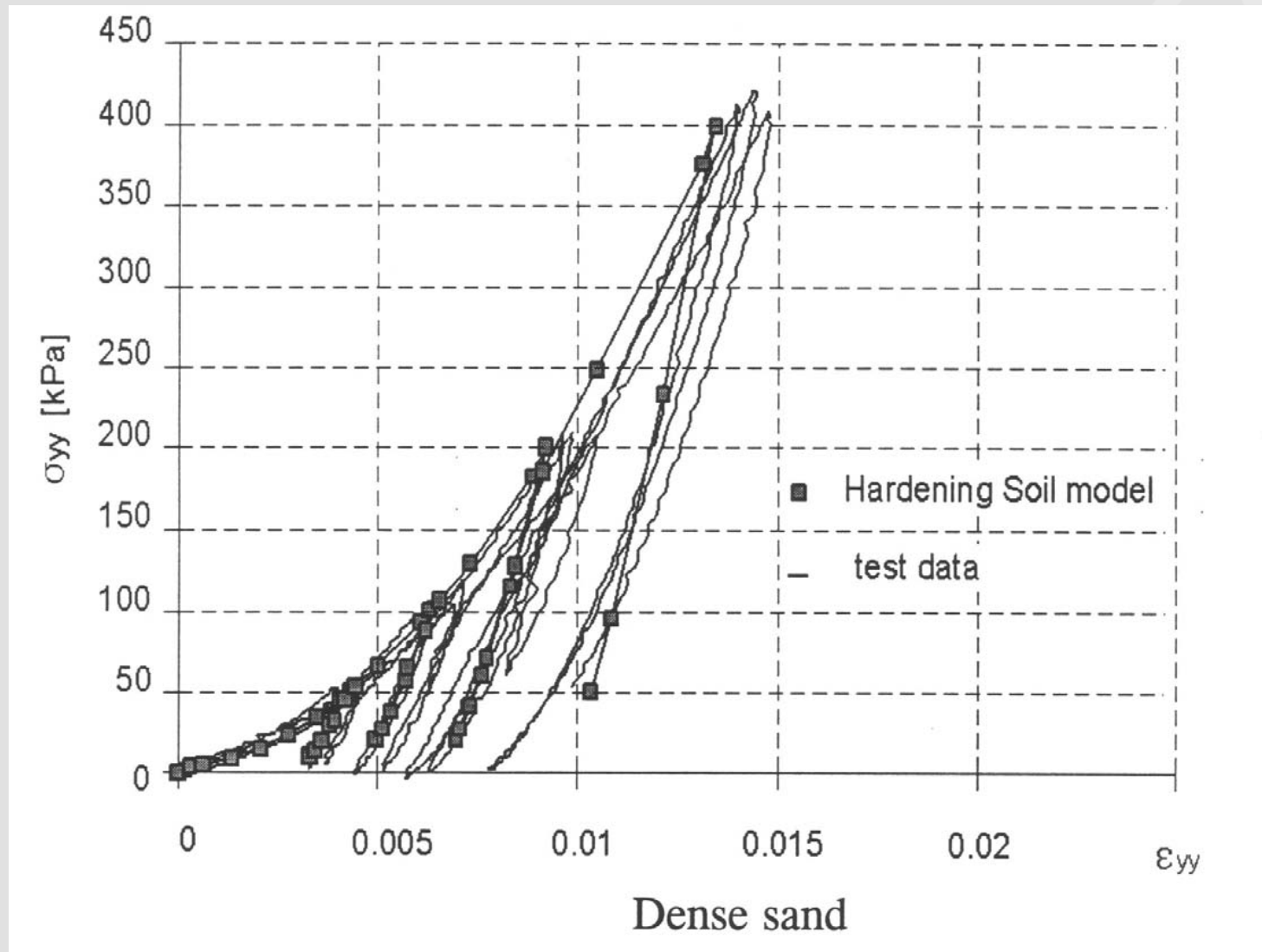


**dense Hostun sand**

## COMPARISON WITH EXPERIMENTAL DATA



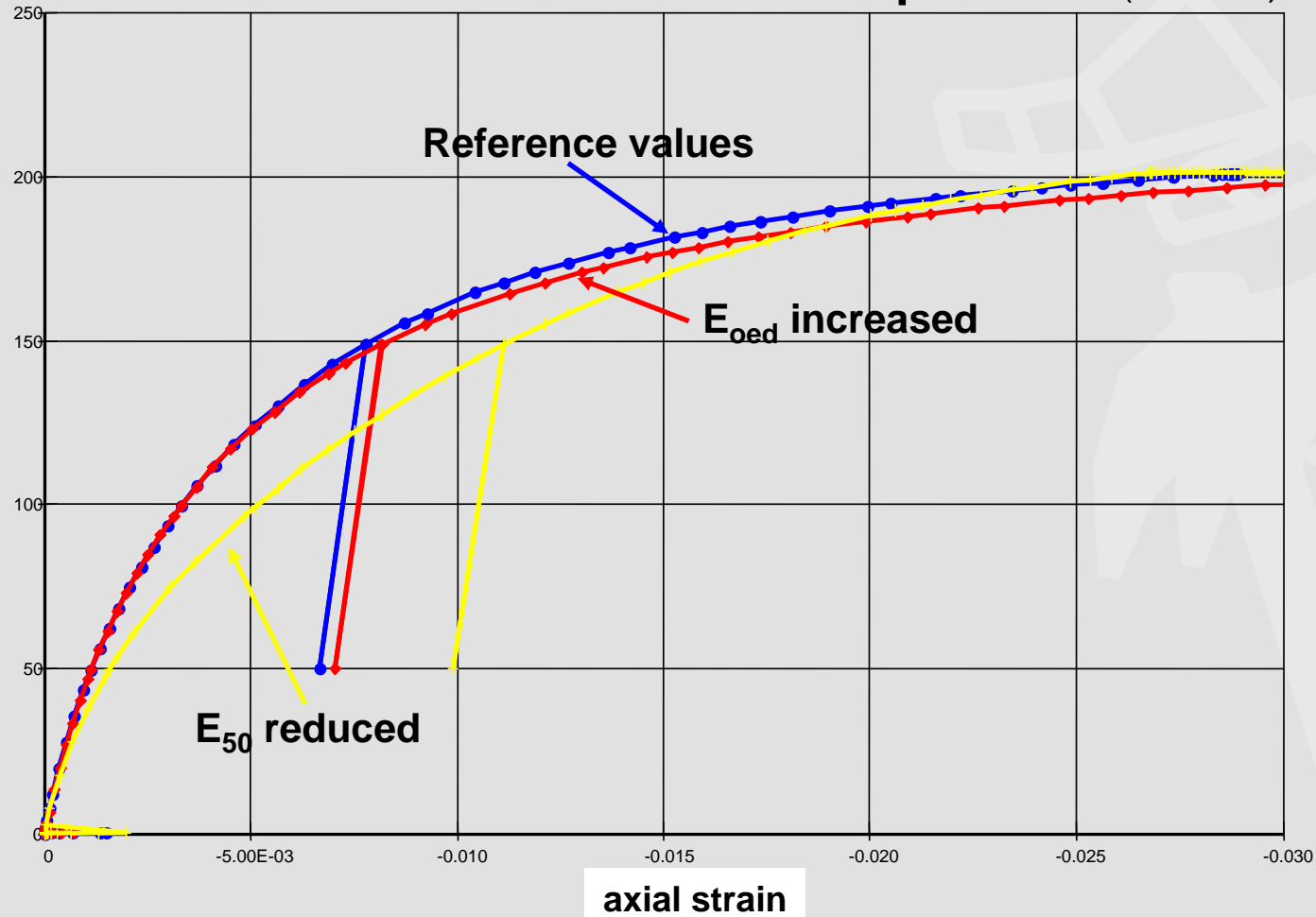
## COMPARISON WITH EXPERIMENTAL DATA



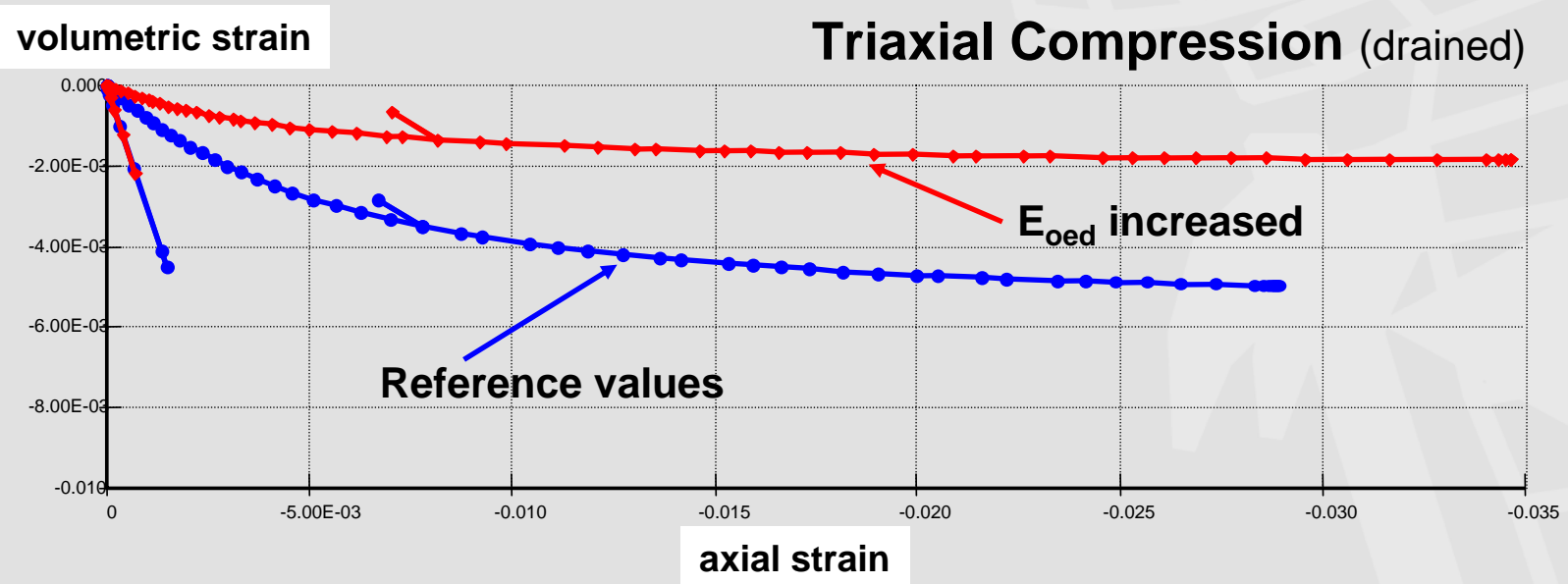
**INFLUENCE  $E_{50} / E_{oed}$**

deviatoric stress

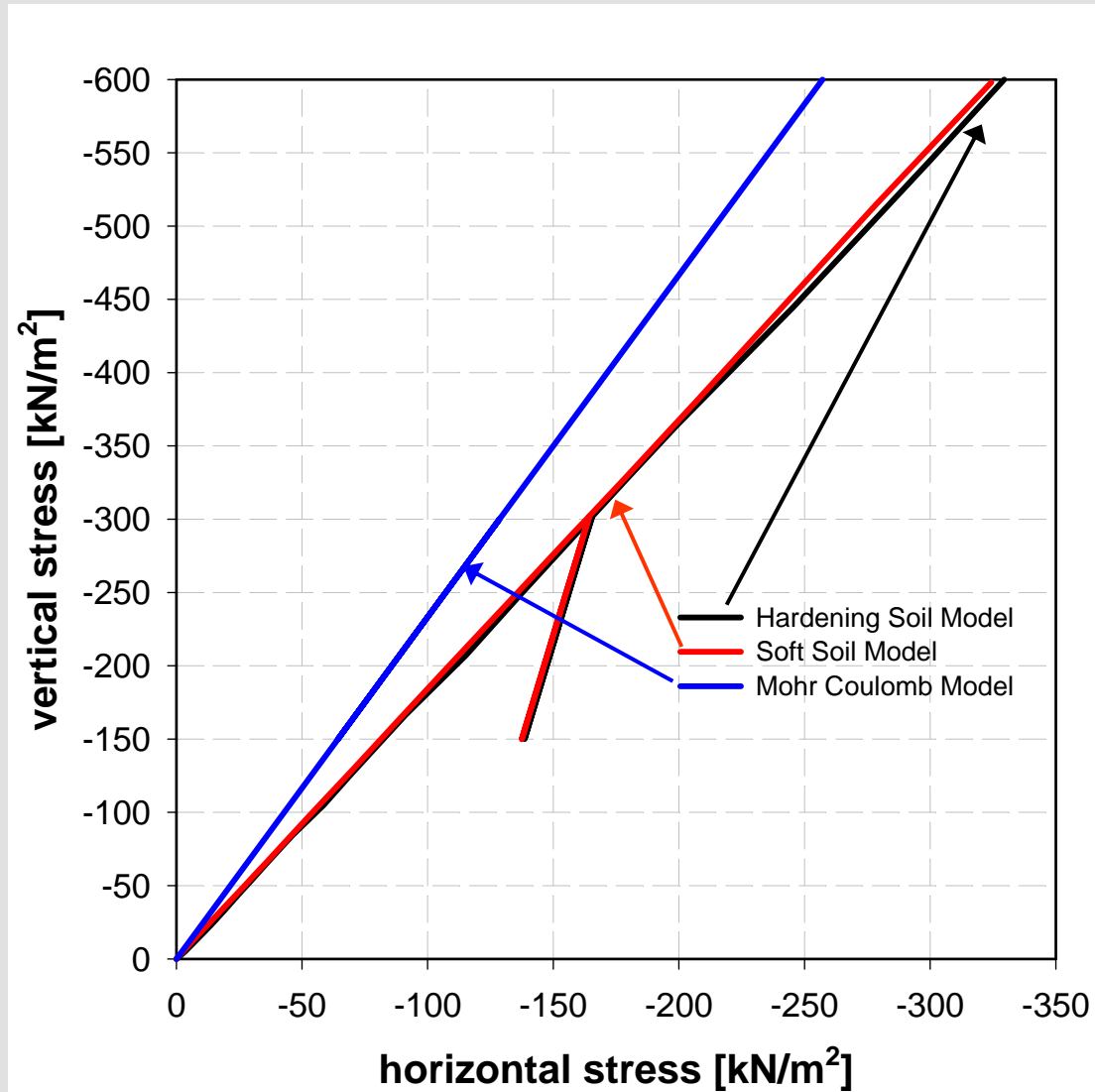
**Triaxial Compression (drained)**



## INFLUENCE $E_{50} / E_{oed}$



## OEDOMETER TEST - COMPARISON MC / SS / HS

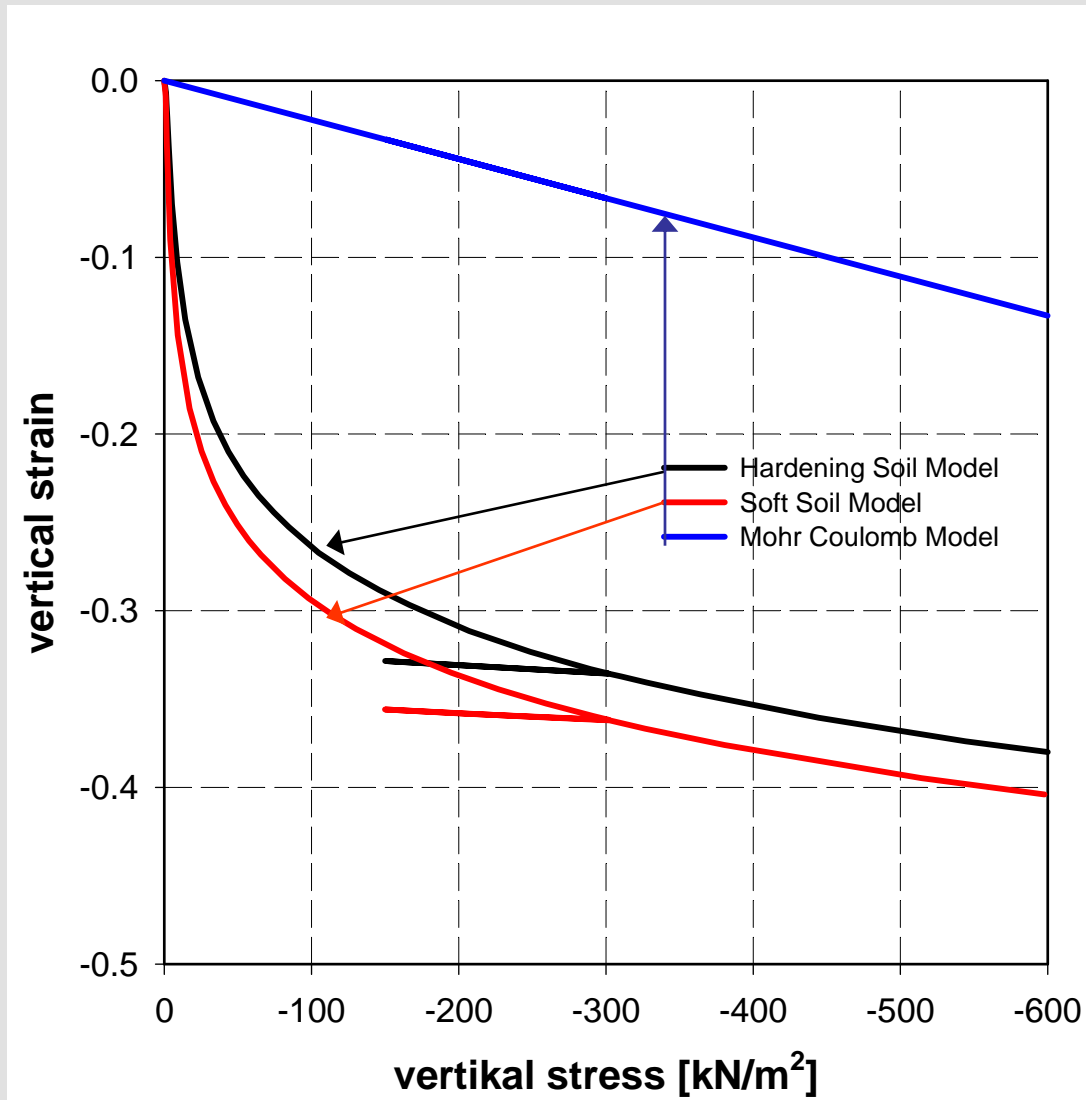


**Mohr-Coulomb:**  
ratio  $\sigma_3/\sigma_1$  determined by  $\nu$

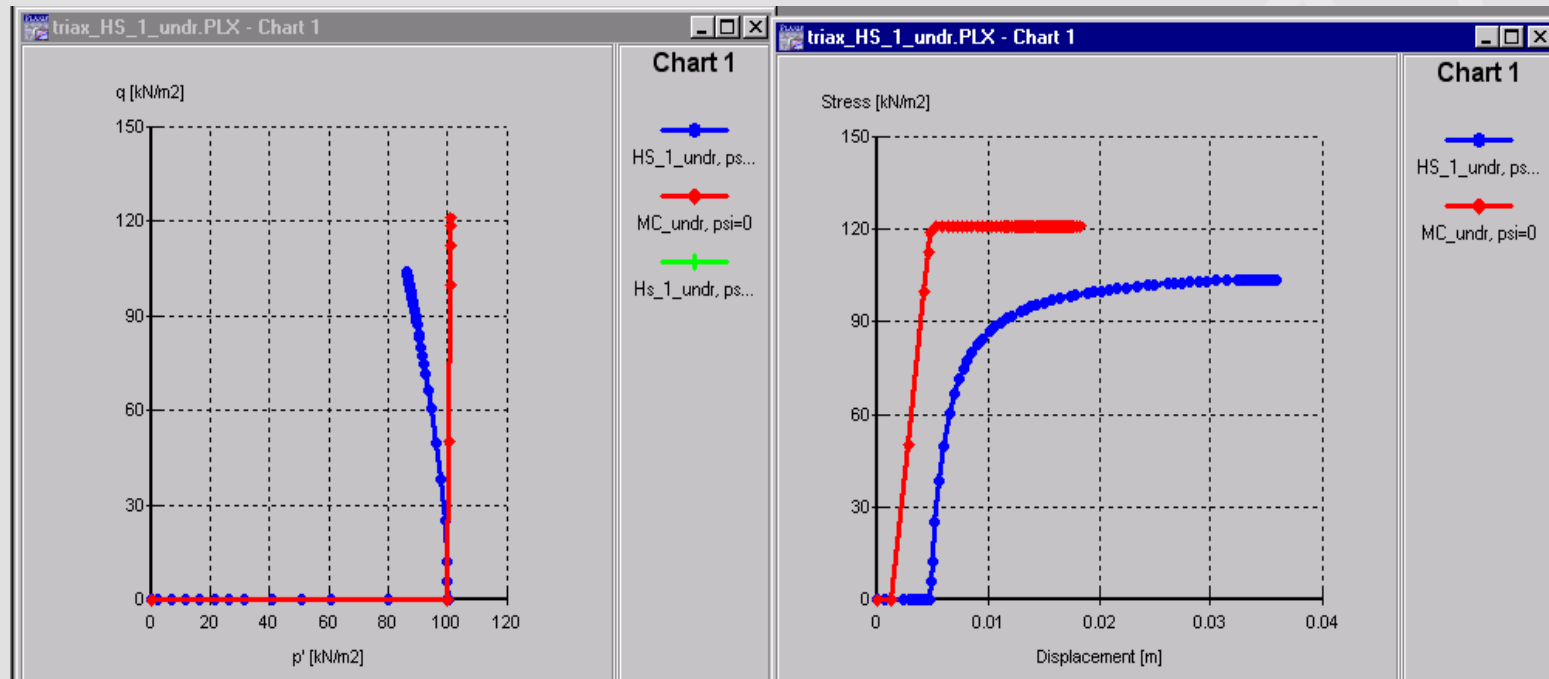
**Hardening Soil:**  
ratio  $\sigma_3/\sigma_1$  determined  
by  $K_0^{nc}$

Unloading:  $\nu_{ur}$

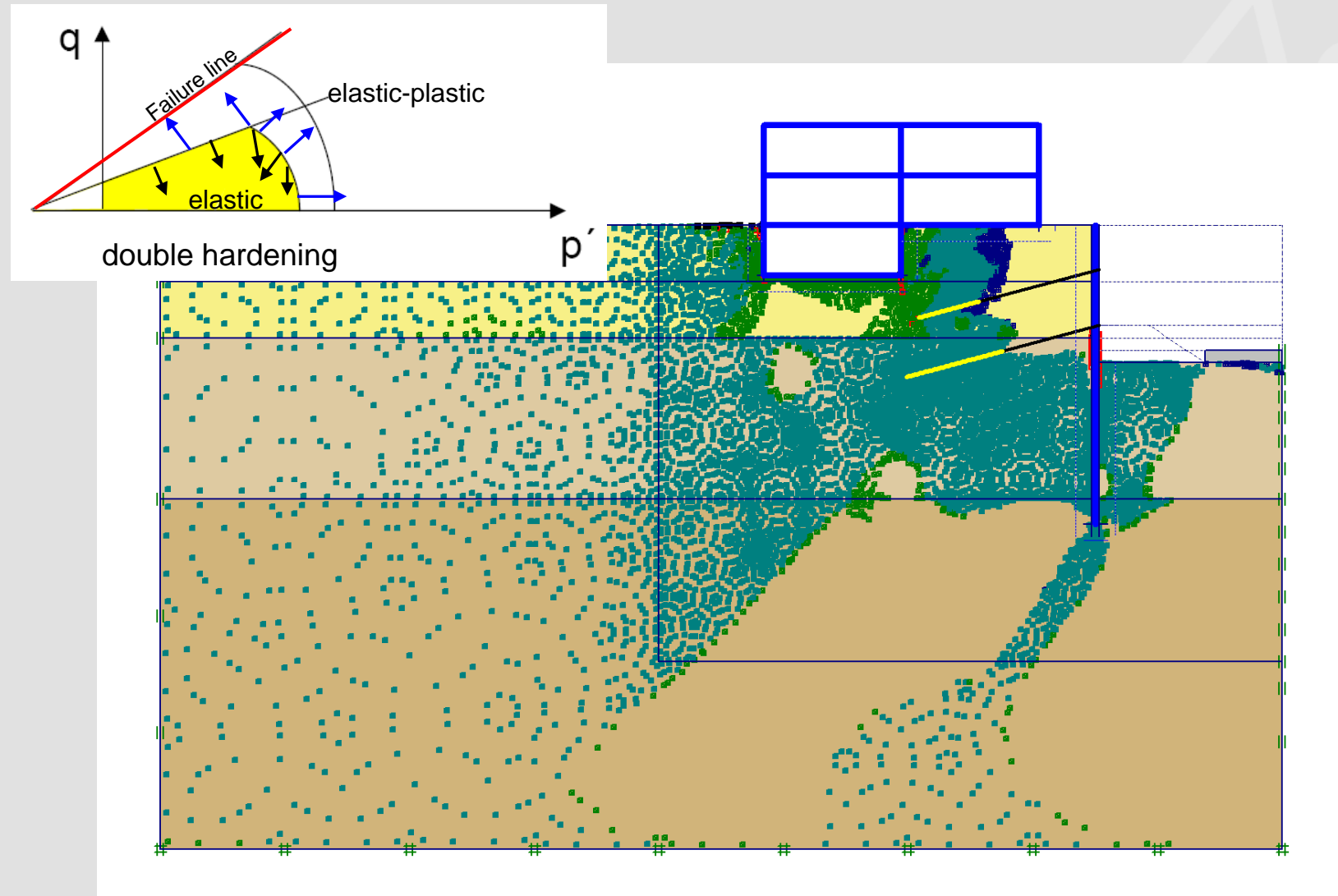
## OEDOMETER TEST - COMPARISON MC / SS / HS



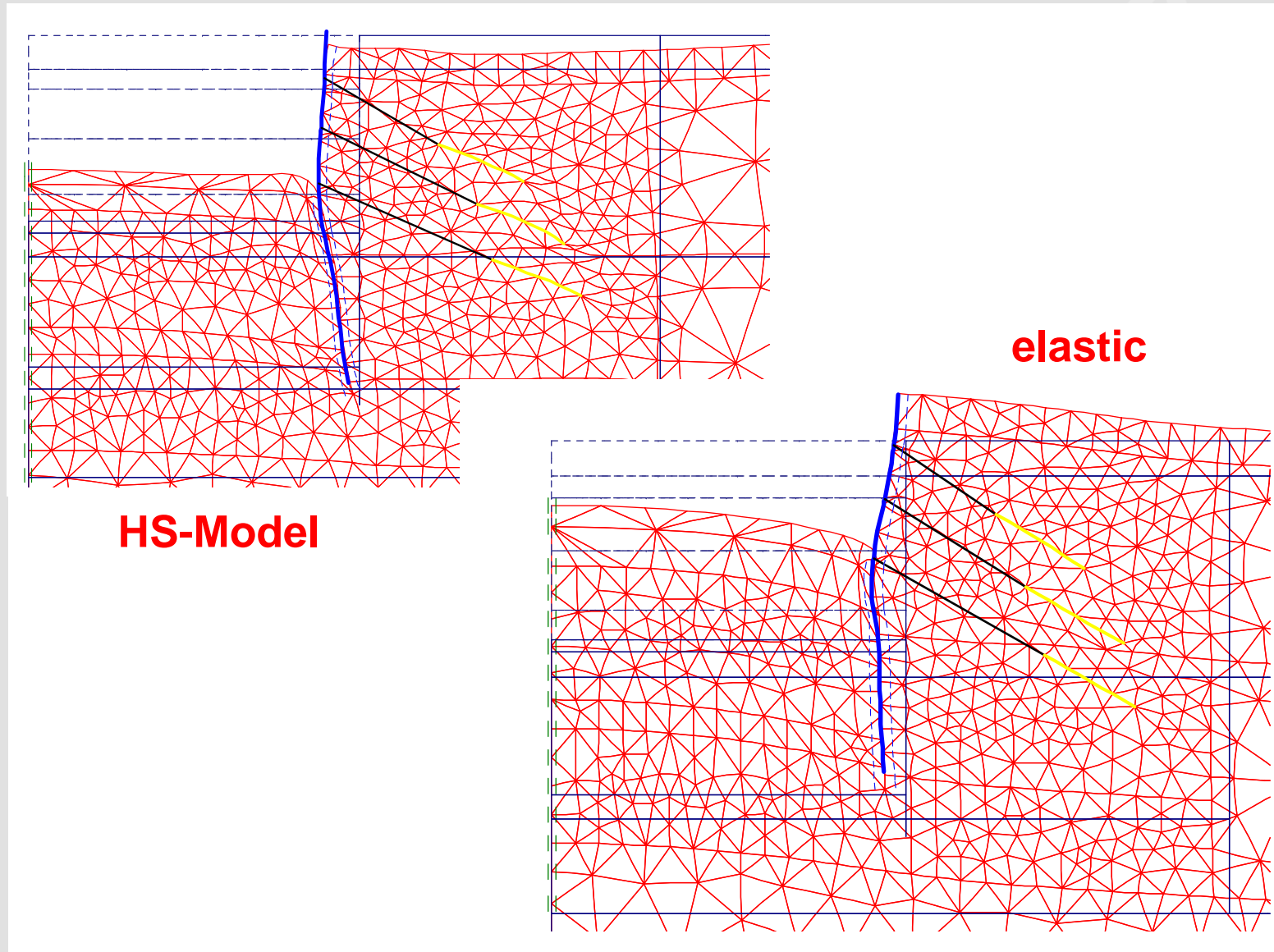
## UNDRAINED BEHAVIOUR



## PLASTIC POINTS



## SUMMARY



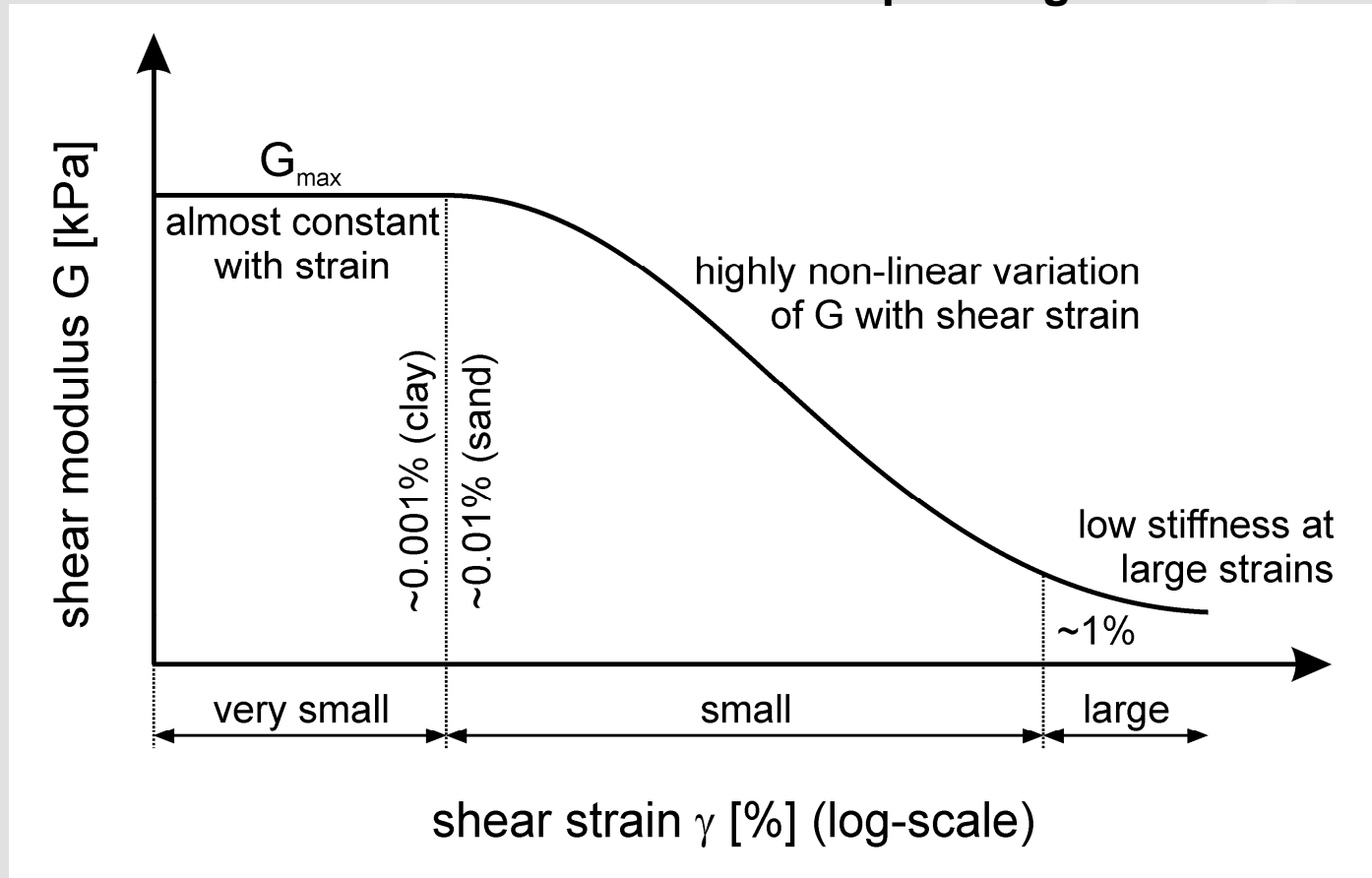
## SUMMARY

	Mohr-Coulomb Model	Hardening Soil Model
stress dependent stiffness*	NO	YES
distinction in stiffness for primary loading and unloading / reloading	NO	YES
plastic strains for stress states below MC - failure line (deviatoric and volumetric hardening)	NO	YES
failure according to Mohr-Coulomb	YES	YES

\* (not only dependent on  $\sigma_0$ , this is possible also with MC-Model)

## FURTHER DEVELOPMENTS

### HS-small: extension of HS model incorporating small strain stiffness



### 2 additional parameters:

- reference shear modulus at very small strains:  $G_0^{\text{ref}}$
- shear strain at which  $G = 0.7 G_0$ :  $\gamma_{0.7}$