

3. One-dimensional model

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Constitutive modelling 1

- Stress and strain variables
- Basic features of soil response: stiffness
- Basic features of soil response: critical states
- Basic features of soil response: strength

Stress and strain variables

- triaxial apparatus: two degrees of freedom
- soil = rigid particles + voids
- importance of volume (density) changes (or their prevention)
- separate volumetric (size) and distortional (shape) effects

Stress and strain variables

- soil behaviour controlled by effective stresses
- $\sigma'_{ij} = \sigma_{ij} - u\delta_{ij}$
- axial and radial strain increments $\delta\varepsilon_a$ and $\delta\varepsilon_r$
- axial and radial effective stresses σ'_a and σ'_r

Stress and strain variables

- volumetric effects
- volumetric strain increment $\delta\varepsilon_p = \delta\varepsilon_a + 2\delta\varepsilon_r$
- work conjugate volumetric stress $p' = (\sigma'_a + 2\sigma'_r)/3$
- volumetric work increment $\delta W_v = p'\delta\varepsilon_p$

Stress and strain variables

- **distortional effects**
- **distortional stress** $q = \sigma_a - \sigma_r = F/A$
- **work conjugate distortional strain increment**
 $\delta\varepsilon_q = 2(\delta\varepsilon_a - \delta\varepsilon_r)/3$
- **distortional work increment** $\delta W_d = q\delta\varepsilon_q$

Stress and strain variables

- work done in a small increment of strain
- $\delta W = \delta W_v + \delta W_d$
- $\delta W = p' \delta \varepsilon_p + q \delta \varepsilon_q$
- $\delta W = \sigma'_a \delta \varepsilon_a + 2\sigma'_r \delta \varepsilon_r$
- separation of volumetric and distortional effects

Stress and strain variables

- **stress ratio** $\eta = q/p'$
- **equivalent to a mobilised friction** ϕ'_m
- **triaxial compression**

$$\sigma'_a/\sigma'_r = (1 + \sin \phi'_m)/(1 - \sin \phi'_m) = (3 + 2\eta)/(3 - \eta)$$

$$\sin \phi'_m = (\sigma'_a - \sigma'_r)/(\sigma'_a + \sigma'_r) = (3\eta)/(6 + \eta)$$

$$\eta = 6 \sin \phi'_m / (3 - \sin \phi'_m)$$

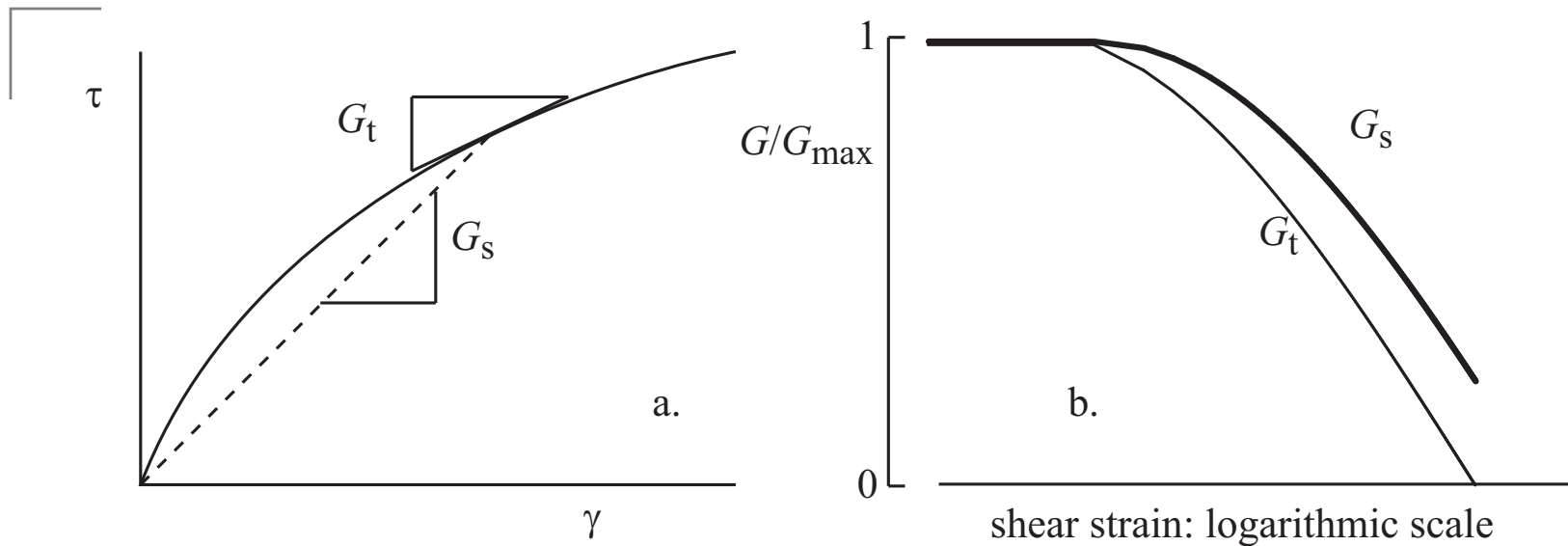
- **triaxial extension**

$$\sigma'_a/\sigma'_r = (1 - \sin \phi'_m)/(1 + \sin \phi'_m) = (3 + 2\eta)/(3 - \eta)$$

$$\sin \phi'_m = (\sigma'_r - \sigma'_a)/(\sigma'_a + \sigma'_r) = -3\eta/(6 + \eta)$$

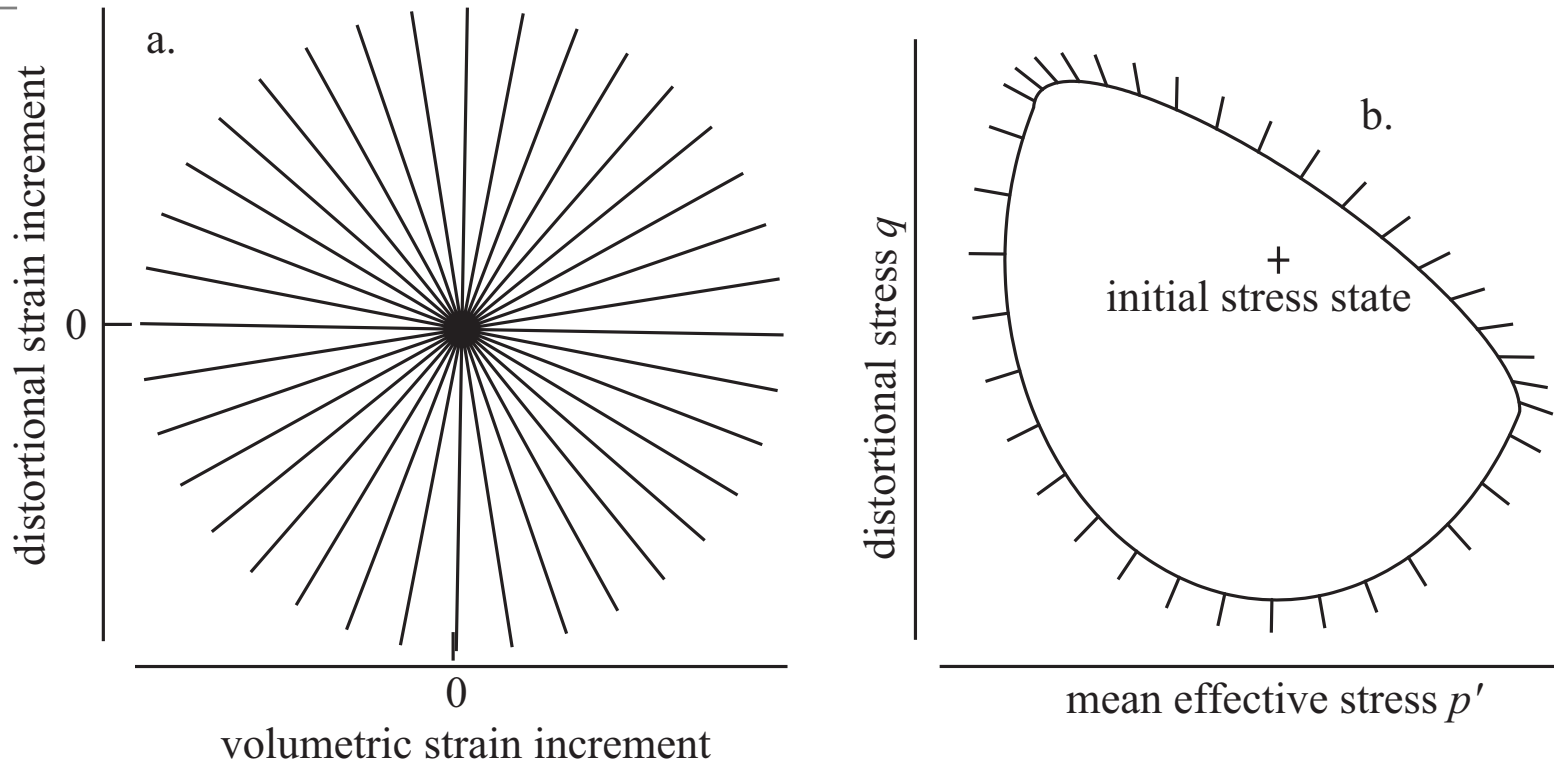
$$\eta = -6 \sin \phi'_m / (3 + \sin \phi'_m)$$

Basic features of soil response: stiffness



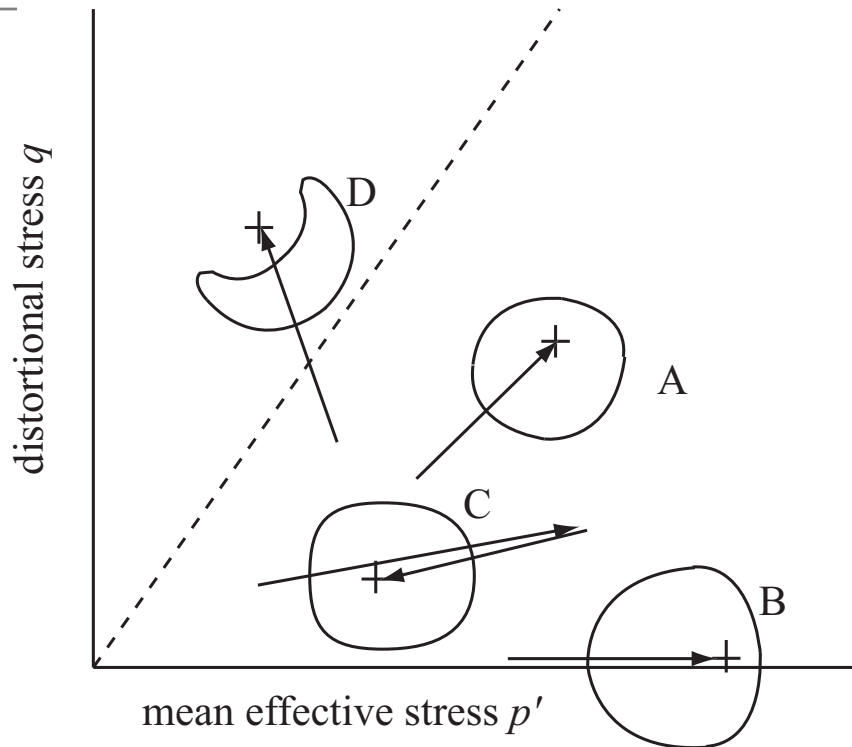
- **tangent and secant stiffness**
- **secant: past:** $G_s = \tau/\gamma$
- **tangent: future:** $G_t = \delta\tau/\delta\gamma$
- tangent (incremental) stiffness falls faster than secant (average) stiffness

Basic features of soil response: stiffness



- stress response envelope
- rosette of strain probes ...
- ... and resulting stress response envelope
- discipline for evaluating models
- discipline for planning laboratory tests

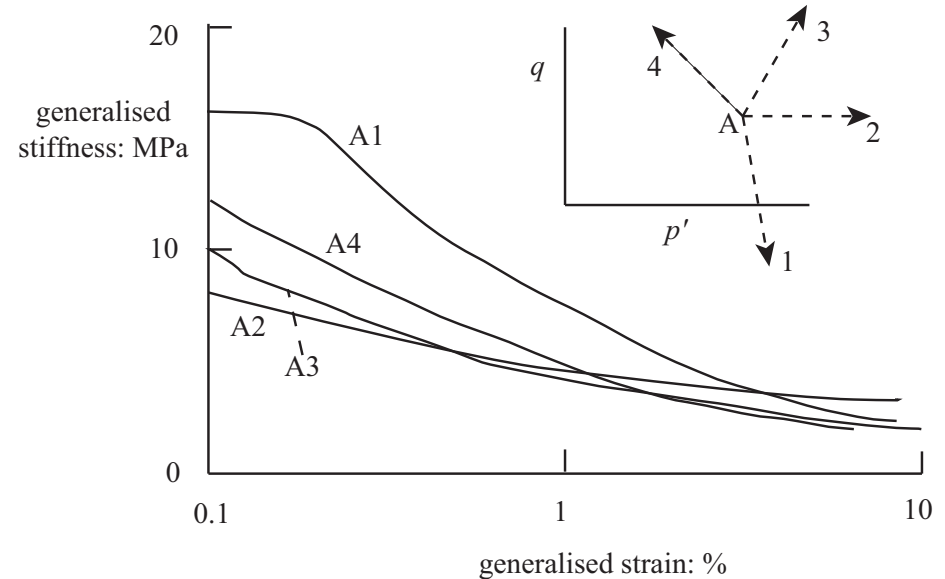
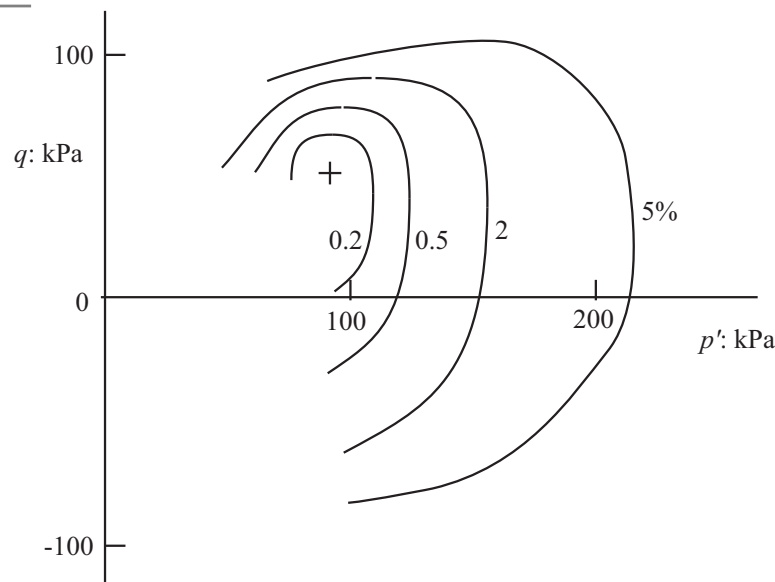
Basic features of soil response: stiffness



- history dependence of stress response envelopes
- points + indicate initial stress states

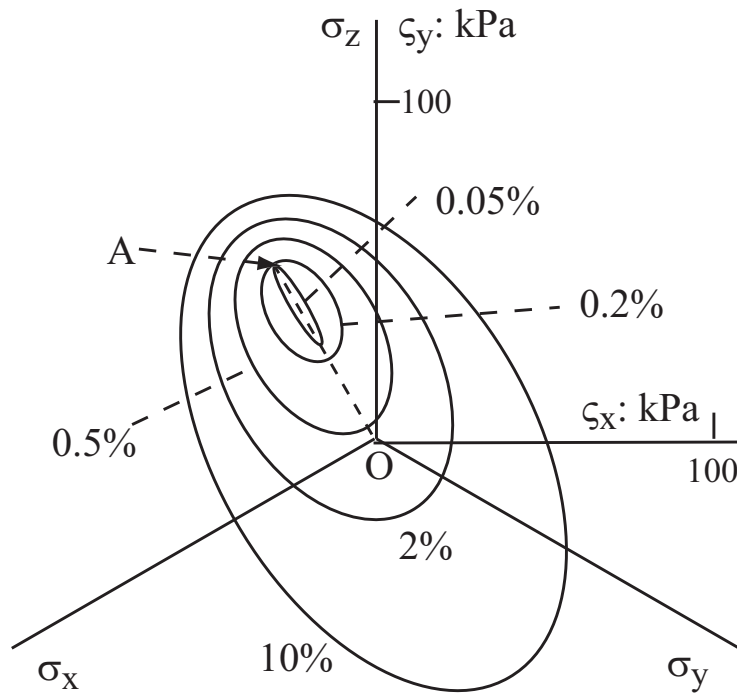
- A, B: flattened towards loading direction
- C: unloaded - response somewhat independent of direction
- D: strain softening: fall in η for all strain increments

Basic features of soil response: stiffness

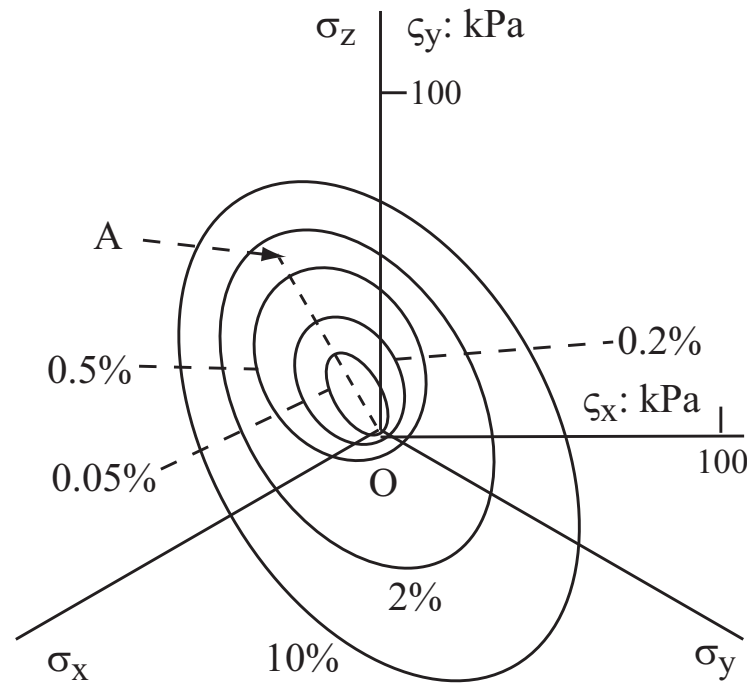


- response envelopes and generalised stiffness for Pisa clay (Callisto)
- effect of strain level
- erasure of memory

Basic features of soil response: stiffness



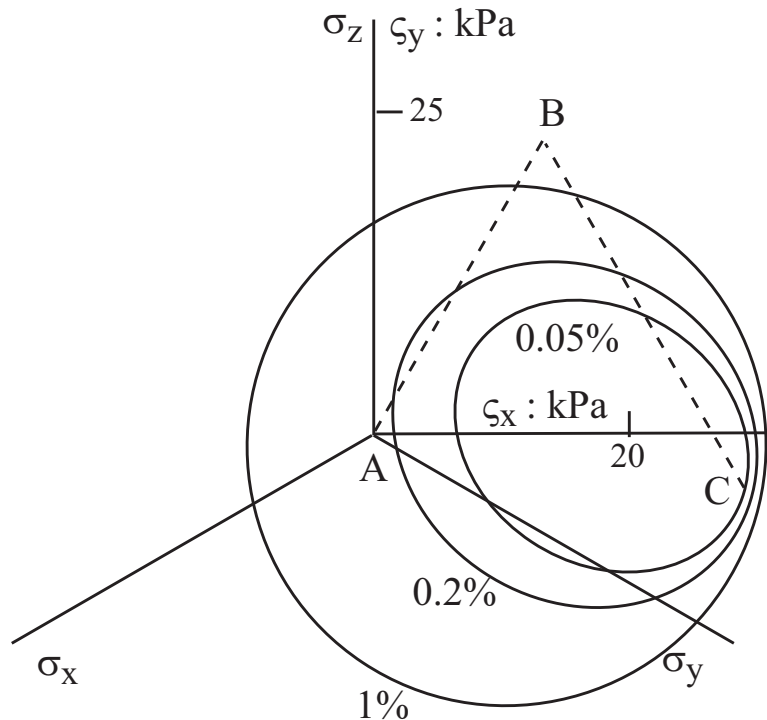
a. history OA



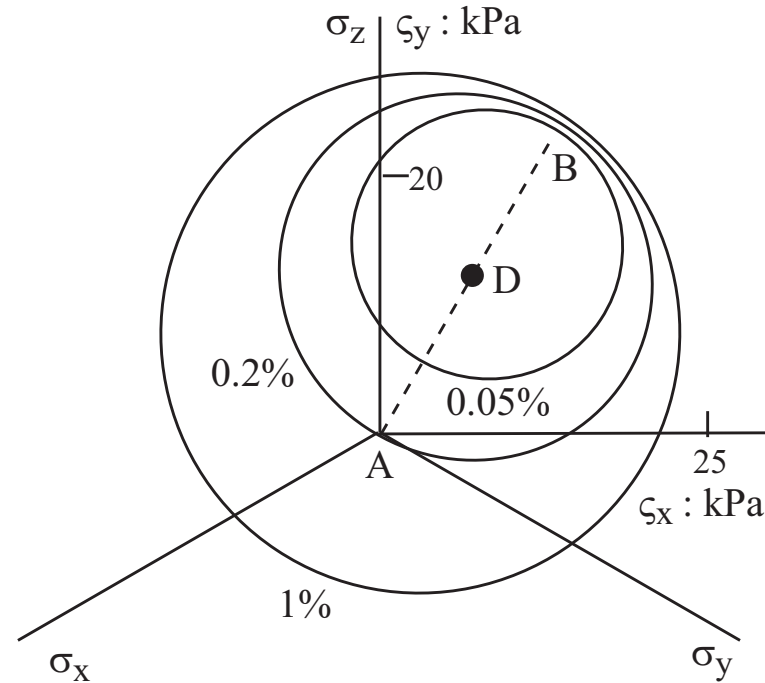
b. history OAO

- true triaxial probing of kaolin
- schematic deviatoric stress response envelopes
- deviatoric history (a) OA and (b) OAO

Basic features of soil response: stiffness



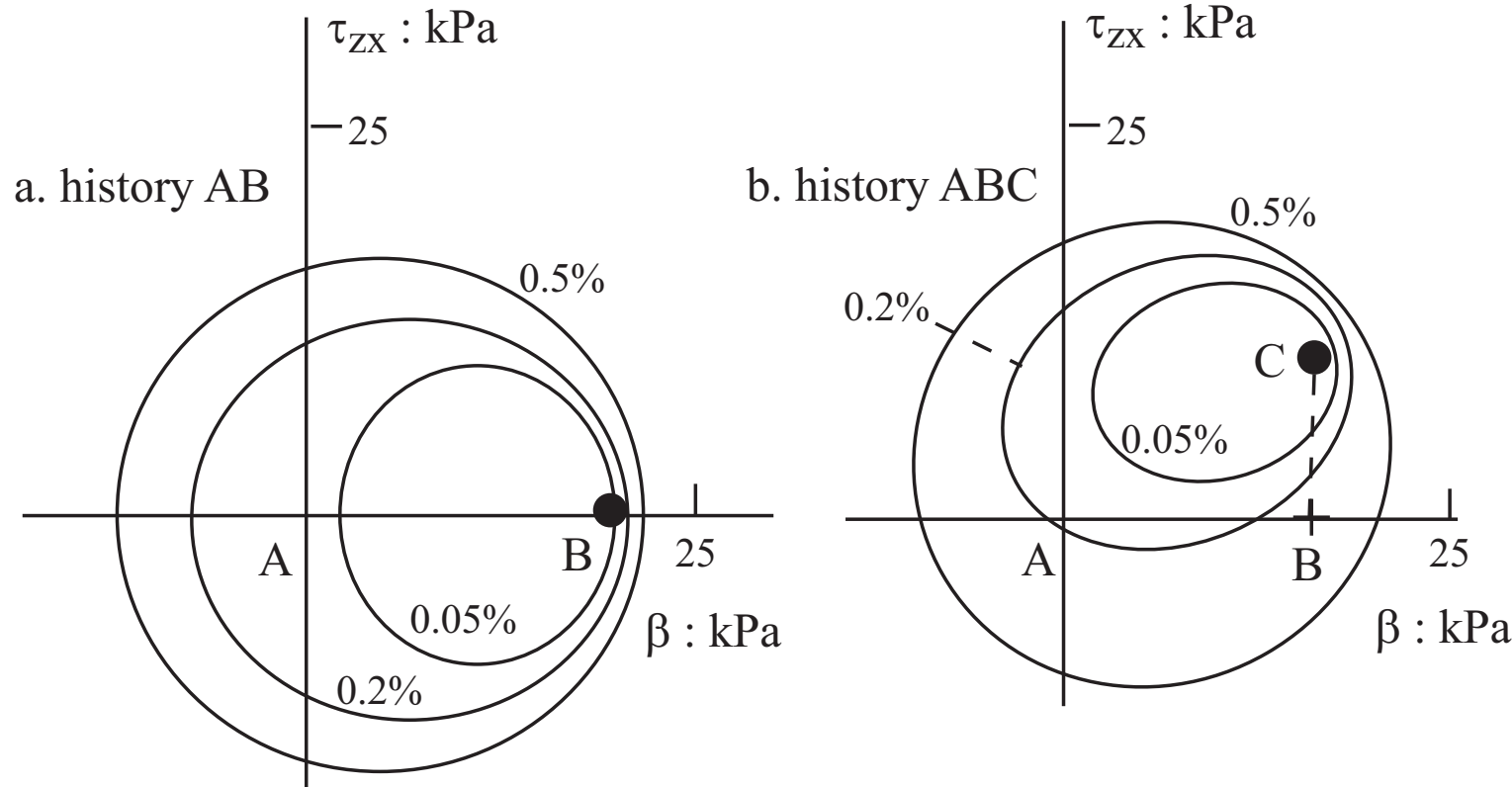
a. history ABC



b. history ABD

- true triaxial probing of Leighton Buzzard sand
- schematic deviatoric stress response envelopes
- deviatoric history (a) ABC and (b) ABD (data from Sture *et al.*, 1988)

Basic features of soil response: stiffness



- directional shear cell probing of Leighton Buzzard sand
- schematic deviatoric stress response envelopes
- deviatoric history (a) AB and (b) ABC (data from Sture *et al.*, 1988)
- rotation of principal axes

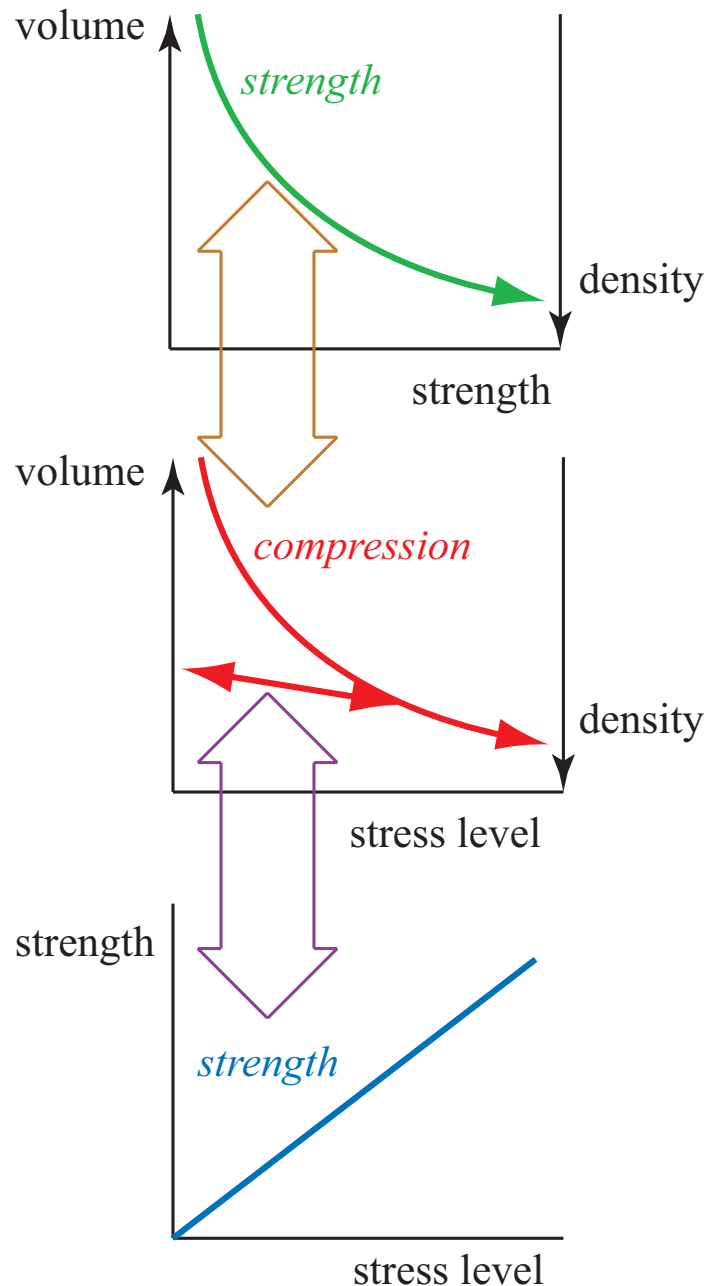
Basic features of soil response: stiffness

- history dependence of stress response envelopes
- stiffness high for strain reversal
- stiffness low for continuing loading
- erasure of memory of past events
- messages for modelling

Basic features of soil response: critical states

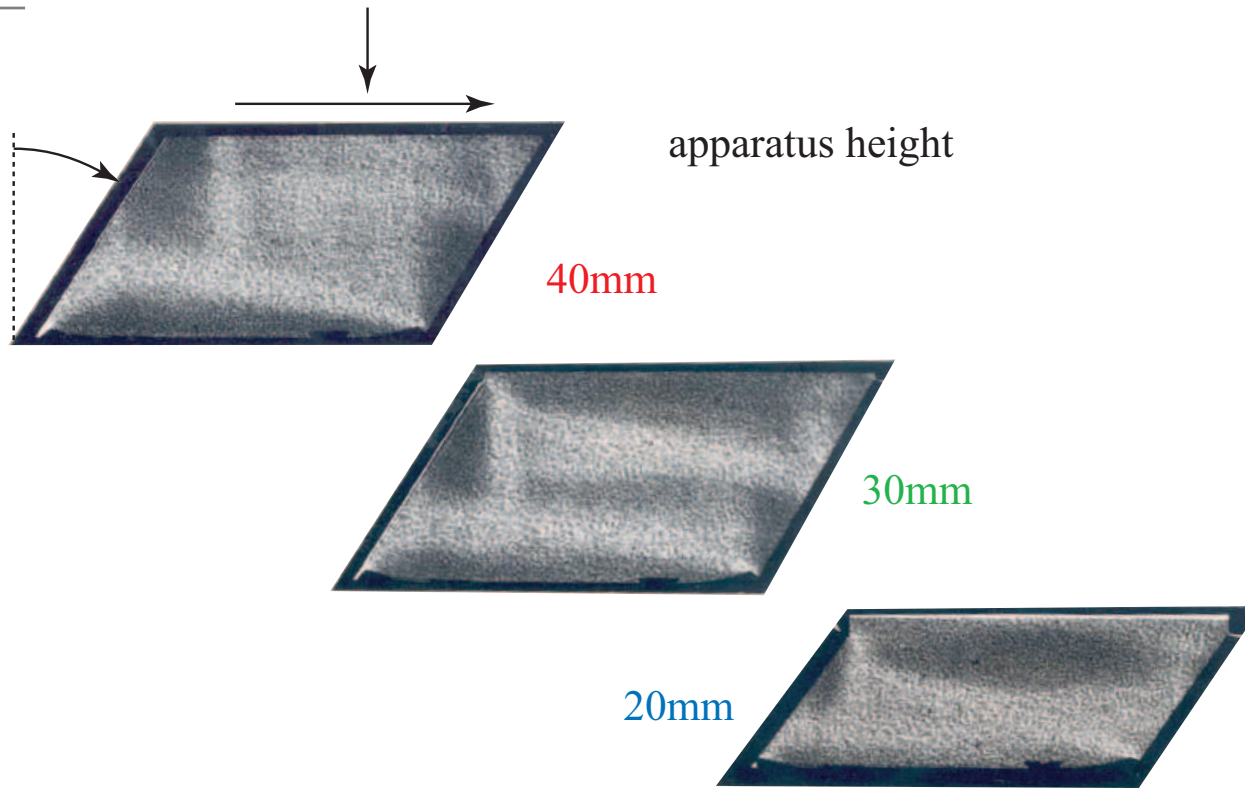
- asymptotic state reached at large strain
- state = stresses, density, fabric (particle arrangement)
- evidence from experiments on soils
- evidence from discrete element modelling
- central feature of constitutive models (explicit or implicit)

Basic features of soil response: critical states



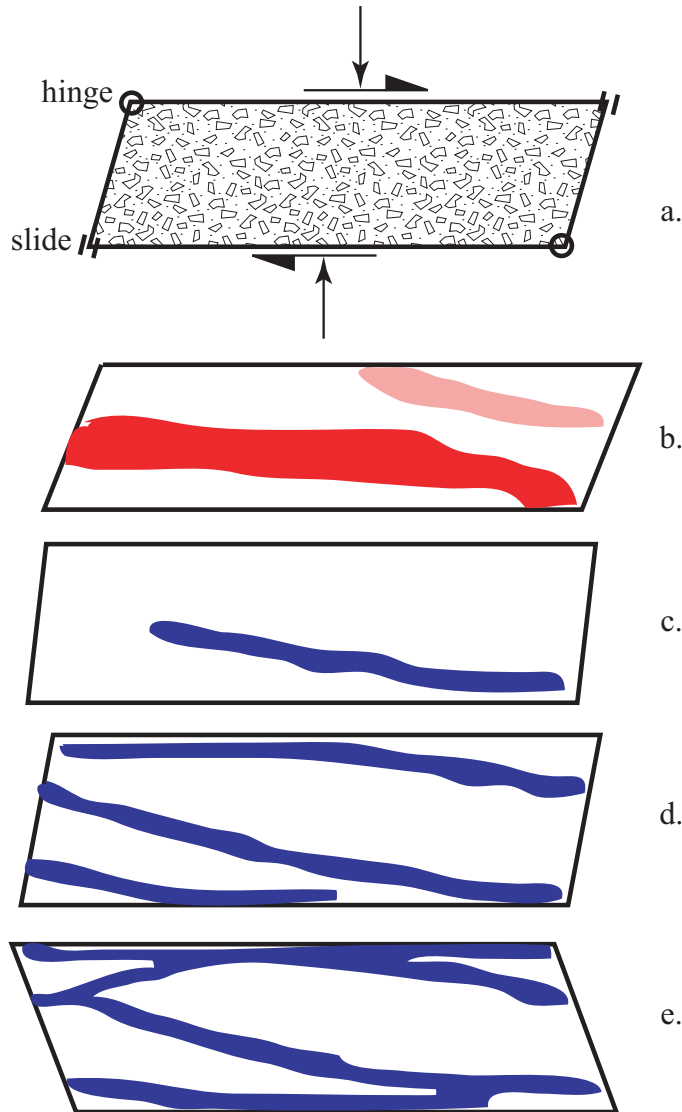
- critical state soil mechanics (weak form)
- discipline for exploring and interpreting mechanical response of soils
- importance of considering stresses *and* density

Basic features of soil response: critical states



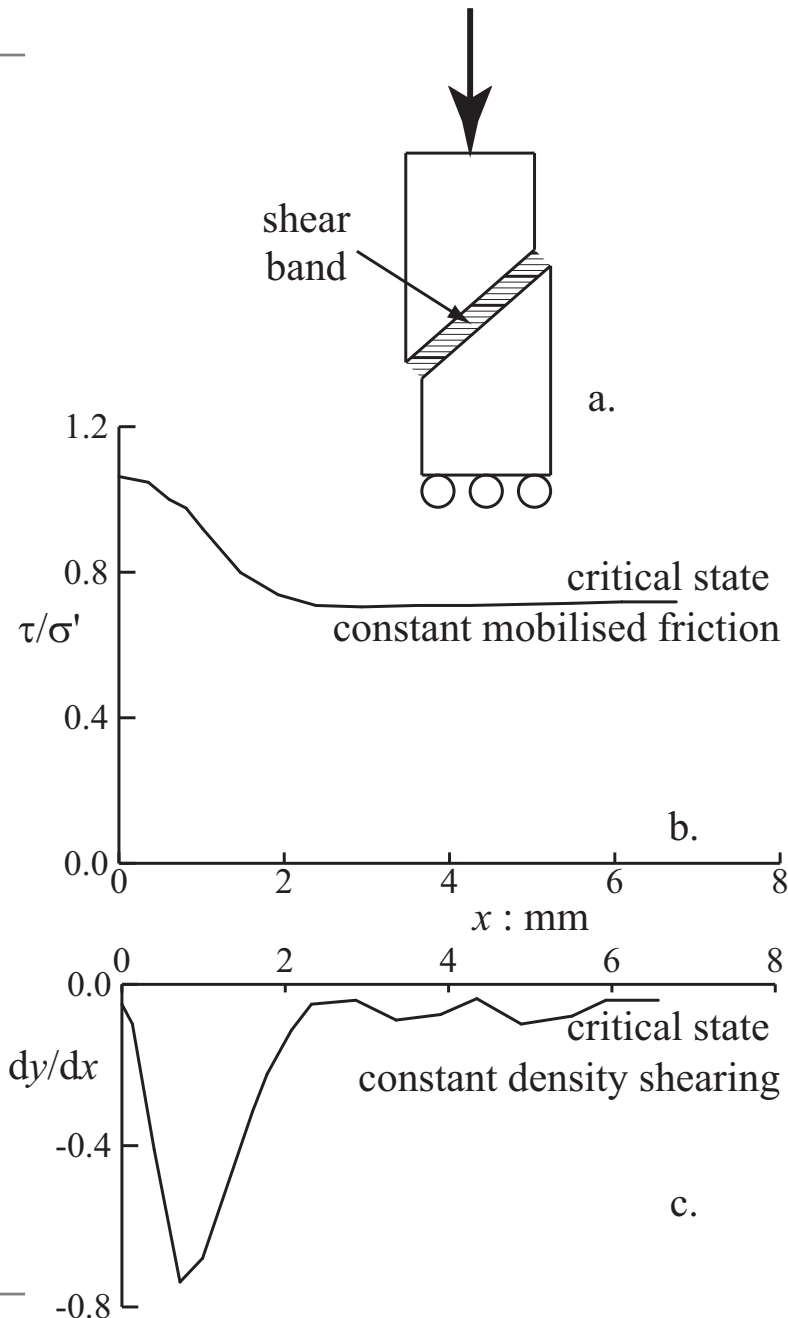
- observation of critical states? simple shear apparatus?
- internal kinematic freedom
- occurrence of localisation
- (Bassett)

Basic features of soil response: critical states



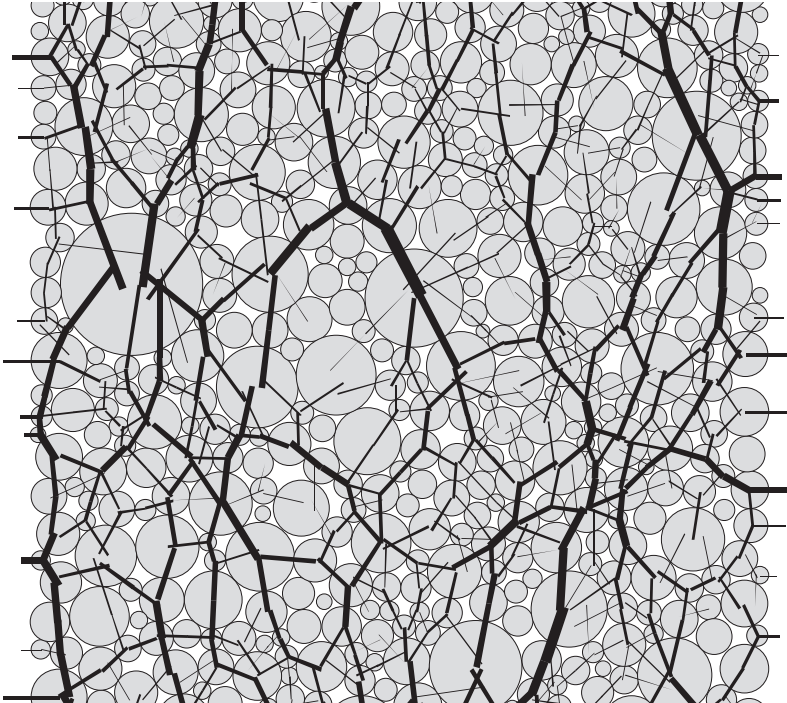
- simple shear apparatus - sample height ~ 20 mm
- coarse sand $d_{50} = \sim 1$ mm - uniform?
- fine sand $d_{50} = \sim 0.3$ mm
- (Stroud, Budhu)

Basic features of soil response: critical states



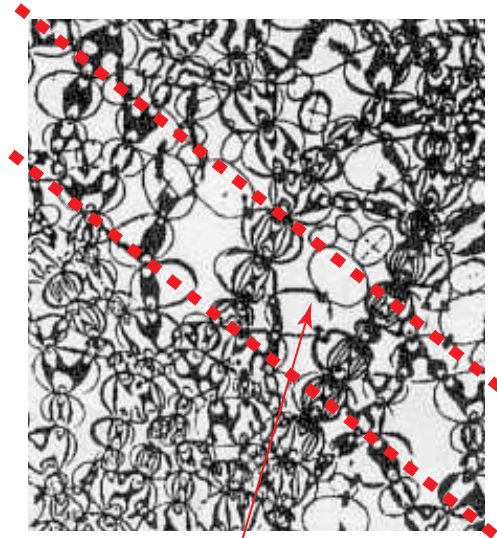
- biaxial plane strain test
- free formation of shear band
- critical state reached in shear band - not elsewhere
- free formation of shear band
- (Vardoulakis)

Basic features of soil response: critical states



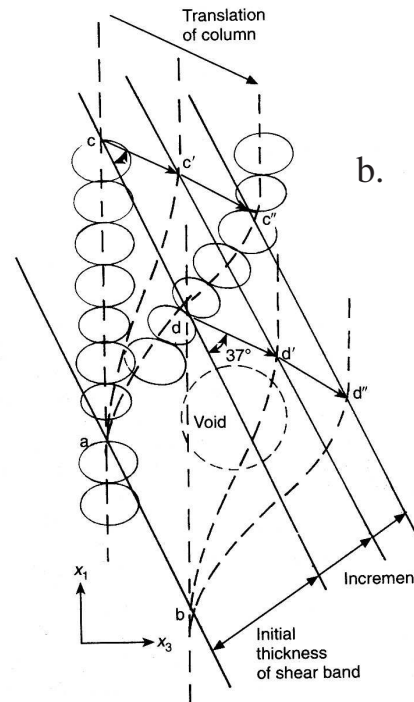
- discrete element modelling
- force chains of heavily loaded particles
- buckling of force chains encouraged by principal stress rotation

Basic features of soil response: critical states



shear band

a.



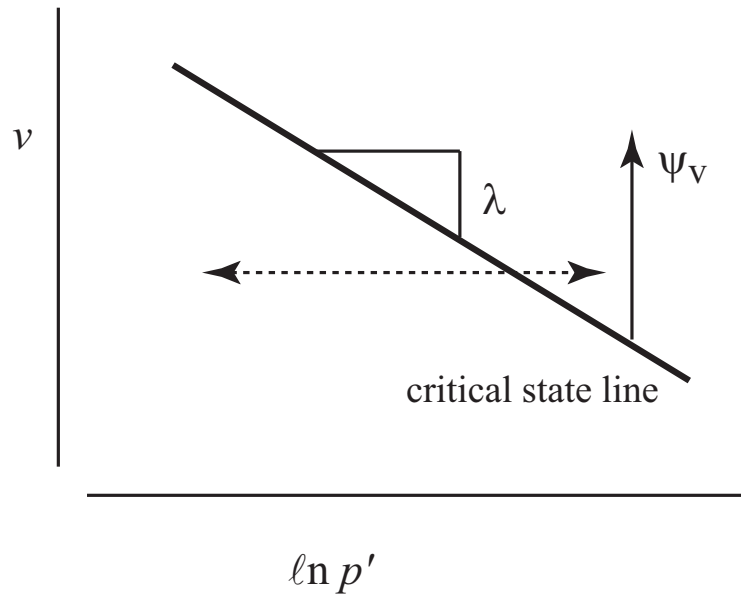
b.

- assembly of elliptical photoelastic discs
- force chains and voids in shear band
- buckling and rotation of columns in shear band
- (from Oda and Kazama, 1998)

Basic features of soil response: critical states

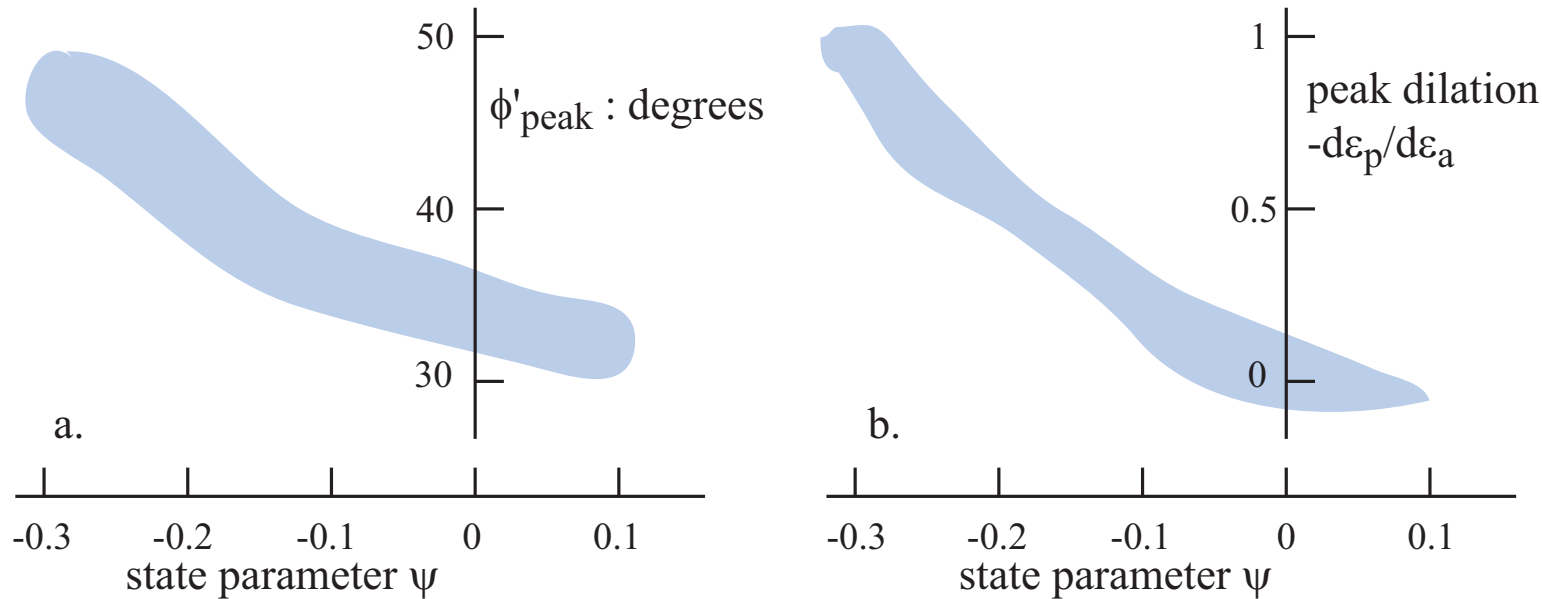
- asymptotic state reached at large strain
- fabric not isotropic at critical state
- difficult to detect experimentally
- central feature of constitutive models (explicit or implicit)

Basic features of soil response: strength



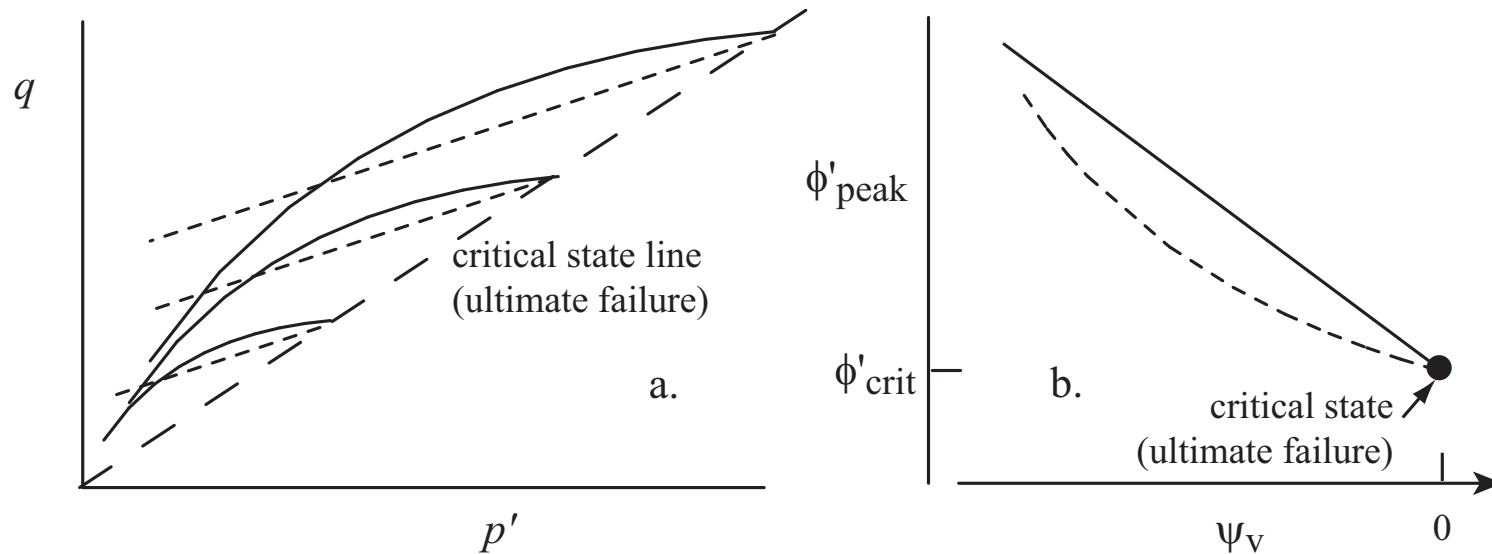
- critical state line
- state parameter or state variable as generalisation of 'dense', 'loose'
- $\psi = v - v_c = v - (\Gamma - \lambda \ln p')$
- semilogarithmic shape - not essential

Basic features of soil response: strength



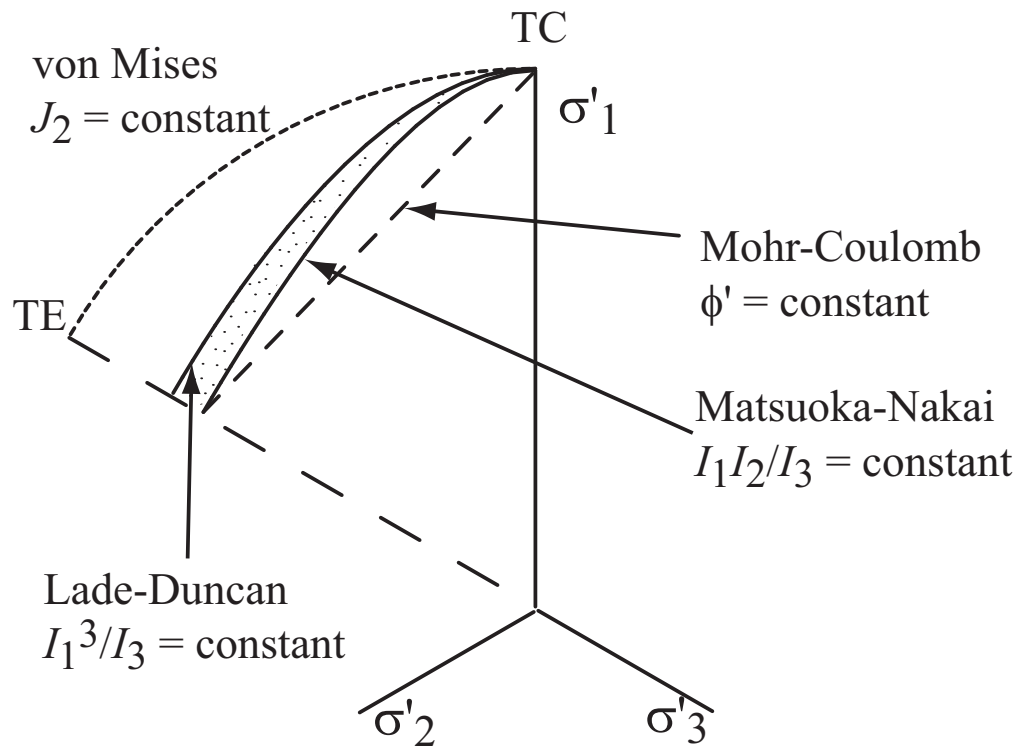
- dependence of peak strength on state parameter
- dependence of peak dilatancy on state parameter
- (Been & Jefferies)

Basic features of soil response: strength



- equivalence of failure relationships
- effective stress plane p', q
- friction angle and state parameter

Basic features of soil response: strength

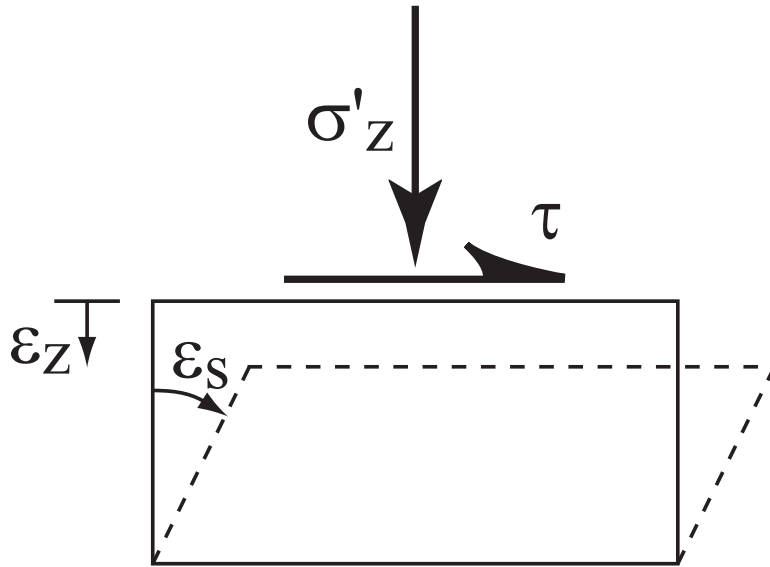


- **multiaxial stress conditions**
- **Matsuoka-Nakai: $I_1 I_2 / I_3 = \text{constant}$**
- **Lade-Duncan: $I_1^3 / I_3 = \text{constant}$**

Basic features of soil response: strength

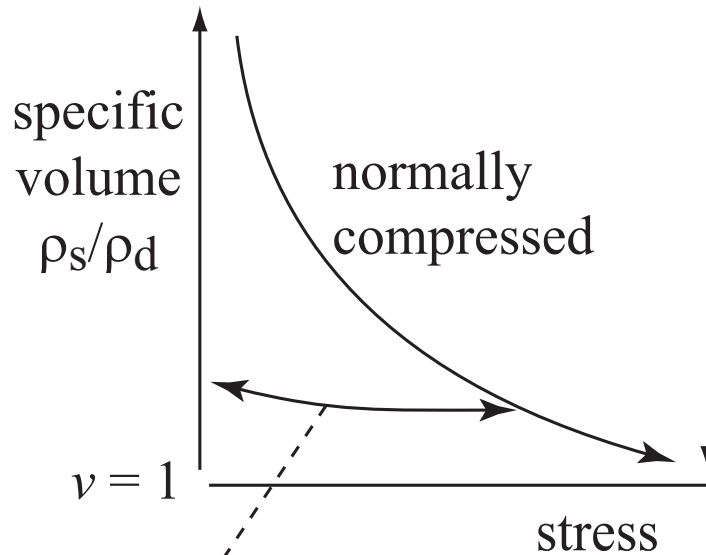
- importance of density and stress level
- peak strength is a dependent variable not a constant
- most stress conditions are not axisymmetric

Simple model of shearing



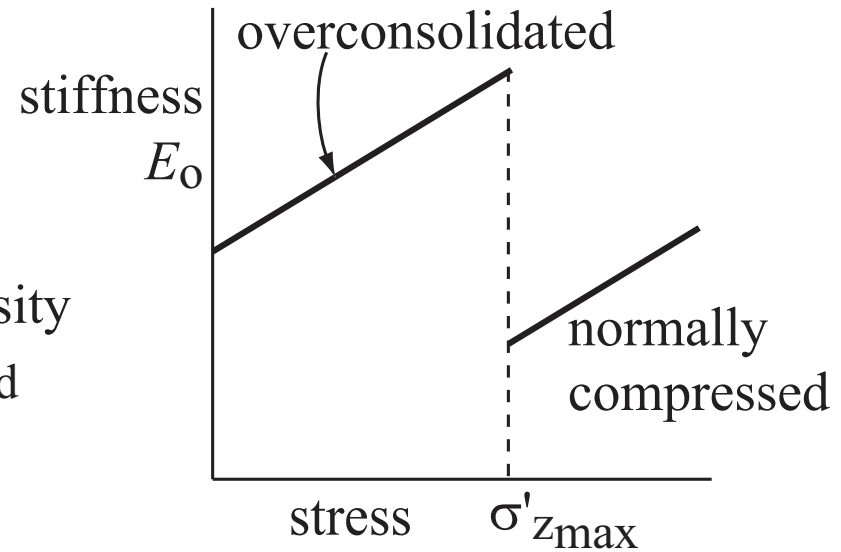
- build one-dimensional model
- simple shear/direct shear box
- separate vertical deformation (oedometer) and shearing
- stiffness - strength - dilatancy

Simple model of shearing



overconsolidated

a.



b.

stiffness - normal consolidation - overconsolidation

$$\frac{E_o}{\sigma_{ref}} = \chi \left(\frac{\sigma'_z}{\sigma_{ref}} \right)^\alpha$$

Simple model of shearing

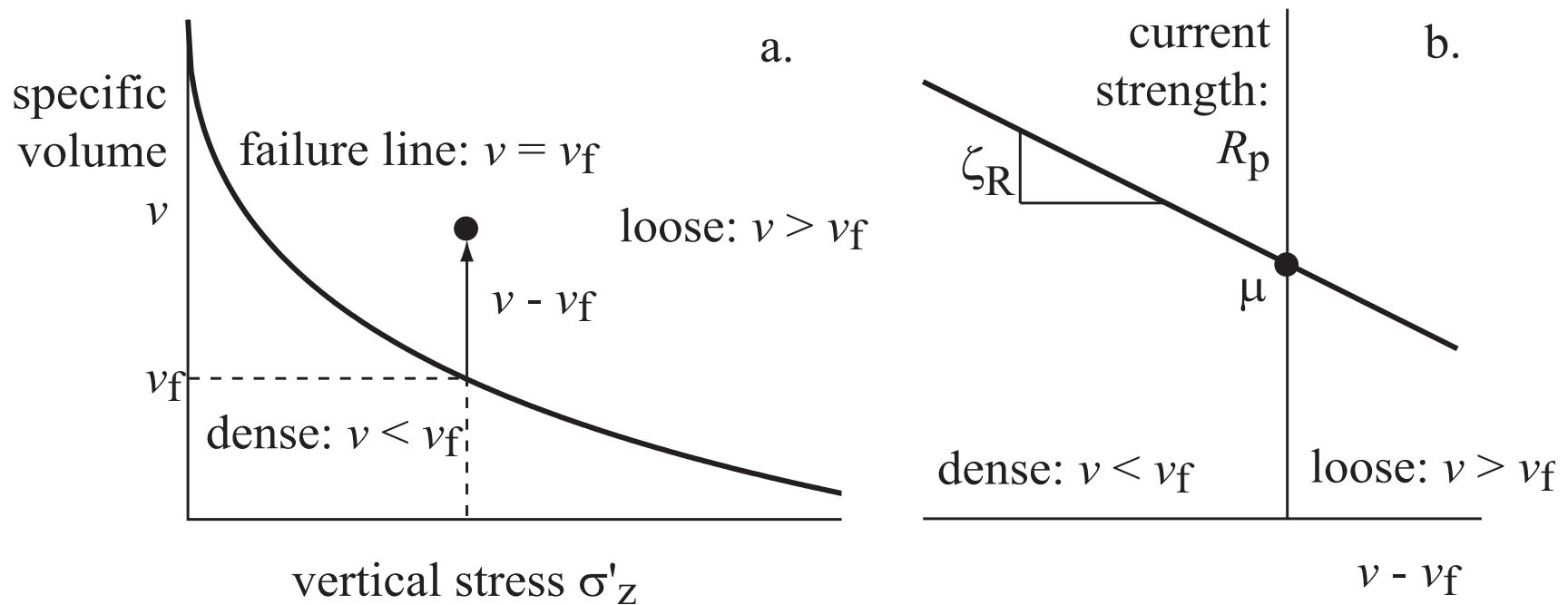
stiffness - normal consolidation (α_{nc}, χ_{nc}) -
overconsolidation (α_{oc}, χ_{oc})

$$\frac{E_o}{\sigma_{ref}} = \chi \left(\frac{\sigma'_z}{\sigma_{ref}} \right)^\alpha$$

$$\delta \varepsilon'_z = \delta \sigma'_z / E_o$$

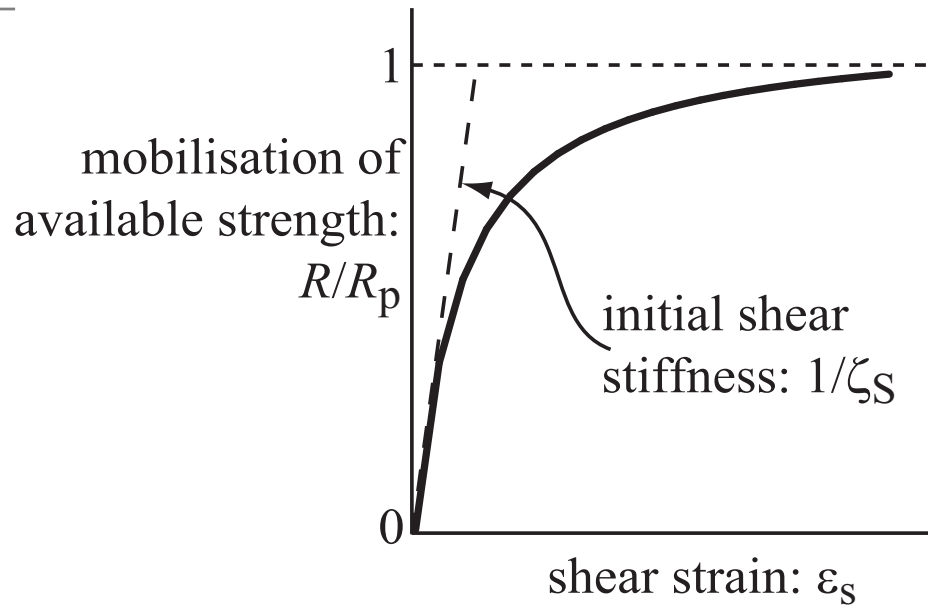
- If $\sigma'_z = \sigma'_{z_{max}}$ and $\delta \sigma'_z > 0$, then $n = 1$, $\alpha = \alpha_{nc}$ and $\chi = \chi_{nc}$ (normally compressed)
- If $\delta \sigma'_z < 0$, then $\delta n > 0$, $n \geq 1$, and $\alpha = \alpha_{oc}$ and $\chi = \chi_{oc}$ (overconsolidated)
- If $\sigma'_z < \sigma'_{z_{max}}$ and $\delta \sigma'_z > 0$, then $n > 1$, $\delta n < 0$, and $\alpha = \alpha_{oc}$ and $\chi = \chi_{oc}$ (overconsolidated)

Simple model of shearing



- **critical state line** $v_f = v_{min} + \Delta v \exp \left[-(\sigma'_z / \sigma_{ref})^\beta \right]$
- **state parameter** $\psi = v - v_f$
- **current strength** $R_p = \mu + \zeta_R(v_f - v)$
- **strength is a variable**

Simple model of shearing

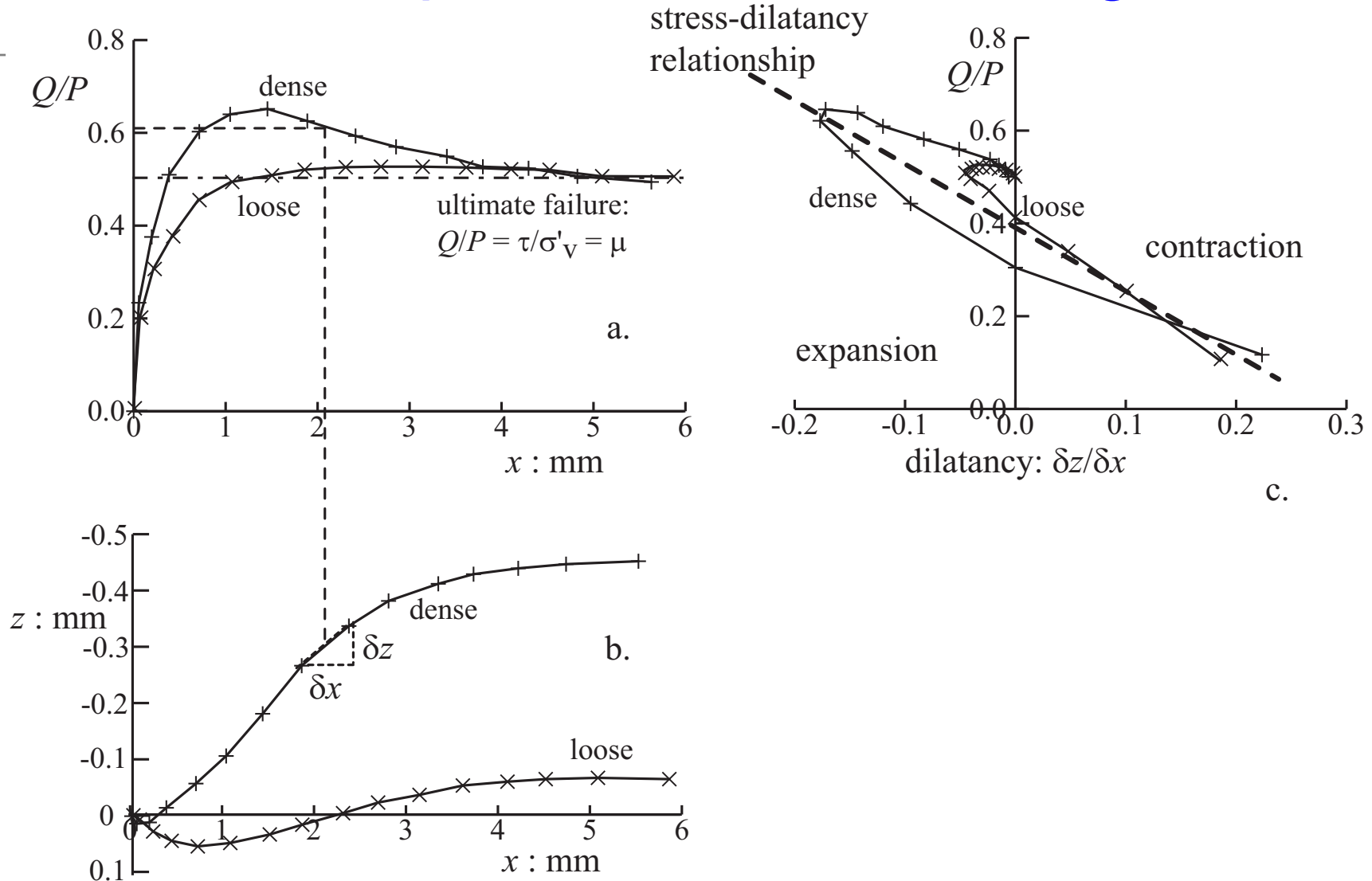


hyperbolic mobilisation of strength

$$\frac{R}{R_p} = \frac{\varepsilon_s}{\zeta_s + \varepsilon_s}$$

$$\delta R = \frac{1}{R_p} \left[(R_p - R)^2 \frac{\delta \varepsilon_s}{\zeta_s} + R \delta R_p \right]$$

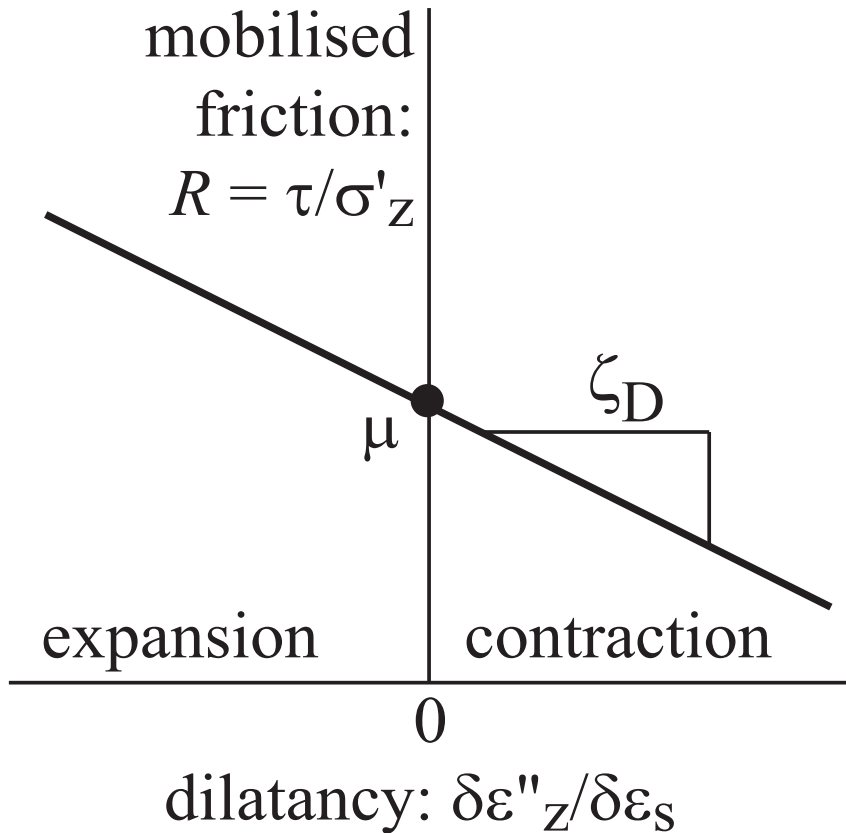
Simple model of shearing



- shear box data for dense and loose sand
- stress-dilatancy relationship (Taylor)

Simple model of shearing

stress-dilatancy relationship



$$\frac{\delta\epsilon''_z}{\delta\epsilon_s} = \zeta_D(\mu - R)$$

- feedback mechanism: if soil not at critical state, volume change occurs to bring it to asymptotic critical state
- total vertical strain
 $\delta\epsilon_z = \delta\epsilon'_z + \delta\epsilon''_z$
- **elasticity + dilatancy**

Simple model of shearing

complete stress-strain stiffness relationship

$$\delta\sigma'_z = E_o[\delta\varepsilon_z - \Psi_3\delta\varepsilon_s]$$

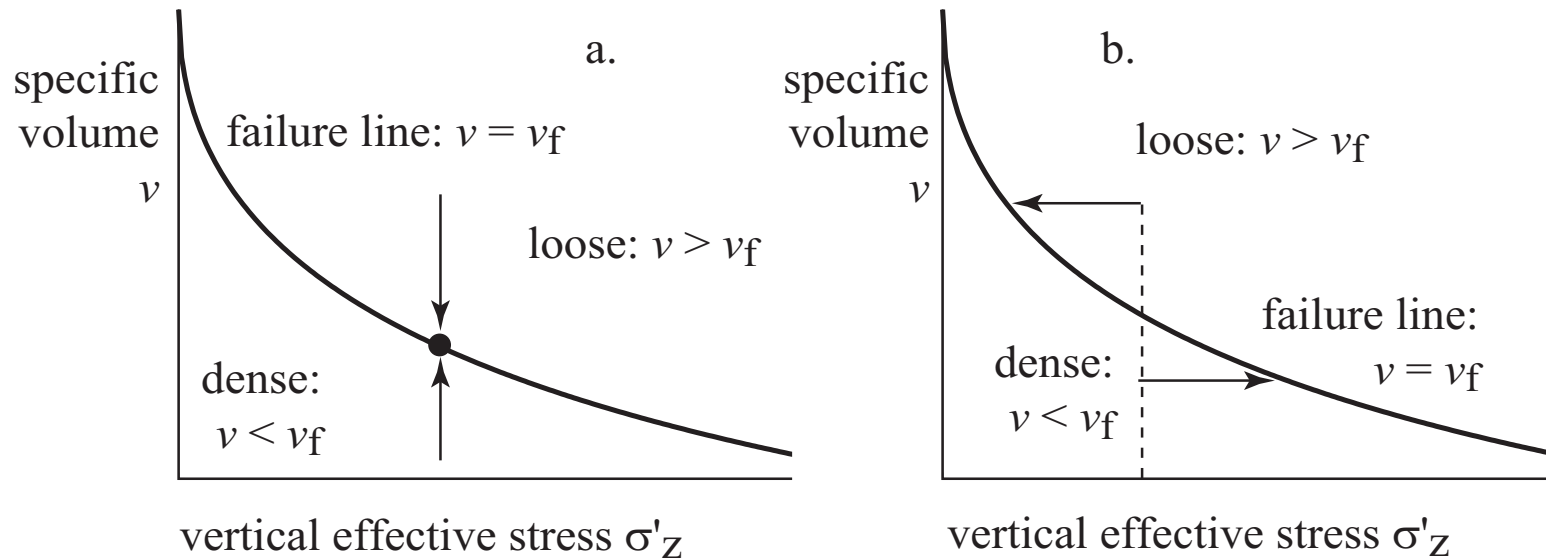
$$\delta\tau = E_o[-\Psi_1\delta\varepsilon_z + (\Psi_2 + \Psi_1\Psi_3)\delta\varepsilon_s]$$

$$\Psi_1 = \frac{\zeta_R R}{R_p} \left[\beta(v_f - v_{min}) \left(\frac{\sigma'_z}{\sigma_{ref}} \right)^\beta - \frac{v\sigma'_z}{E_o} \right] - R$$

$$\Psi_2 = \left[\frac{(R_p - R)^2}{\zeta_S R_p} + \frac{\zeta_R v R \Psi_3}{R_p} \right] \frac{\sigma'_z}{E_o}$$

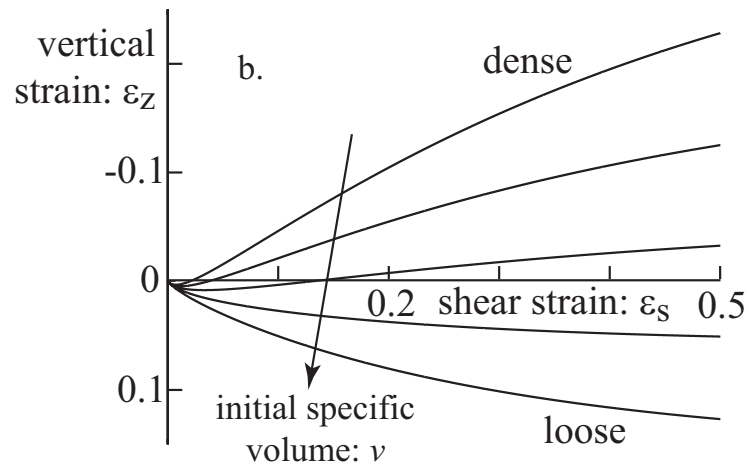
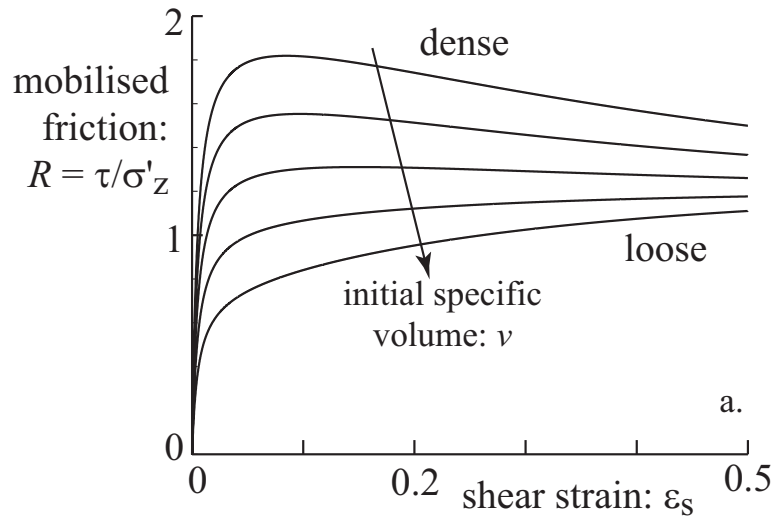
$$\Psi_3 = \zeta_D(\mu - R)$$

Simple model of shearing



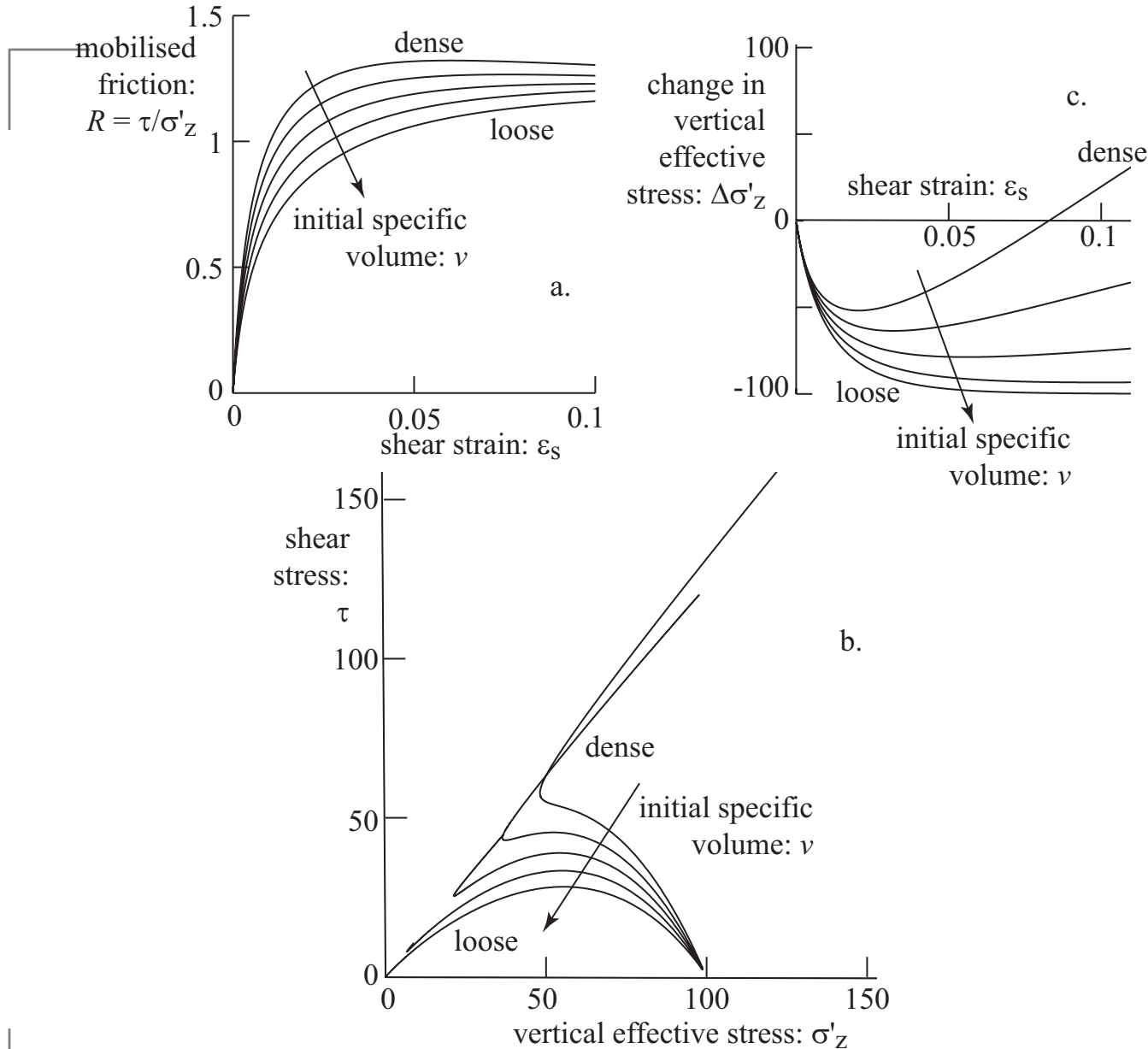
- $\delta\sigma'_z = E_o[\delta\varepsilon_z - \Psi_3\delta\varepsilon_s]$
- $\delta\tau = E_o[-\Psi_1\delta\varepsilon_z + (\Psi_2 + \Psi_1\Psi_3)\delta\varepsilon_s]$
- **drained (constant σ'_z):** $\delta\tau = \Psi_2 E_o \delta\varepsilon_s$, $\delta\varepsilon_z = \Psi_3 \delta\varepsilon_s$
- **undrained (constant height)** $\delta\tau = (\Psi_2 + \Psi_1\Psi_3) E_o \delta\varepsilon_s$,
 $\delta\sigma'_z / \delta\tau = -\Psi_3 / (\Psi_2 + \Psi_1\Psi_3)$

Simple model of shearing



- drained shearing with different initial densities

Simple model of shearing



- undrained shearing with different initial densities

Simple model of shearing

- one-dimensional model
- stiffness - strength - state parameter - dilatancy
- rich range of predicted responses